



Geophysical methods in geoscience and near surface geophysics Ground Penetrating Radar

Pisa, 22 January 2025

- Azadeh Hojat (azadeh.hojat@polimi.it)



IR0000032 – ITINERIS, Italian Integrated Environmental Research Infrastructures System
(D.D. n. 130/2022 - CUP B53C22002150006) Funded by EU - Next Generation EU PNRR-
Mission 4 "Education and Research" - Component 2: "From research to business" - Investment
3.1: "Fund for the realisation of an integrated system of research and innovation infrastructures"

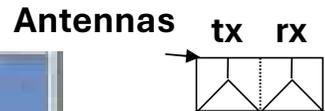


Ground Penetrating Radar (6 hours):

- Principles of operation of the GPR technique
- Electrical permittivity
- Reflection and transmission coefficients
- Directivity of antennas
- Spatial aliasing
- Radargram
- Velocity analysis in the GPR case
- Application examples

GPR (Ground Penetrating Radar) method

Acquisition

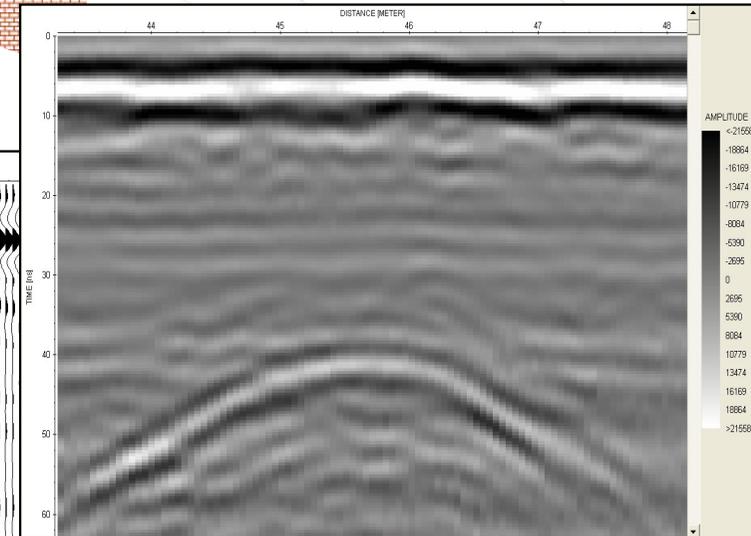
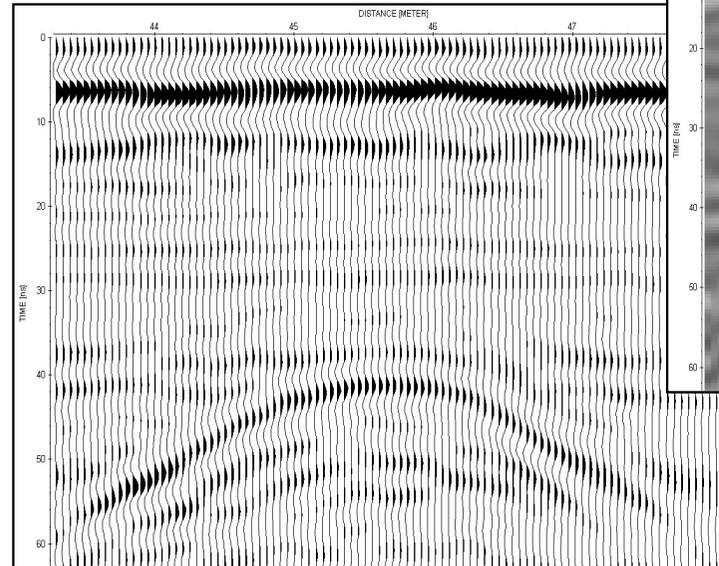


masonry bridge

Data

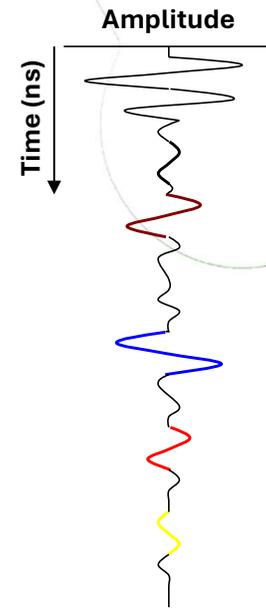
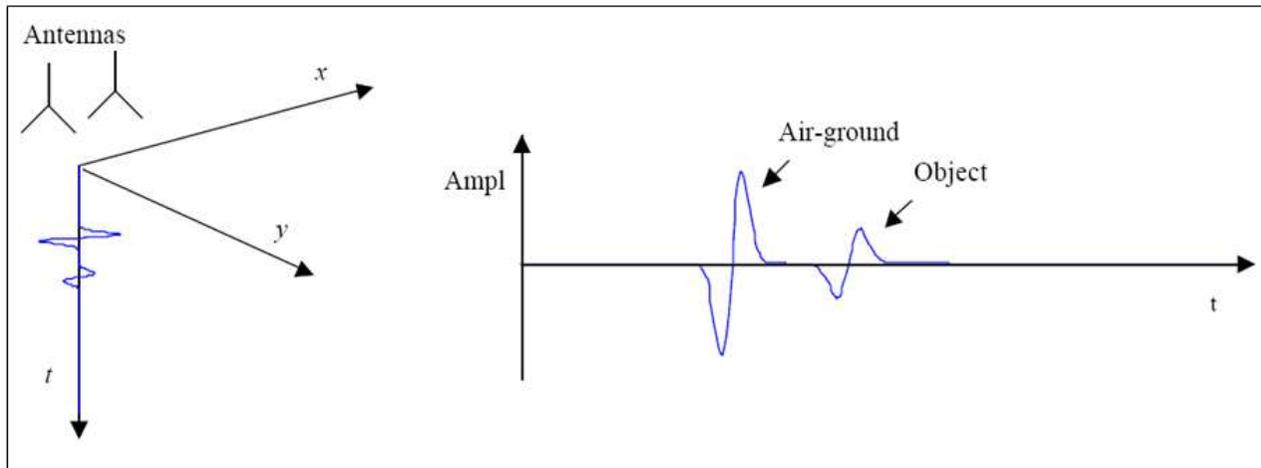


Data



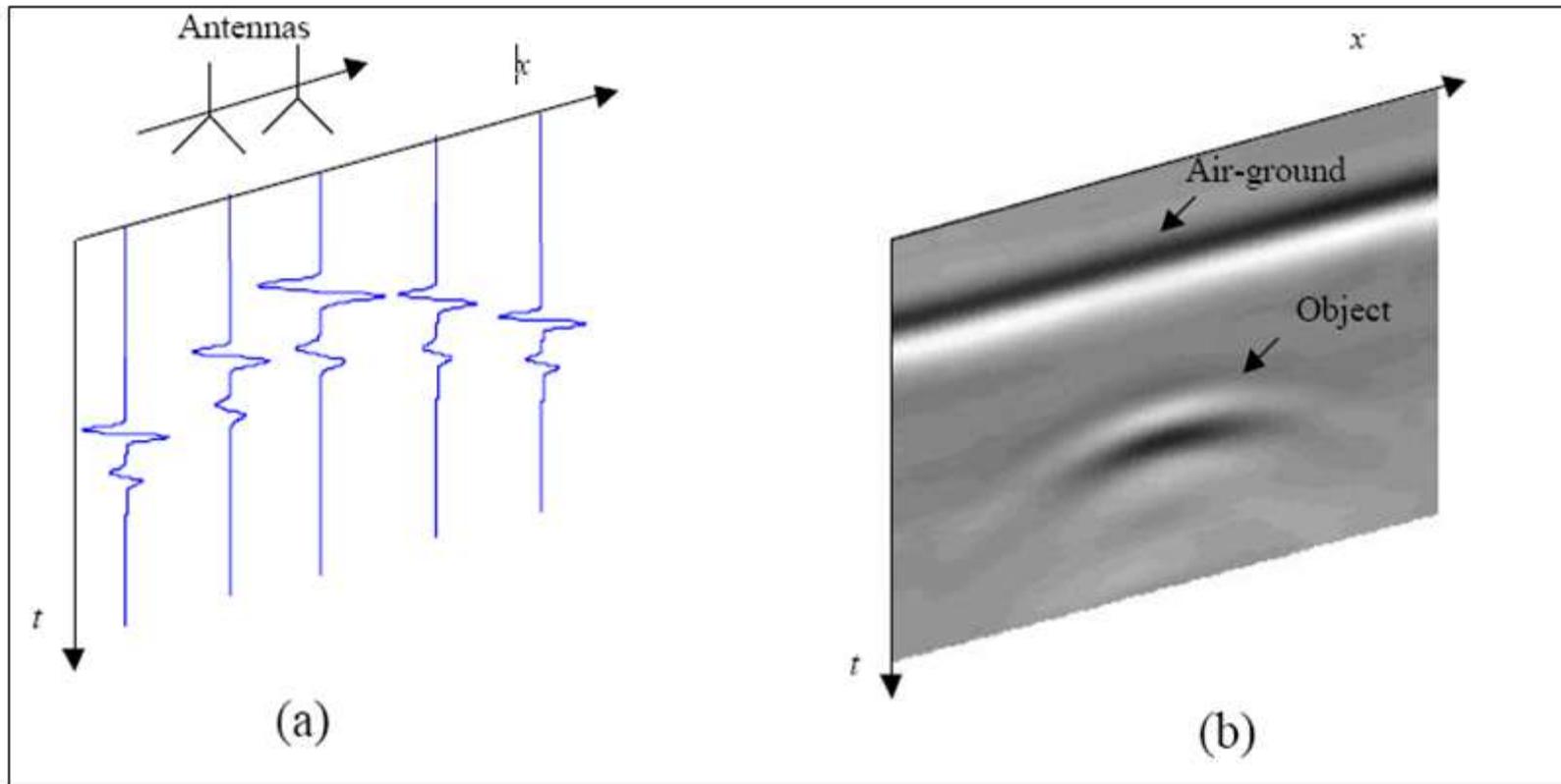
A-scan (1D-radar survey)

Configuration and representation of an A-scan.



(Scheers, 2001, U.C. Louvain)

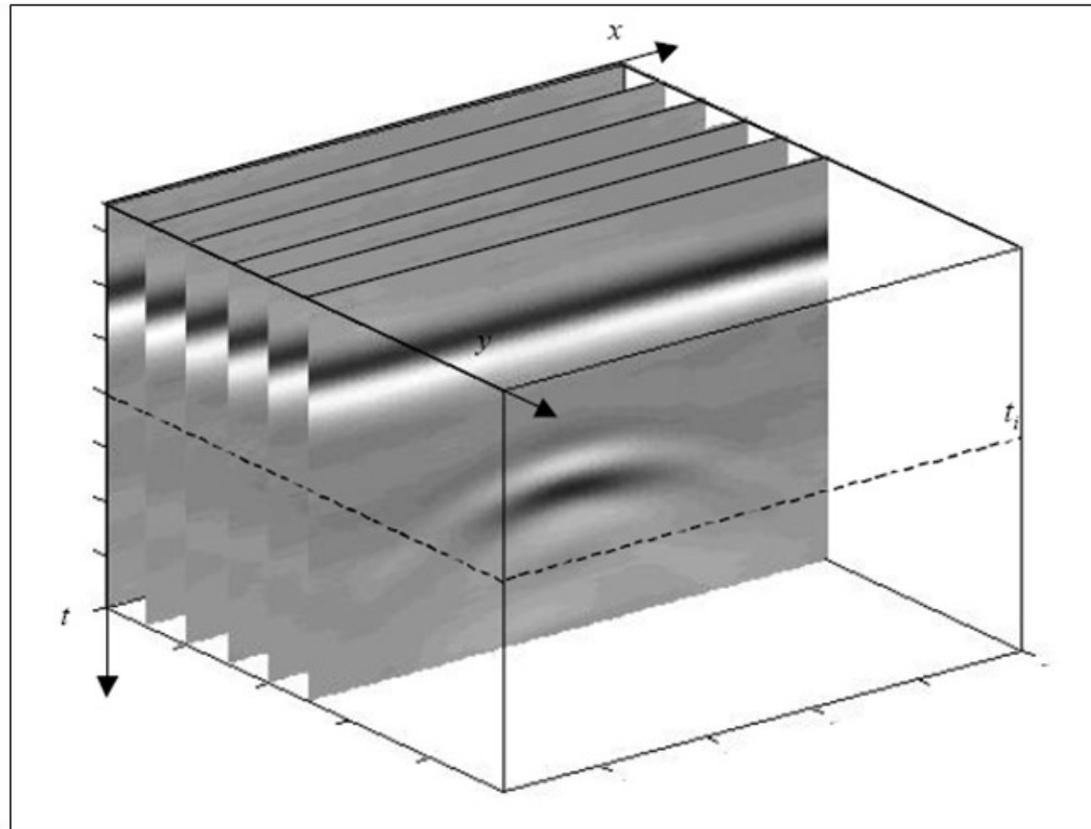
B-scan (2D-radar survey)



(a) Multiple A-scans forming a B-scan. (b) Representation of a B-Scan on a grey-scale.

(Scheers, 2001, U.C. Louvain)

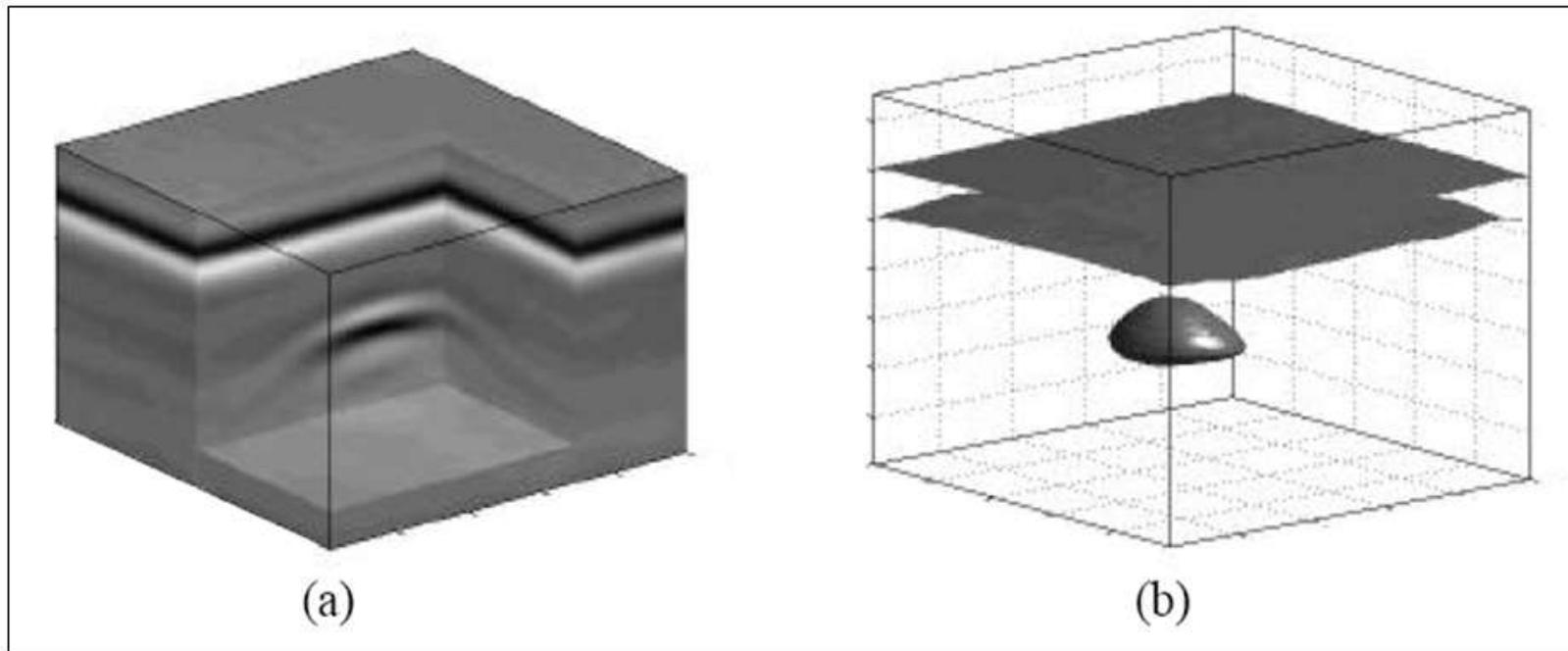
C-scan (3D-radar survey)



Multiple parallel B-scans forming a C-scan.

(Scheers, 2001, U.C. Louvain)

C-scan (3D-radar survey)

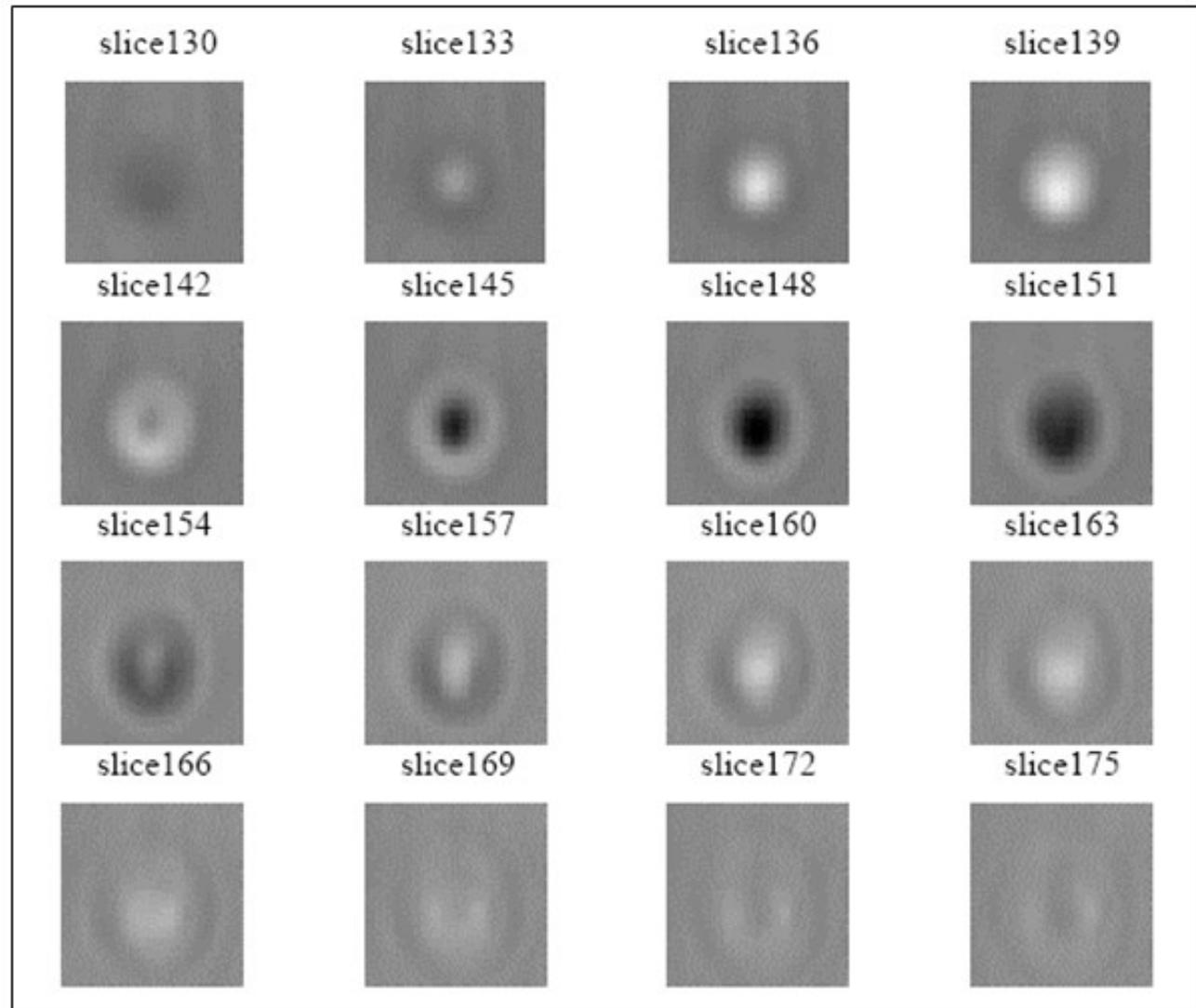


(a) Arbitrary cut in the 3-D volume. (b) Iso-surface representation.

(Scheers, 2001, U.C. Louvain)

C-scan (3D-radar survey)

Representation of a C-scan by horizontal slices at different depths.



(Scheers, 2001, U.C. Louvain)

Theory

Maxwell equations: $\nabla \wedge \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}$ $\nabla \wedge \vec{H} = \sigma \vec{E} + \varepsilon \frac{\partial \vec{E}}{\partial t}$

Since: $\nabla \wedge (\nabla \wedge \vec{V}) = \nabla(\nabla \cdot \vec{V}) - \nabla^2 \vec{V}$

$$\nabla \wedge (\nabla \wedge \vec{E}) = \nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -\mu \frac{\partial(\nabla \wedge \vec{H})}{\partial t}$$

\downarrow \downarrow

$= 0$ $= \sigma \vec{E} + \varepsilon \frac{\partial \vec{E}}{\partial t}$

$$\nabla^2 \vec{E} - \sigma \mu \frac{\partial \vec{E}}{\partial t} - \varepsilon \mu \frac{\partial^2 \vec{E}}{\partial t^2} = 0$$

The solution for a wave propagating in direction z in a homogeneous medium with an electric field parallel to x is:

$$E_x(z, t) = E_0 e^{-\gamma z} e^{j\omega t}$$

$$\gamma = \sqrt{j\omega\mu\sigma - \omega^2\mu\varepsilon} = \alpha + j\beta \rightarrow \text{phase constant}$$

γ = propagation constant, is a complex function

\downarrow attenuation factor

Theory

Thus: $E_x(z, t) = E_0 e^{-\alpha z} e^{j(\omega t - \beta z)}$

For a generic dielectric, permittivity is a complex number: $\epsilon = \epsilon' - j\epsilon''$

Then: $\gamma = \sqrt{-\omega^2 \mu \epsilon' + j\omega^2 \mu \epsilon'' + j\omega \mu \sigma} \Rightarrow \gamma = j\omega \sqrt{\mu \epsilon' \left[1 - j \left(\frac{\epsilon''}{\epsilon'} + \frac{\sigma}{\omega \epsilon'} \right) \right]}$

1 $\sigma = 0$ and $\epsilon'' = 0$ \Rightarrow $\alpha = 0$

2 $\sigma = 0$ and $\epsilon'' \ll \epsilon'$ \Rightarrow $\alpha \cong \omega \sqrt{\mu \epsilon'} \frac{\epsilon''}{2 \epsilon'}$

absorption is proportional to ϵ'' and to frequency

Theory

3 $\sigma \ll \varepsilon' \omega$ and $\varepsilon'' = 0$ \longrightarrow

absorption is proportional to σ and to frequency through ε'

$$\alpha \cong \sqrt{\mu \varepsilon'} \frac{\sigma}{2 \varepsilon'}$$

4 $\sigma \ll \varepsilon' \omega$ and $\varepsilon'' \ll \varepsilon'$ \longrightarrow

$$\alpha \cong \frac{\sqrt{\mu \varepsilon'}}{2 \varepsilon'} (\omega \varepsilon'' + \sigma)$$

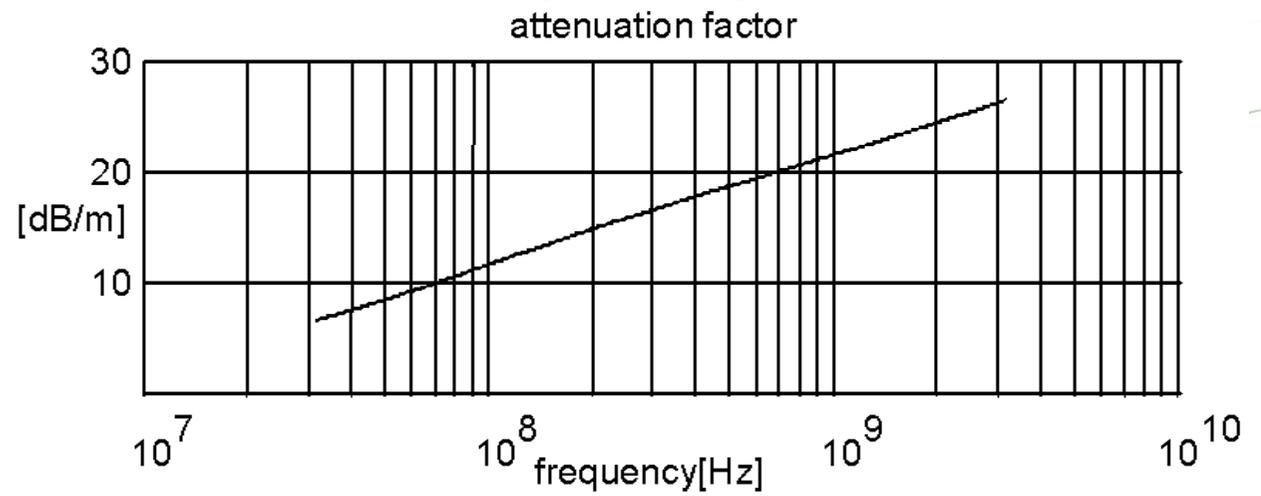
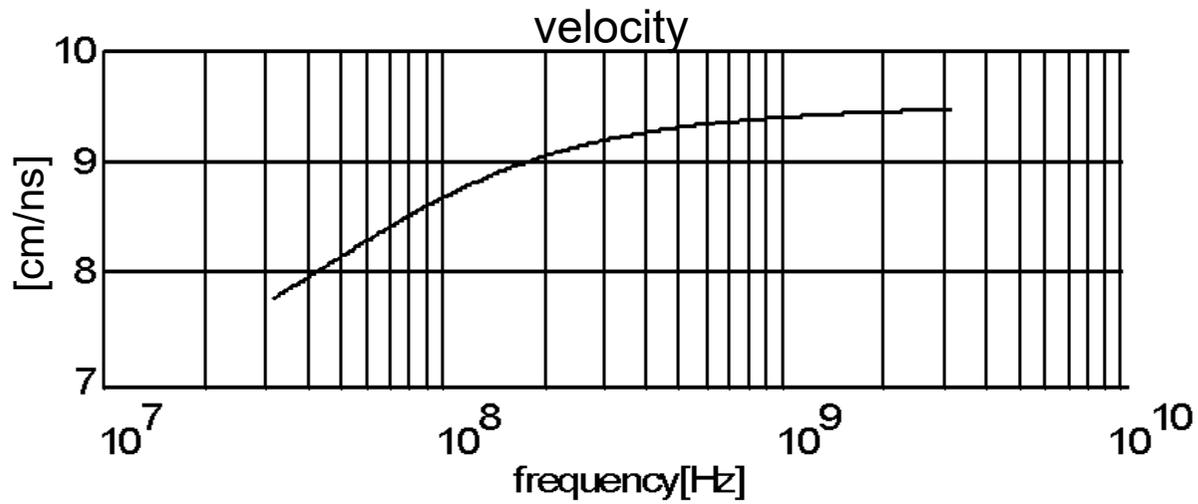
σ and ε'' are responsible for attenuation attenuation increases with frequency

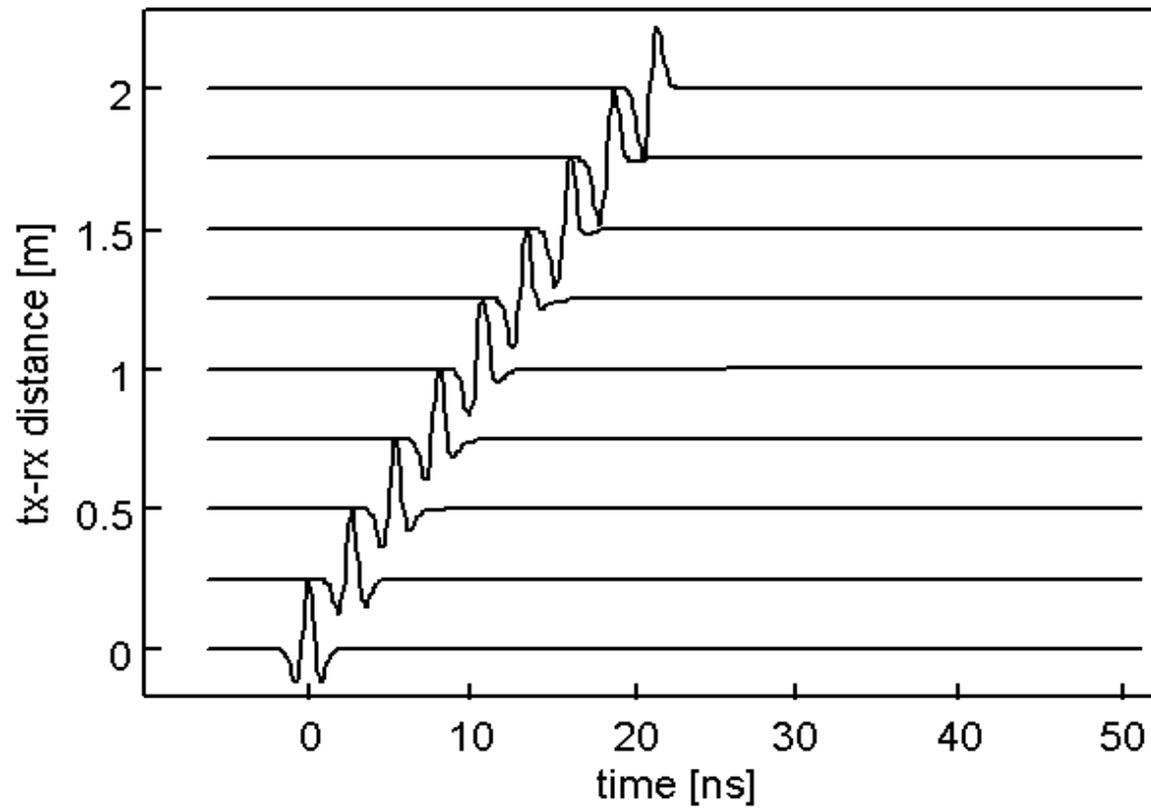
In all the situations: $\beta \cong \omega \sqrt{\mu \varepsilon'}$ \longrightarrow $v = \frac{\lambda}{T} = \frac{\omega}{\beta} \cong \frac{1}{\sqrt{\mu \varepsilon'}}$

If c indicates the speed of light, i.e., the free space velocity $c = \frac{1}{\sqrt{\mu_0 \varepsilon_0}}$ then $v \cong \frac{c}{\sqrt{\mu_r \varepsilon_r'}}$

Since for most rock formations, $\mu_r = 1$ \longrightarrow $v \cong \frac{c}{\sqrt{\varepsilon_r'}}$

Theory





500 MHz Ricker wavelet propagating at different distances through the medium

Reflection and transmission coefficients

When a wave arrives at a surface which separates two media with different electromagnetic characteristics, energy is partially reflected and partially transmitted.

For normal incidence  $R = \frac{Z_2 - Z_1}{Z_2 + Z_1}$ and $T = \frac{2Z_1}{Z_2 + Z_1}$ $Z = \sqrt{\frac{j\omega\mu}{j\omega\epsilon + \sigma}}$

Z = the electromagnetic impedance

Any μ or ϵ or σ contrast between two materials will produce a GPR energy return to the surface.

For perfect dielectric materials: $\sigma = 0$ and $\epsilon'' = 0$ 

$$Z = \sqrt{\frac{\mu}{\epsilon'}}$$

and considering that for most rock formations, $\mu_r = 1$: 

$$R = \frac{\sqrt{\epsilon_{r1}} - \sqrt{\epsilon_{r2}}}{\sqrt{\epsilon_{r1}} + \sqrt{\epsilon_{r2}}}$$

Reflection and transmission coefficients

For metal targets:

$$\sigma \Rightarrow \infty$$



$$Z = \sqrt{\frac{j\omega\mu}{j\omega\epsilon + \sigma}} \Rightarrow 0$$



$$R = \frac{Z_2 - Z_1}{Z_2 + Z_1} \Rightarrow -1$$

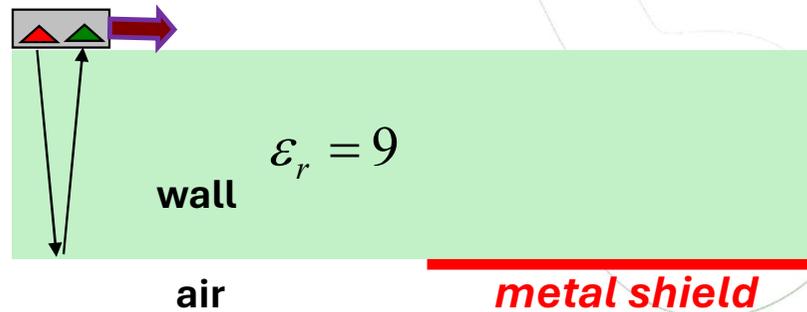
Example

$$R = \frac{\sqrt{\epsilon_{r1}} - \sqrt{\epsilon_{r2}}}{\sqrt{\epsilon_{r1}} + \sqrt{\epsilon_{r2}}}$$



$$R = \frac{3-1}{3+1} = 0.5$$

$$R > 0$$

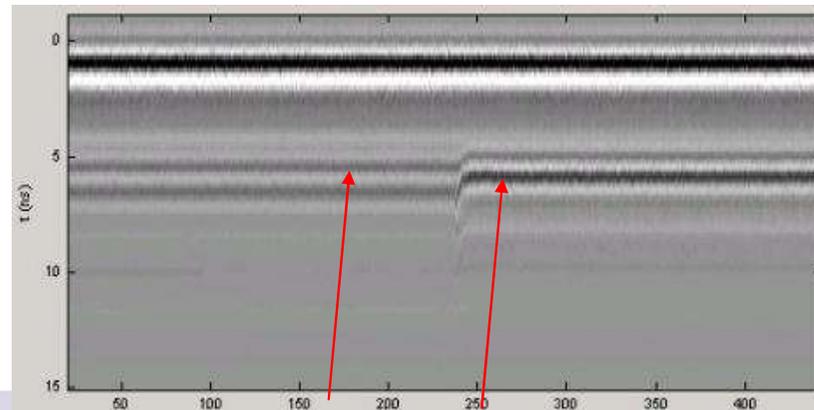


$$Z = 0$$



$$R = -1$$

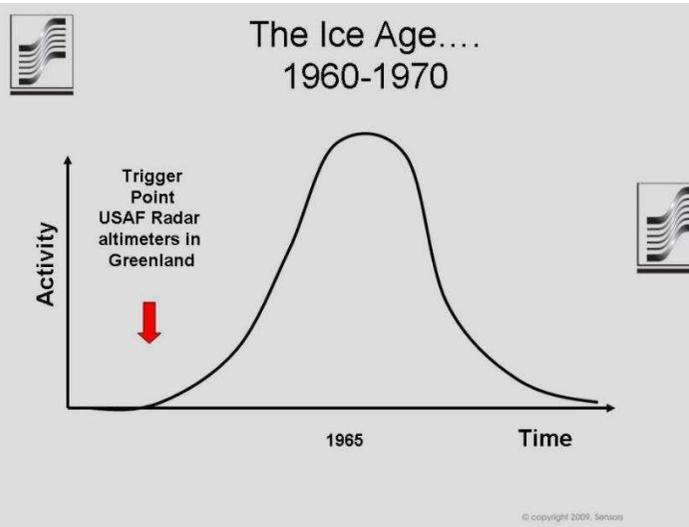
$$R < 0$$



reflections with opposite polarity

Material properties

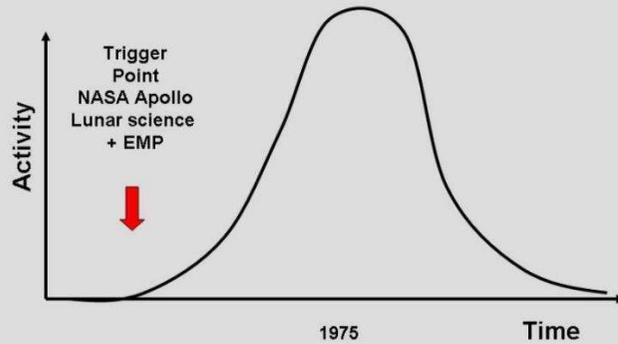
material	ϵ_r	σ (mS/m)	V (m/ns)	α (dB/m)
air	1	0	0.30	0
distilled water	80	0.01	0.033	2×10^{-3}
fresh water	80	0.5	0.033	0.1
salt water	80	3×10^4	0.01	10^3
dry sand	3-5	0.01	0.15	0.01
saturated sand	20-30	0.1-1.0	0.06	0.03-0.3
limestone	4-8	0.5-2	0.12	0.4-1
shale	5-15	1-100	0.09	1-100
silt	5-30	1-100	0.07	1-100
clay	5-40	2-1000	0.06	1-300
granite	4-6	0.01-1	0.13	0.01-1
dried salt	5-6	0.01-1	0.13	0.01-1
ice	3-4	0.01	0.16	0.01



Data acquisition



Soils & Rocks 1965-1980



© copyright 2009, Sensors & Software



Apollo Lunar Science Program

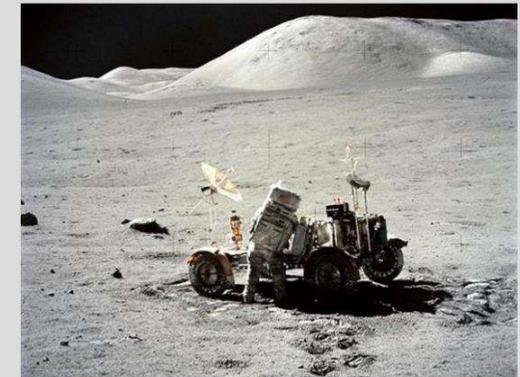


16

© copyright 2009, Sensors & Software



Apollo 17 Surface Electric Properties



17

© copyright 2009, Sensors & Software Inc.

Data acquisition

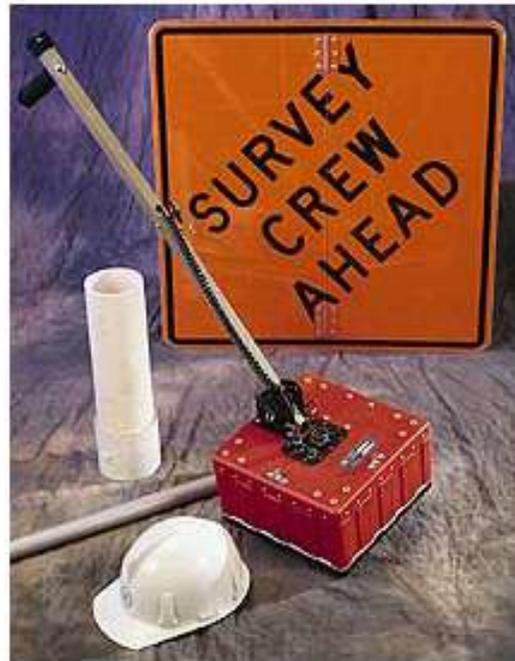
1971 First commercial GPR by GSSI

1990 First multi-channel GPR by GSSI (SIR10 model)

GSSI system (SIR20)



SIR-10 radar unit



400 MHz antenna



Data acquisition

**RAMAC system
(100MHz)**

**RAMAC system
(50 MHz unshielded)**



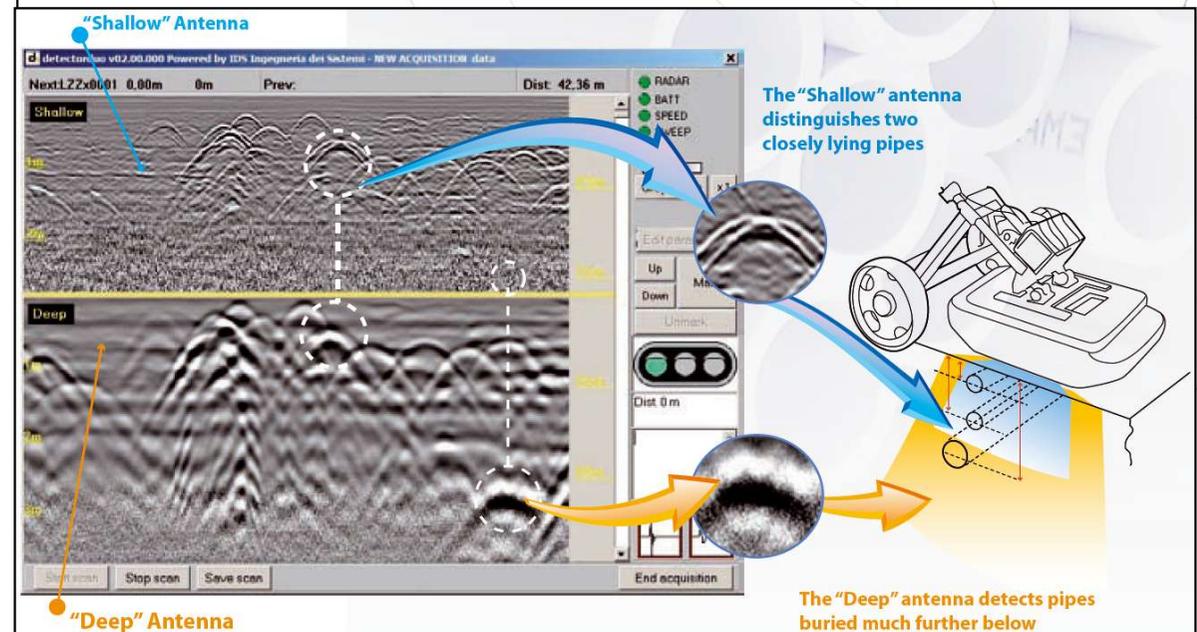
IDS antenna (200 MHz)



Multi-frequency antennas

Detector DUO (IDS)

250 and 700 MHz pairs in one antenna



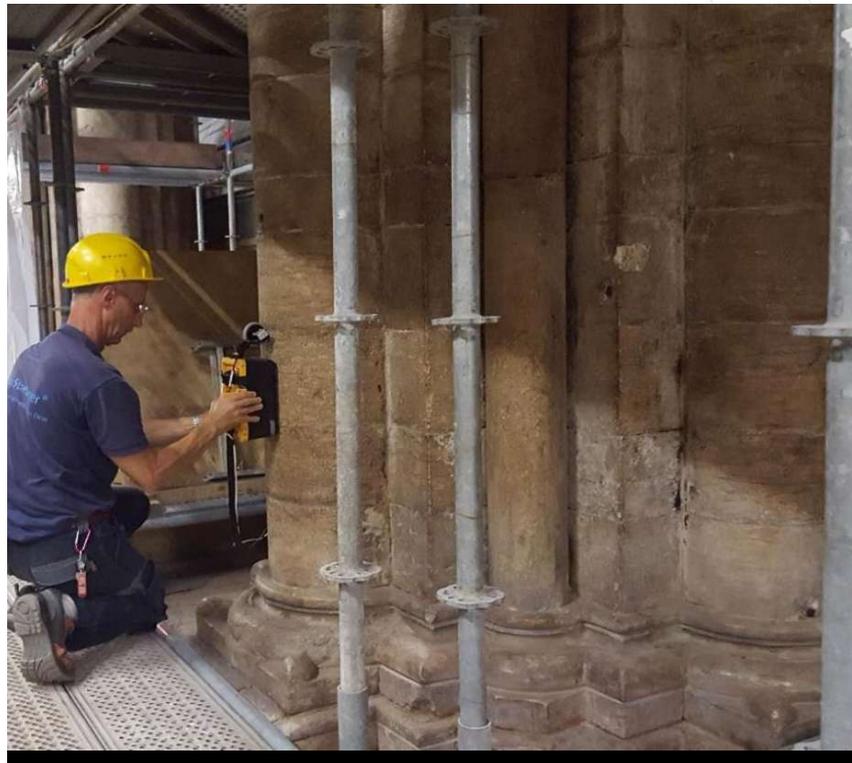
Data acquisition

SnowScan system (500 MHz)



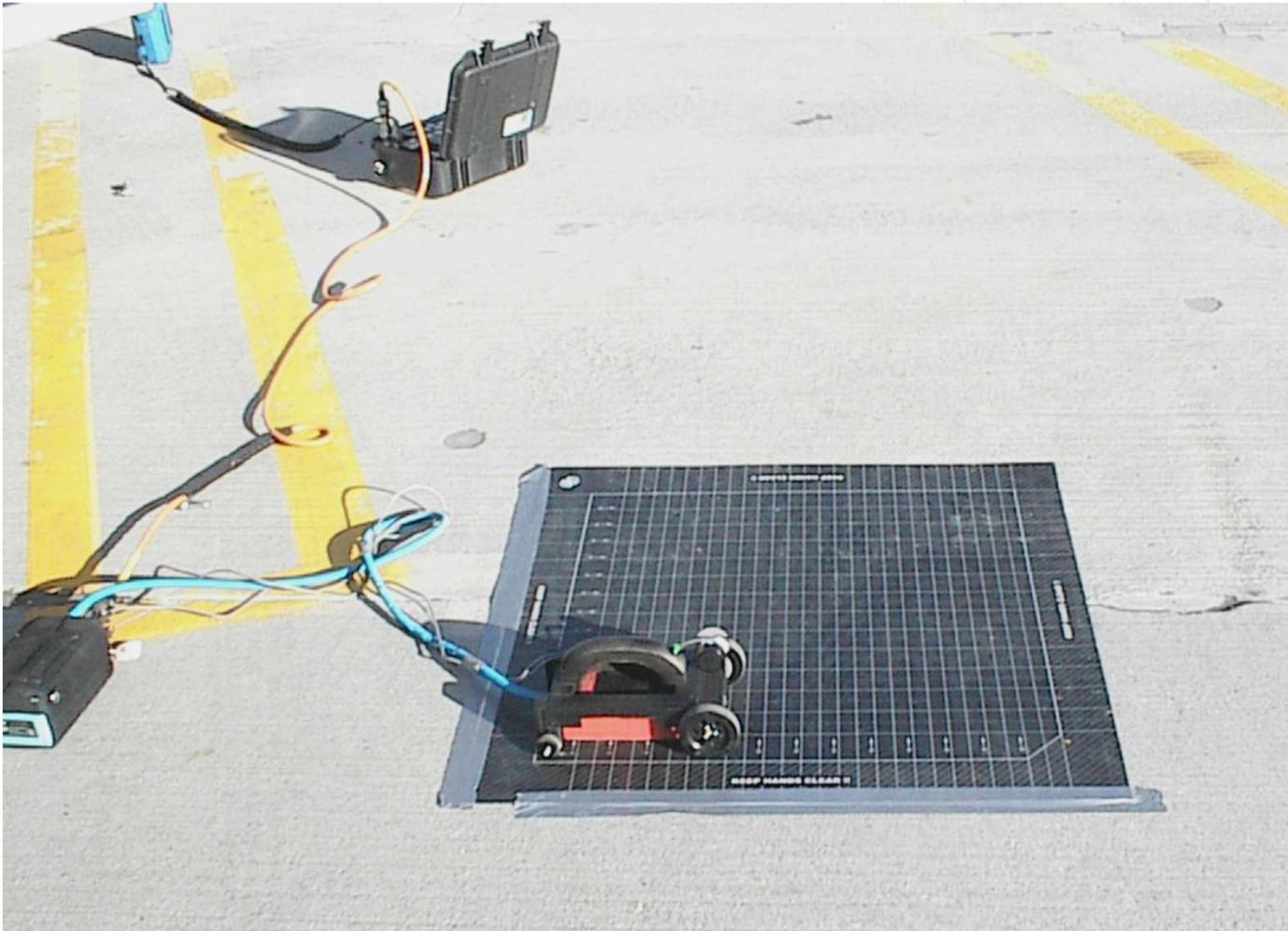
Data acquisition

RAMAC system (1GHz)



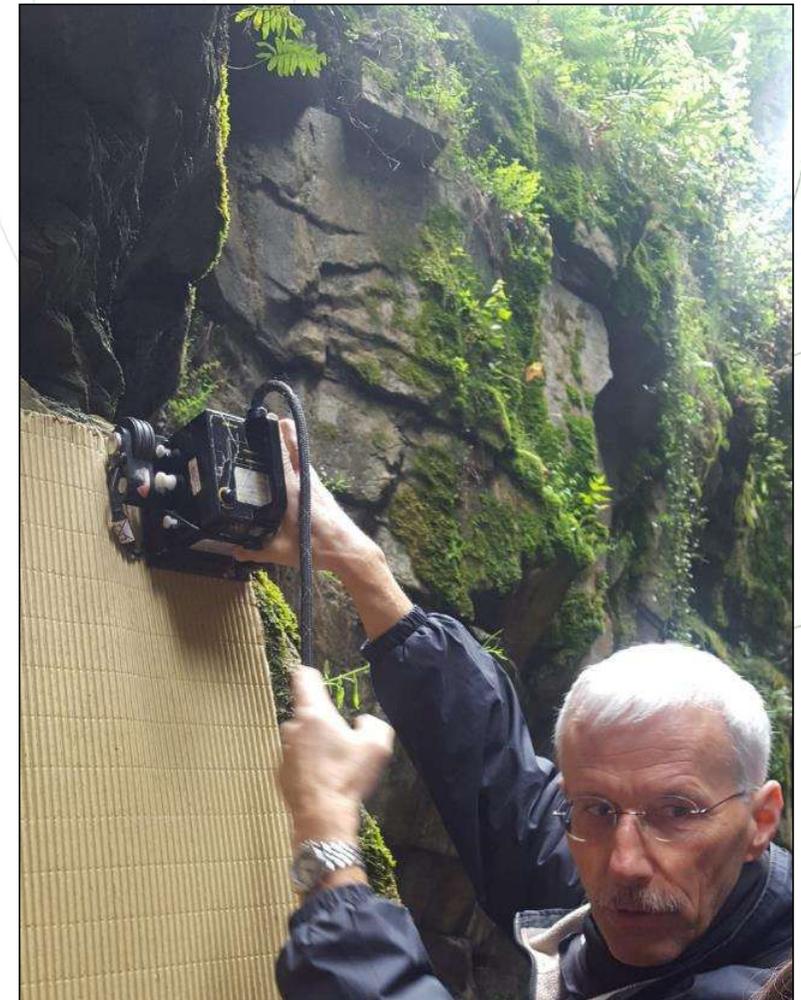
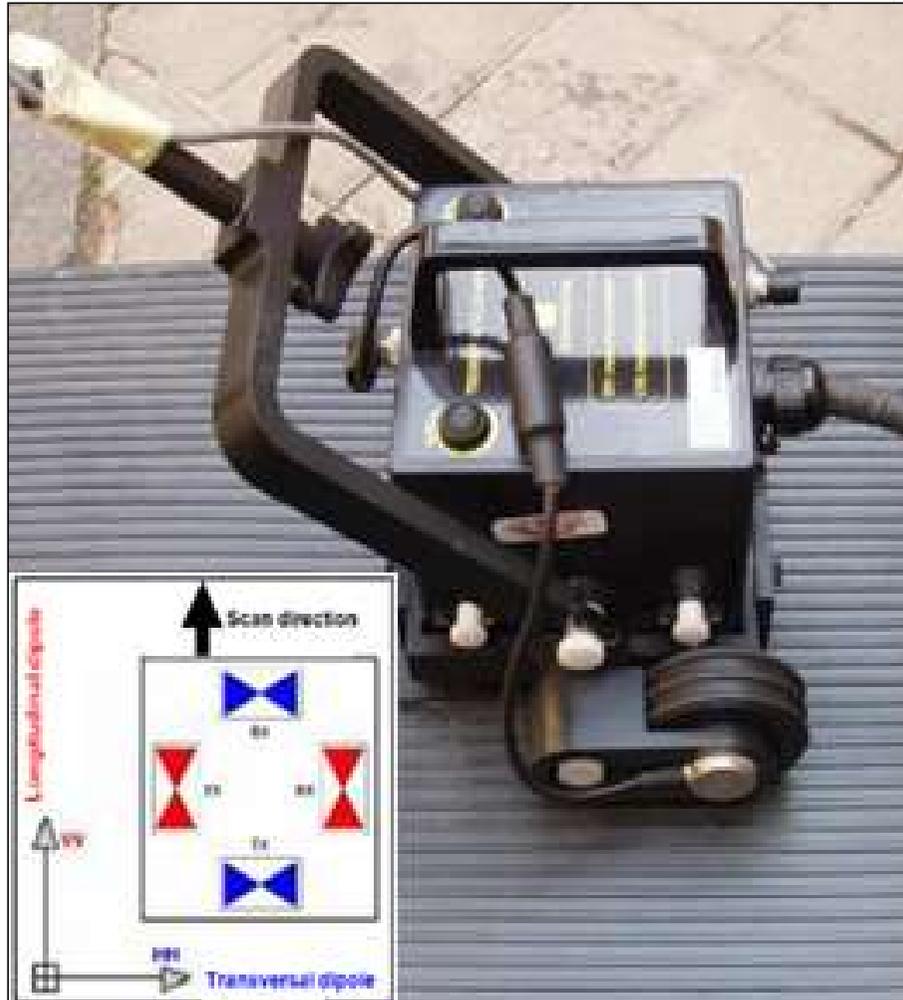
Data acquisition

**GSSI system
(1.5GHz)**



Data acquisition

IDS bipolar antenna
(2GHz)



RAMAC system (borehole antennas)



MALÅ 100MHz Slimhole Borehole Antenna:

Dimensions:

Tx: 189 cm including batteries. Diameter: 40 mm

Weight: 3.3 kg

Rx: 176 cm including batteries. Diameter: 40 mm

Weight: 3.6 kg

The MALÅ 250MHz Borehole Antenna:

Dimensions:

Tx: 129 cm including batteries. Diameter: 48 mm

Weight: 4.75 kg

Rx: 129 cm including batteries. Diameter: 48 mm

Weight: 4.75 kg

Data acquisition

Antenna array systems



Data acquisition

Antenna array systems

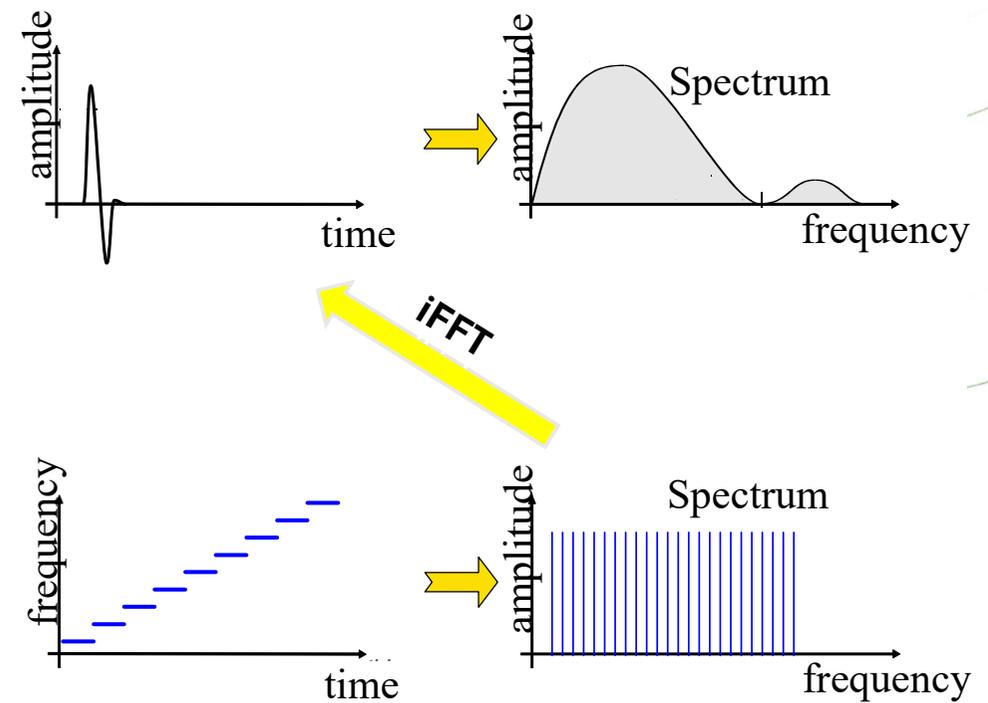


Data acquisition

Antenna array systems



Stepped frequency system from 3D-radar

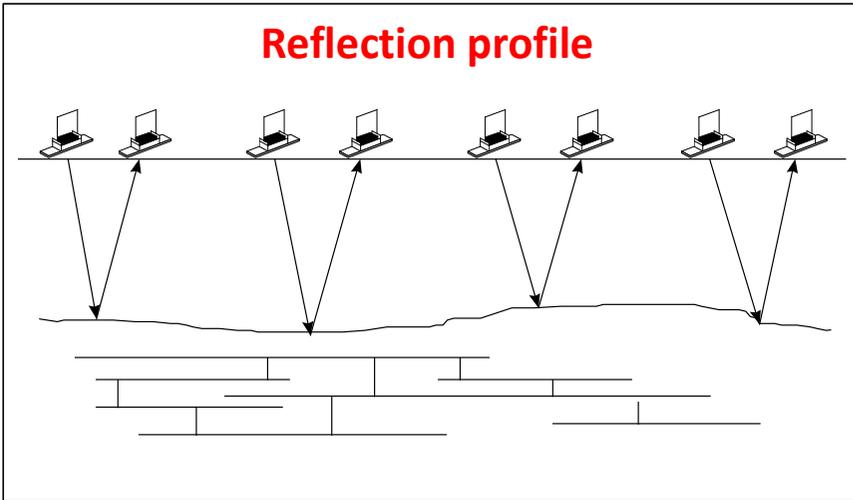


Data acquisition

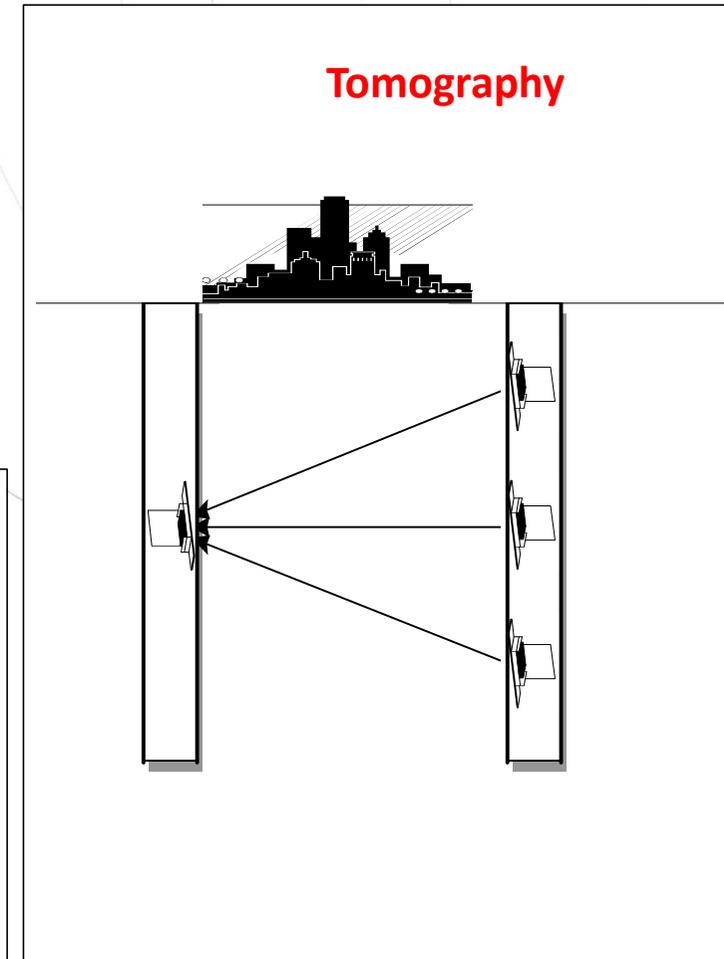


Data acquisition

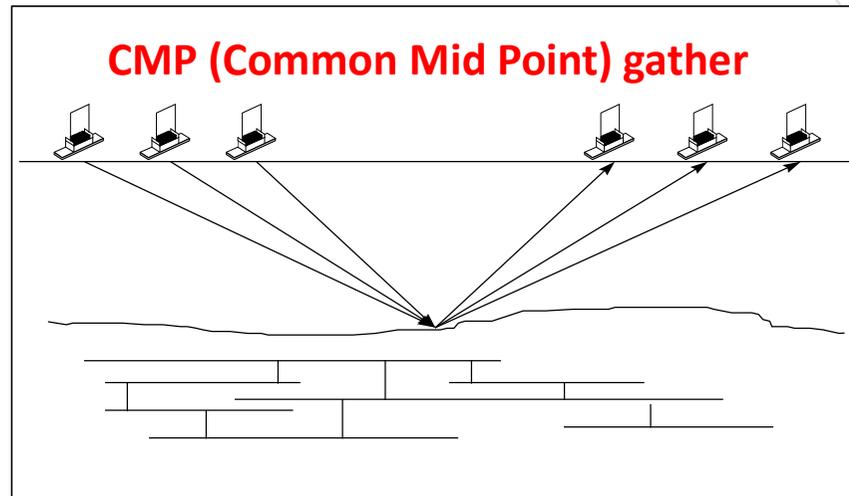
Reflection profile



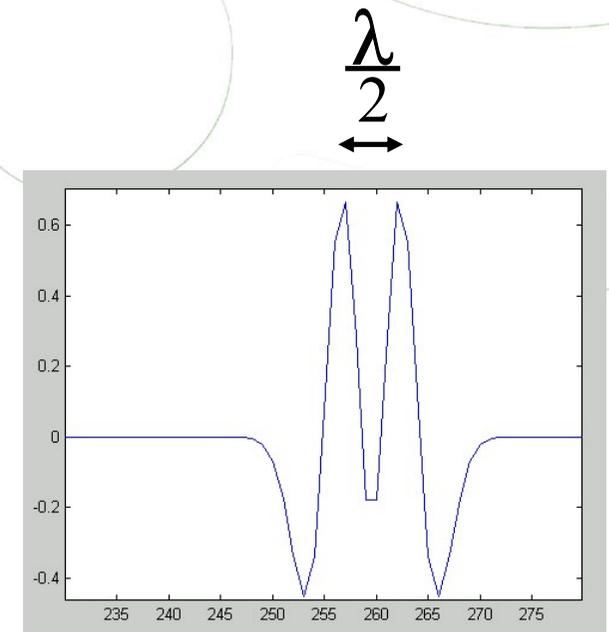
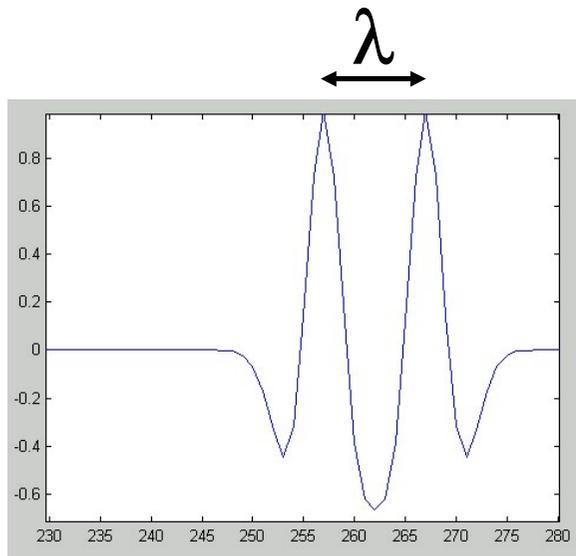
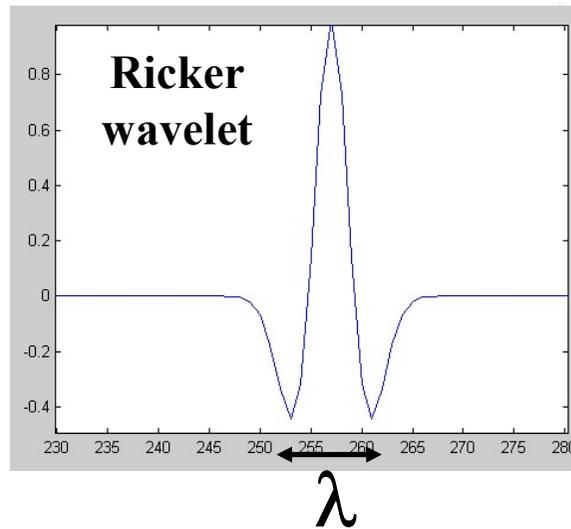
Tomography



CMP (Common Mid Point) gather

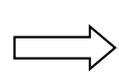
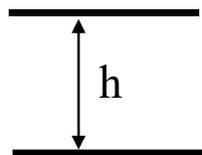
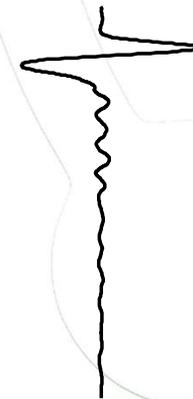
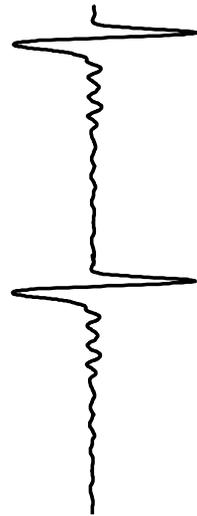


Frequency vs. Resolution

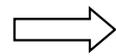


Frequency vs. Resolution

Vertical resolution



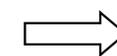
$$2h = \frac{\lambda}{2}$$



$$h = \frac{\lambda}{4}$$

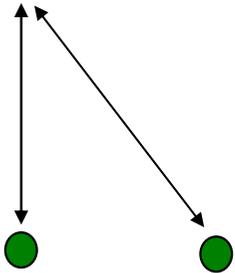
since $\lambda = \frac{v}{f}$

to obtain h as vertical resolution at any depth

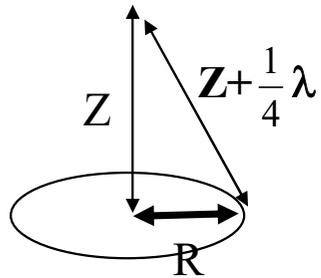
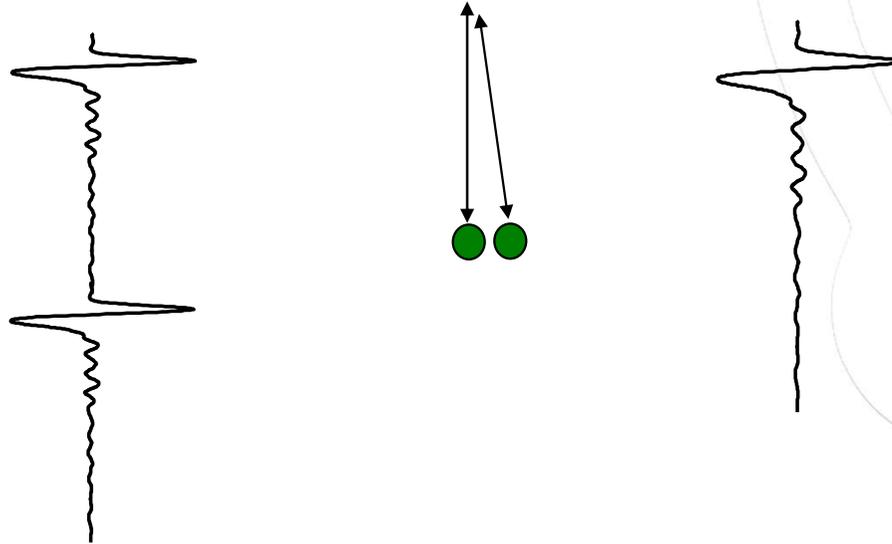


$$f = \frac{v}{4h}$$

Frequency vs. Resolution



Lateral resolution



$$R = \sqrt{\frac{\lambda^2}{16} + \frac{Z\lambda}{2}} \quad \rightarrow \quad \text{for } Z \gg \lambda \quad \rightarrow \quad R = \sqrt{\frac{Z\lambda}{2}}$$

To obtain R as lateral resolution at depth Z ,

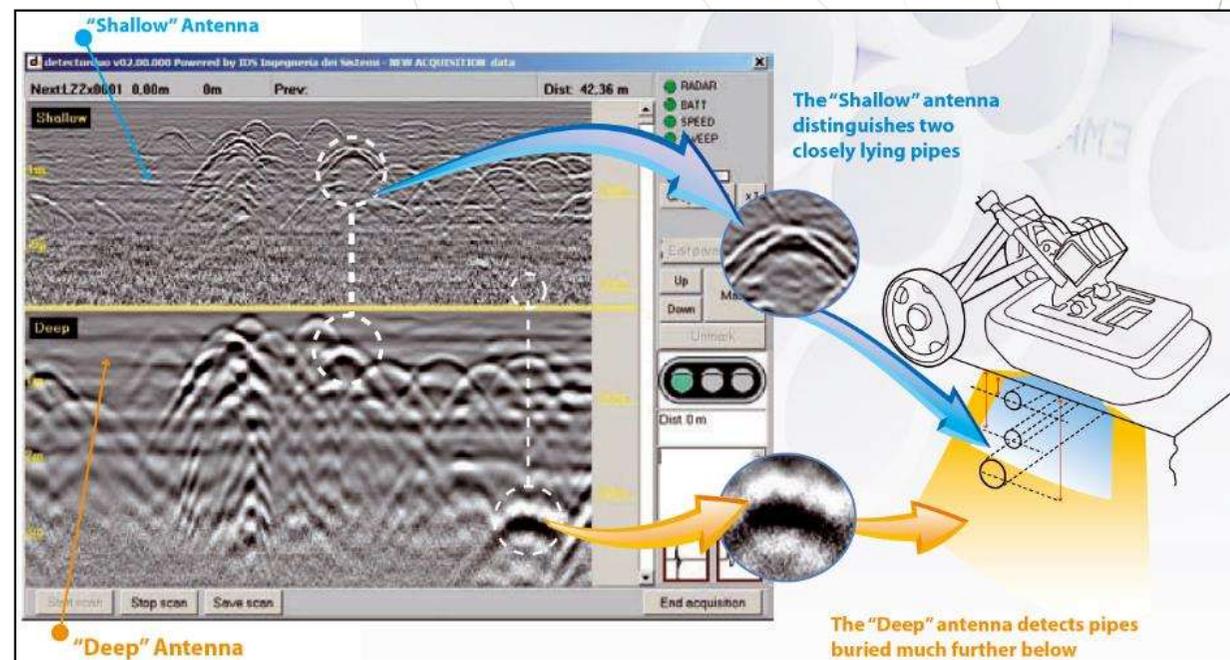
$$f = \frac{Zv}{2R^2}$$

Frequency vs. Penetration

Since absorption is proportional to frequency:

Penetration (m)	Frequency (MHz)
0.5-1.0	1000
1.0-2.0	500
2.0-10	200
5-15	100
10-30	50
30-50	25
50-100	10

Advantage of Multi-frequency antennas



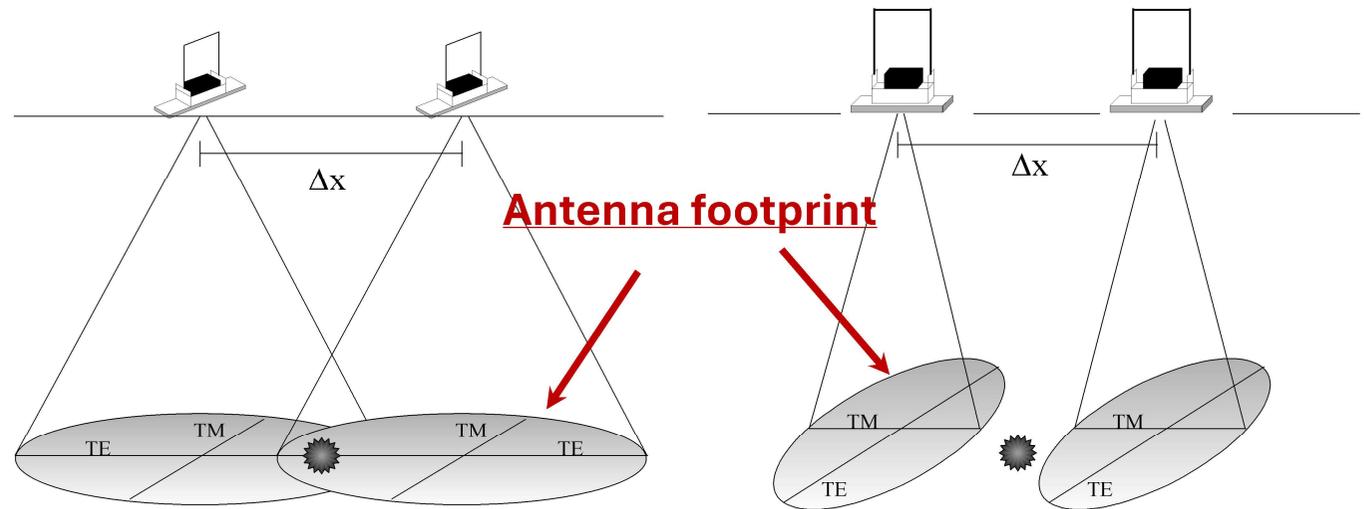
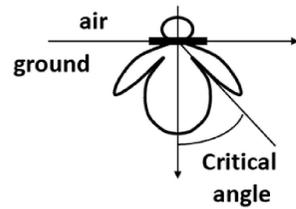
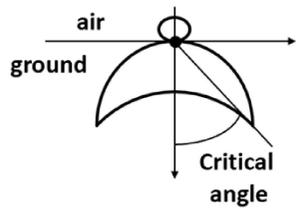
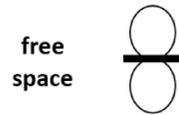
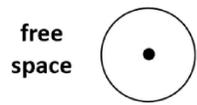
Detector DUO (IDS)

Antenna directivity

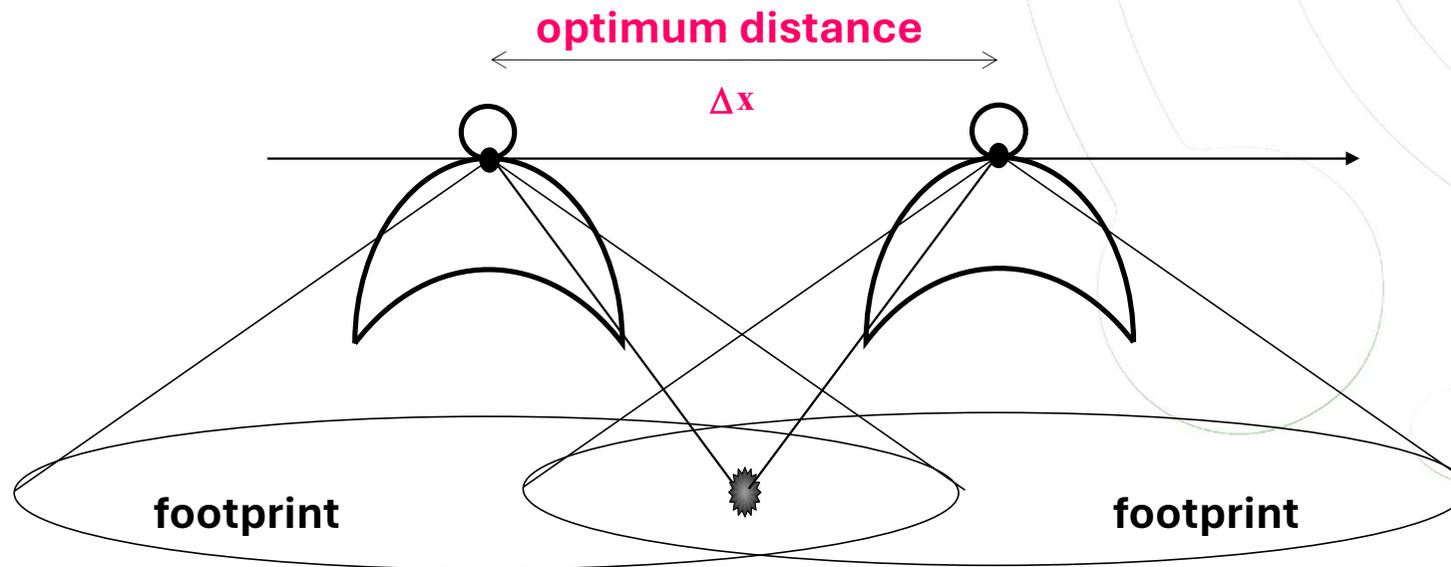
Directivity functions

TE pattern

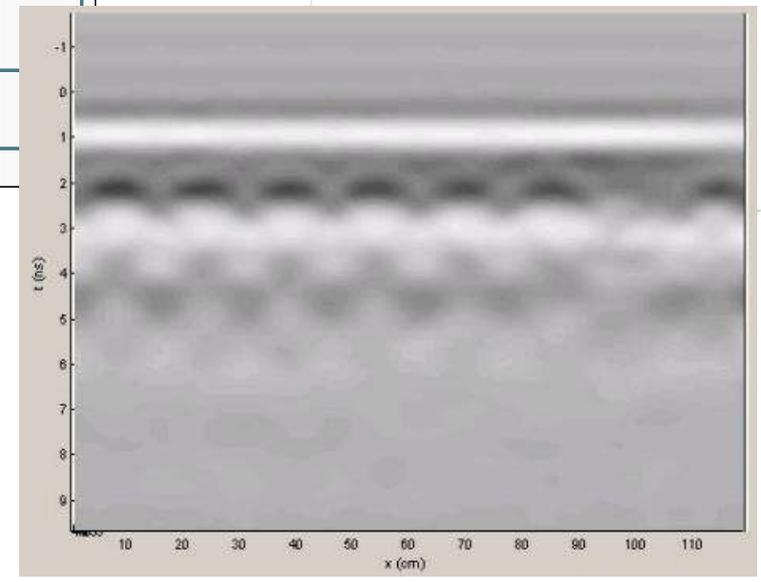
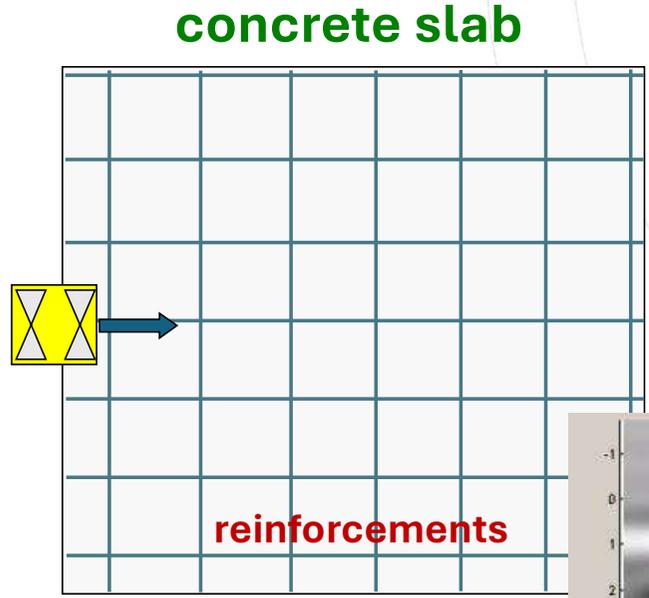
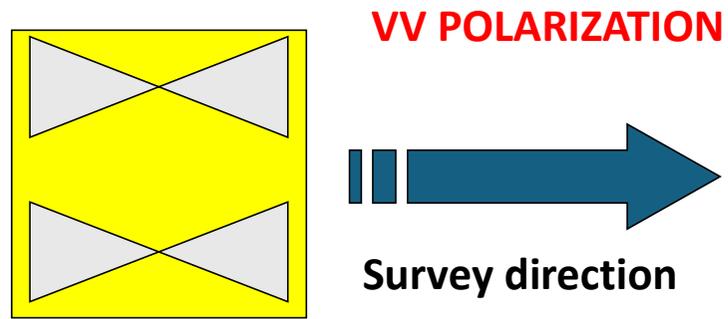
TM pattern



Antenna directivity

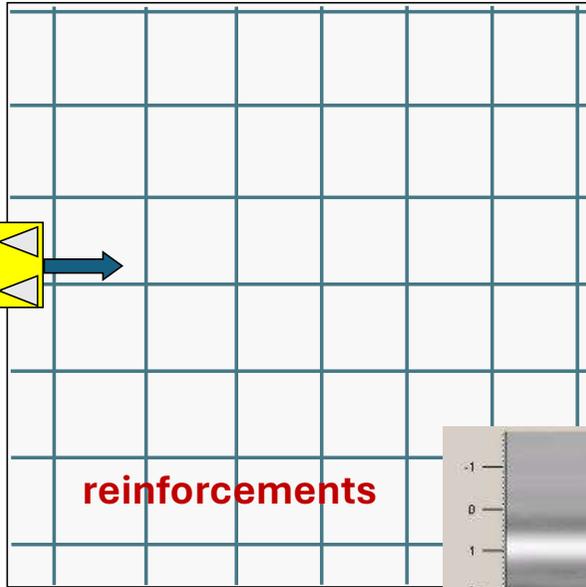


Polarization

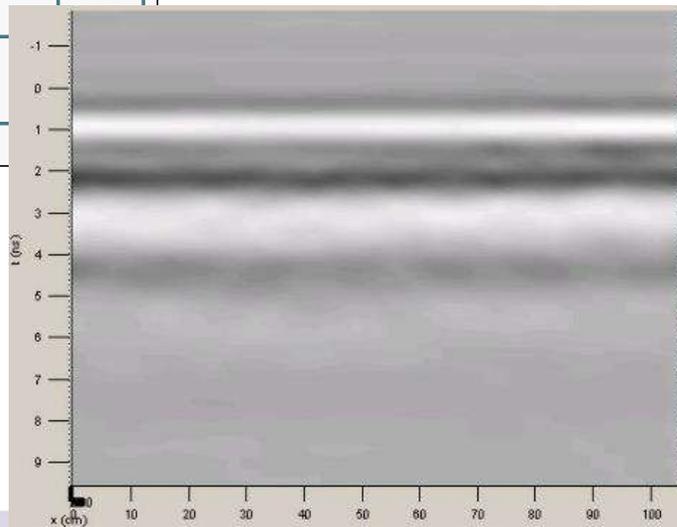


Polarization

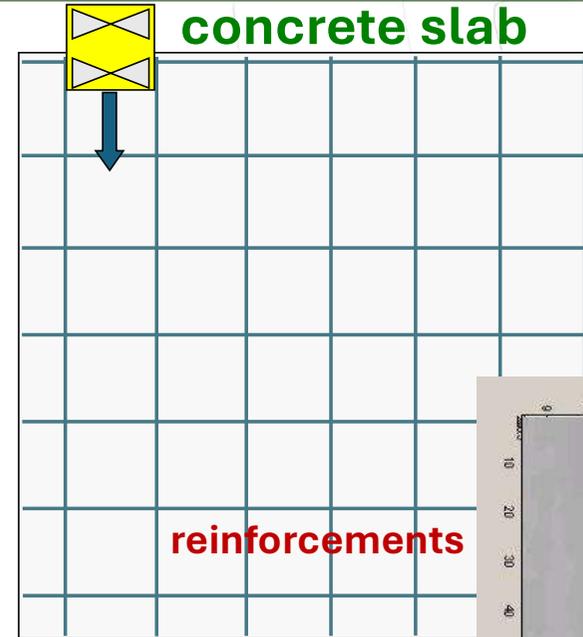
concrete slab



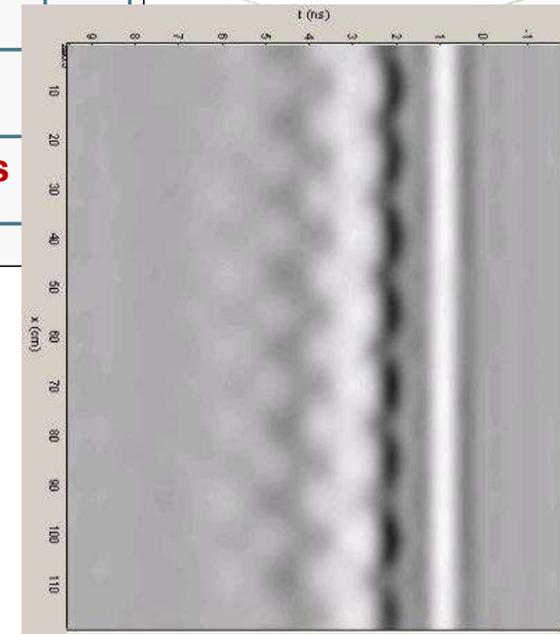
reinforcements



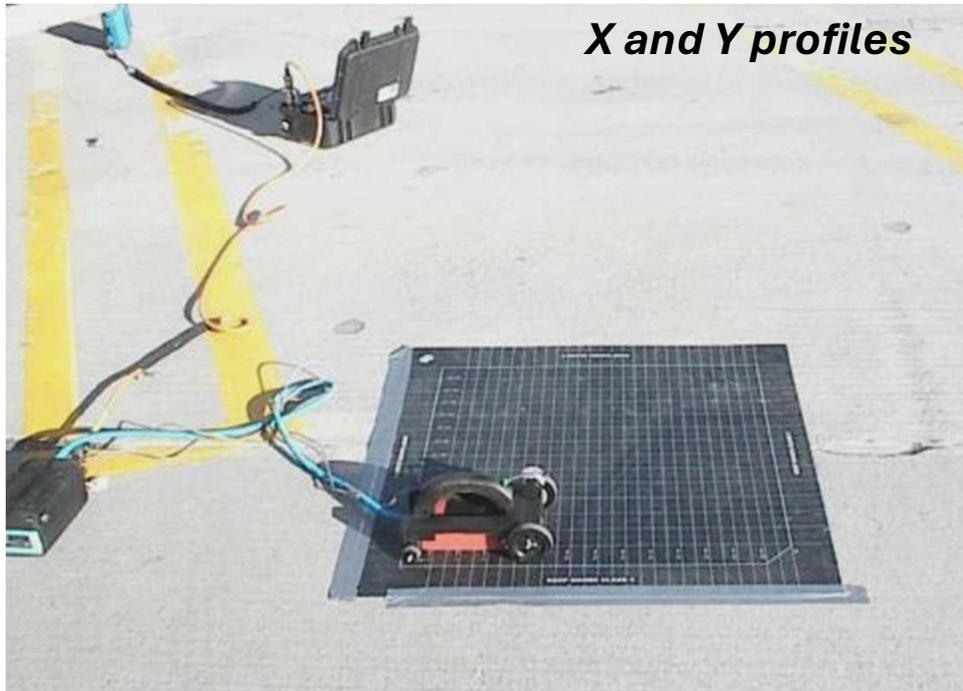
concrete slab



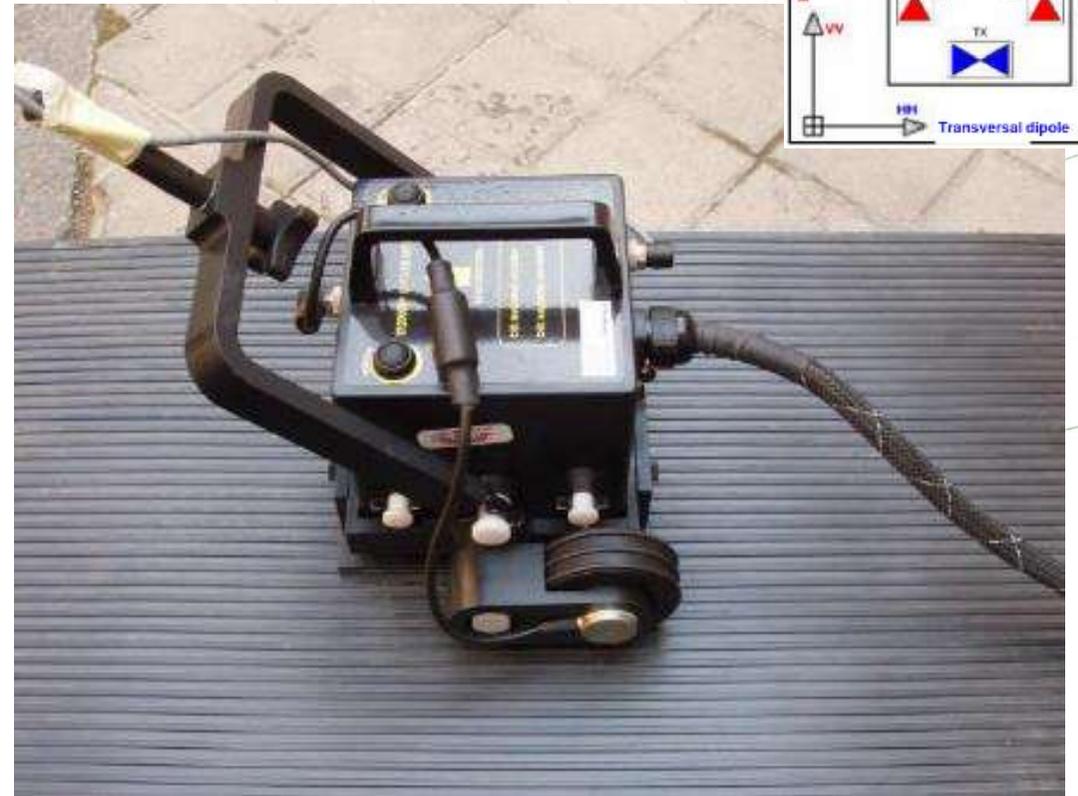
reinforcements



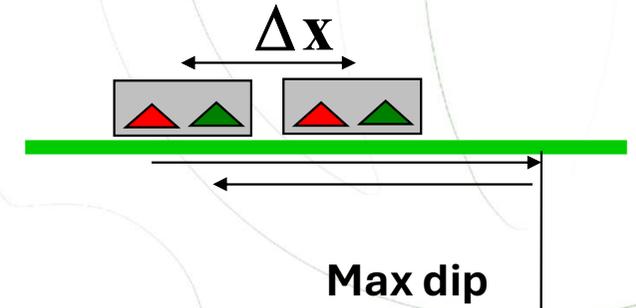
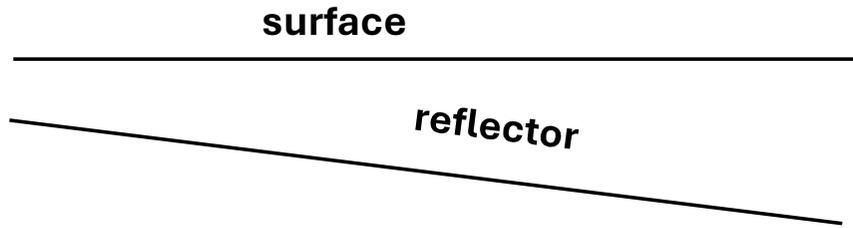
Polarization



X profiles

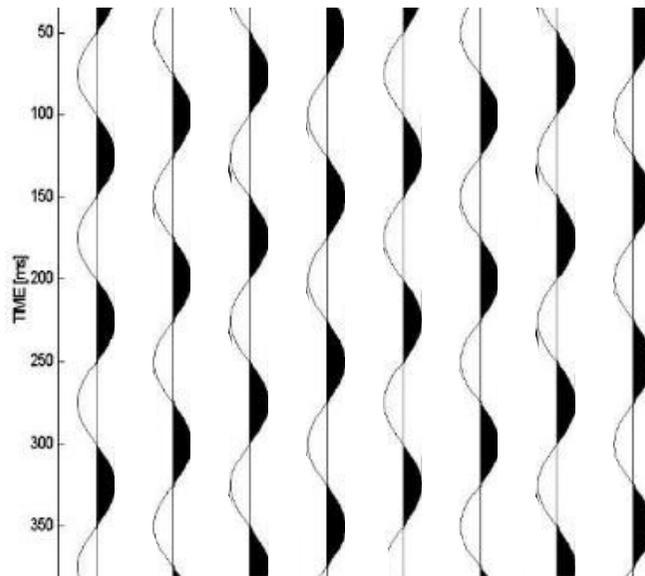
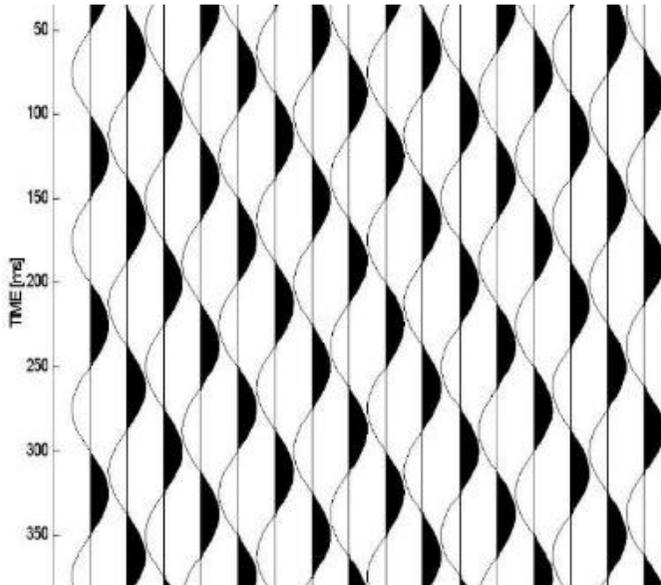


Spatial aliasing



no aliasing

with aliasing



$$\Delta x < \frac{1}{4} \lambda_{\min}$$

$$\Delta x < \frac{1}{4} V / F_{\max}$$

$$\Delta x < \frac{1}{6} V / F$$

Spatial positioning

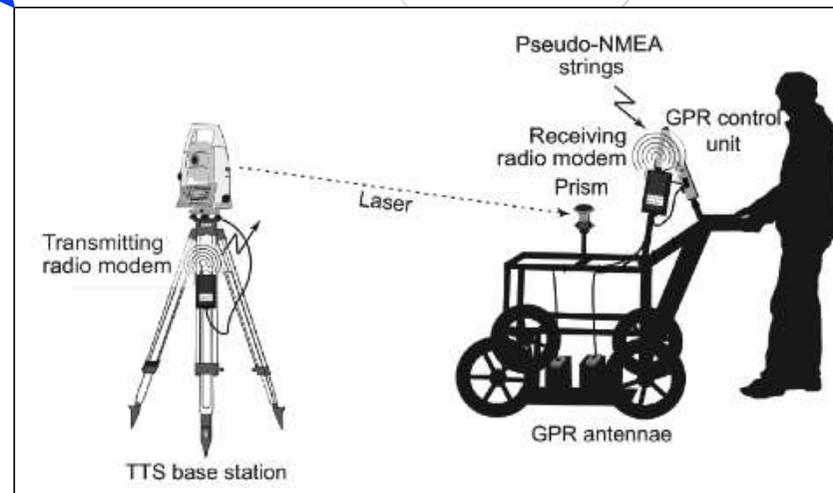
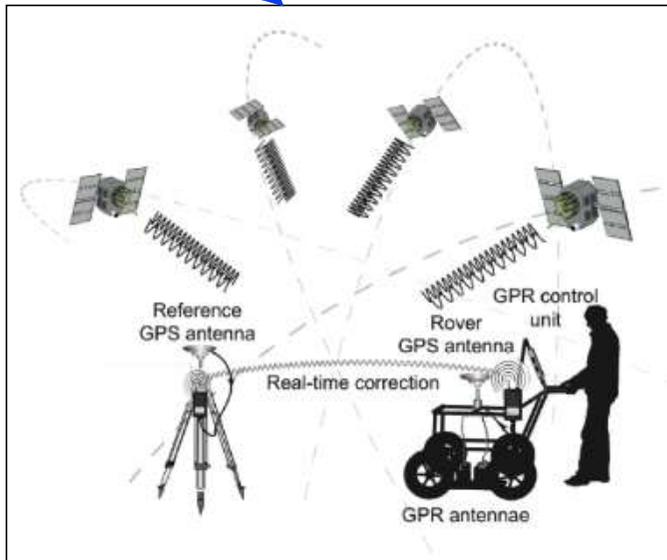
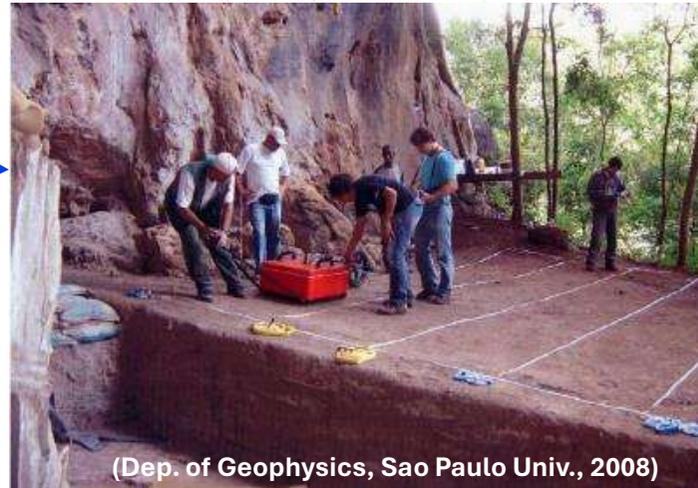
2D survey

- fixed step positioning
- fiducial markers
- odometer

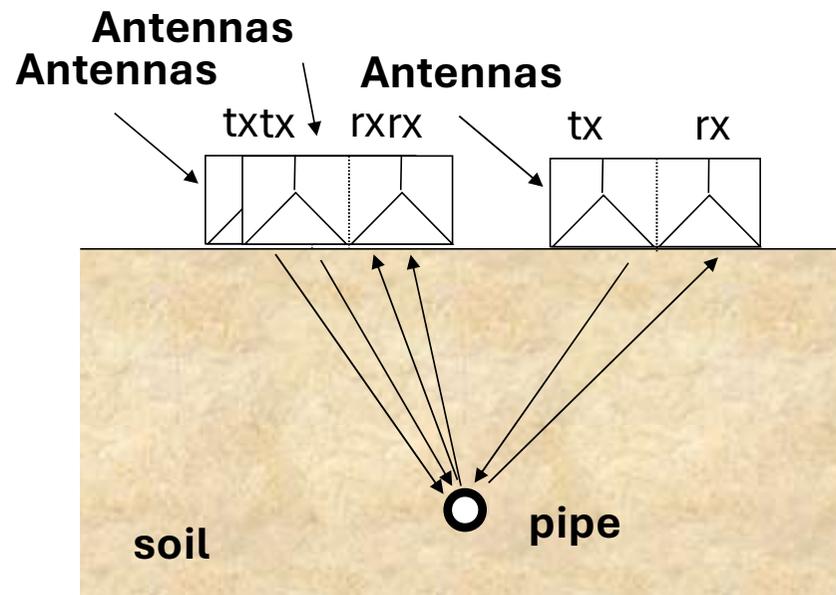


3D survey

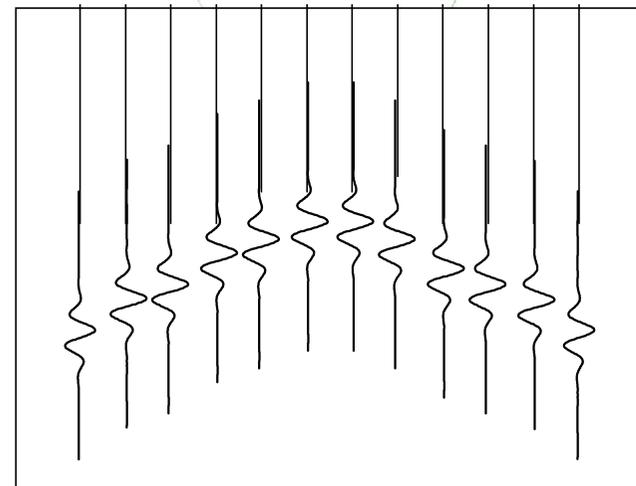
- tapes or ropes
- advanced 3D systems (GPS, Self-Tracking Total Station)



Diffractions



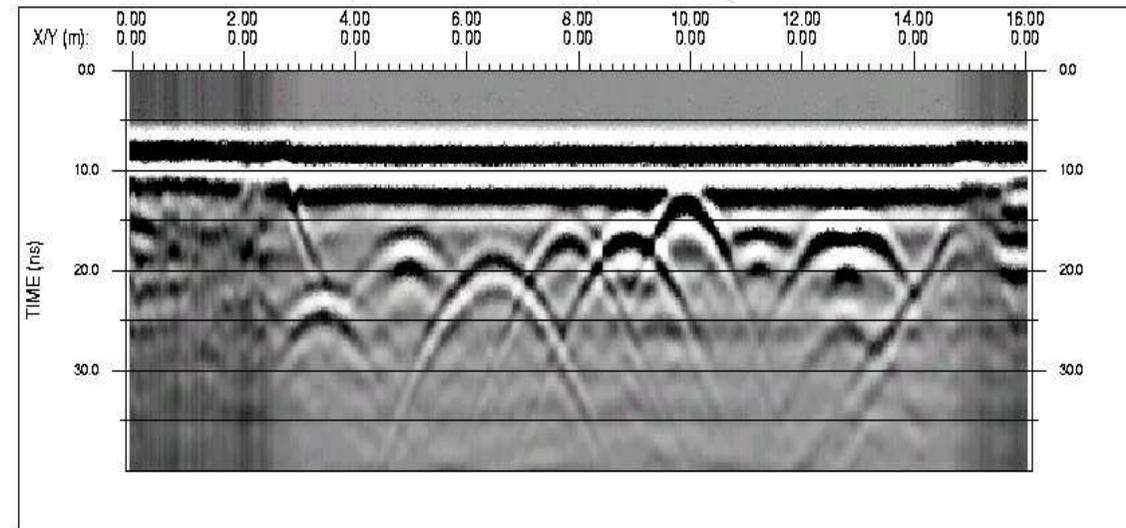
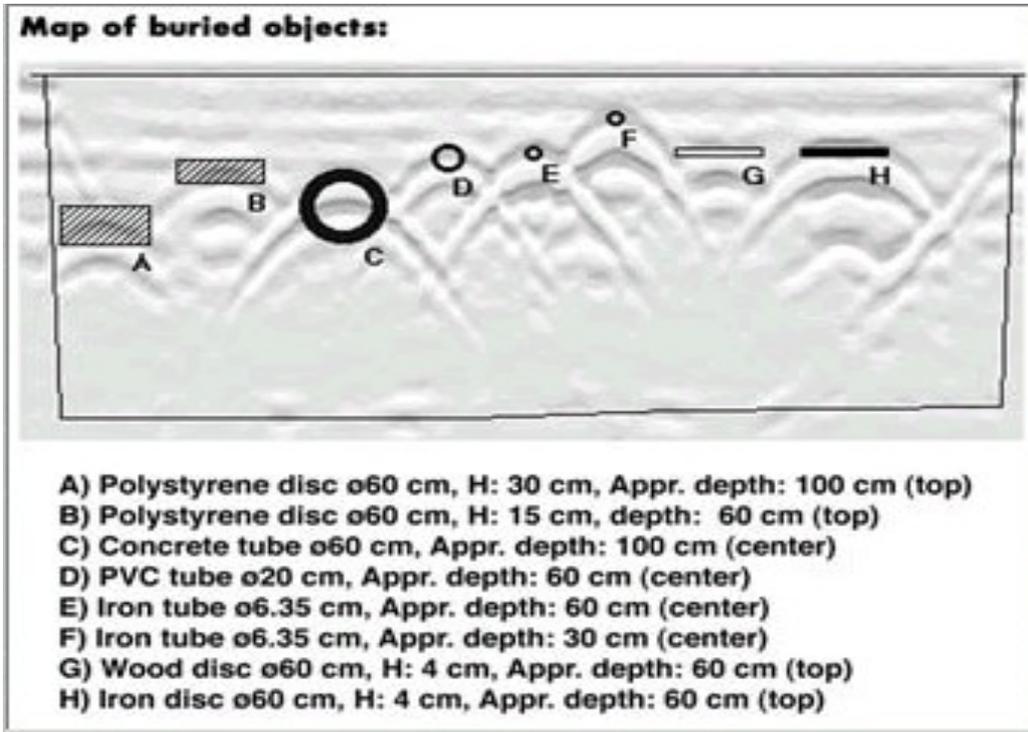
Diffraction generated by the pipe



Data analysis and interpretation

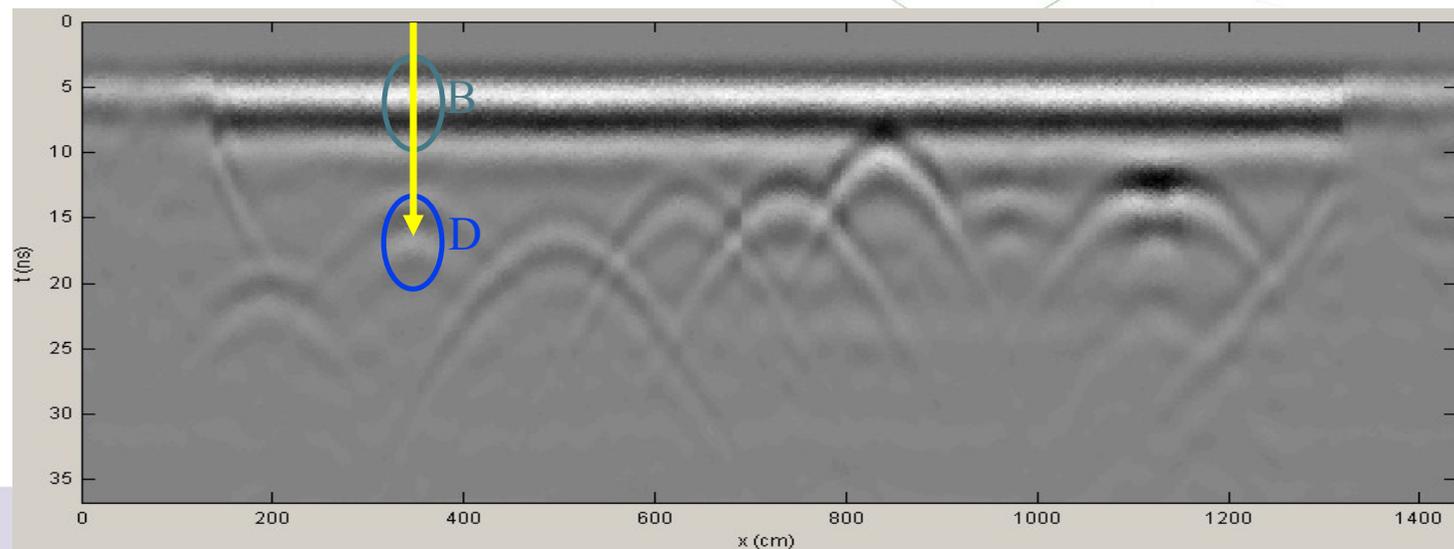
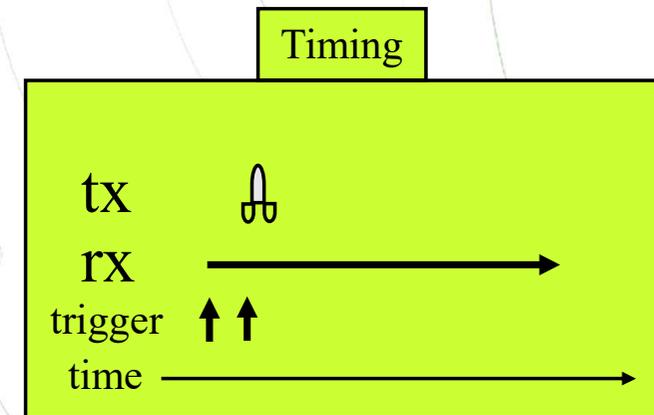
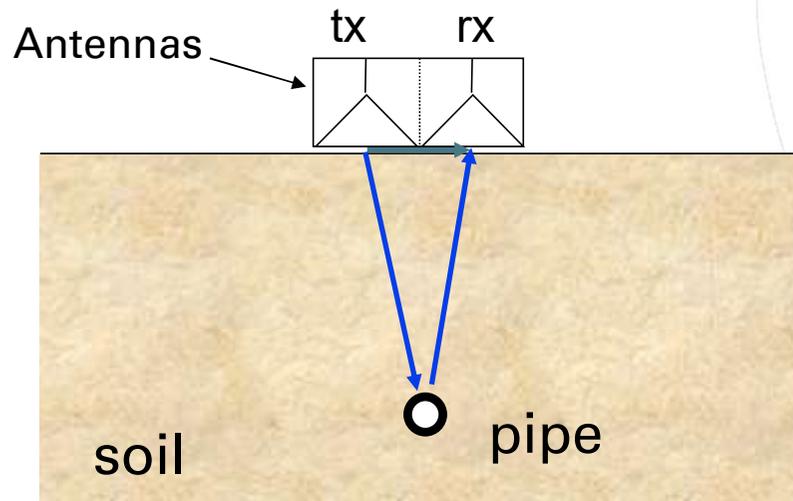
ISMES test site

Raw data (RAMAC 400 MHz)



Data analysis and interpretation

Time calibration



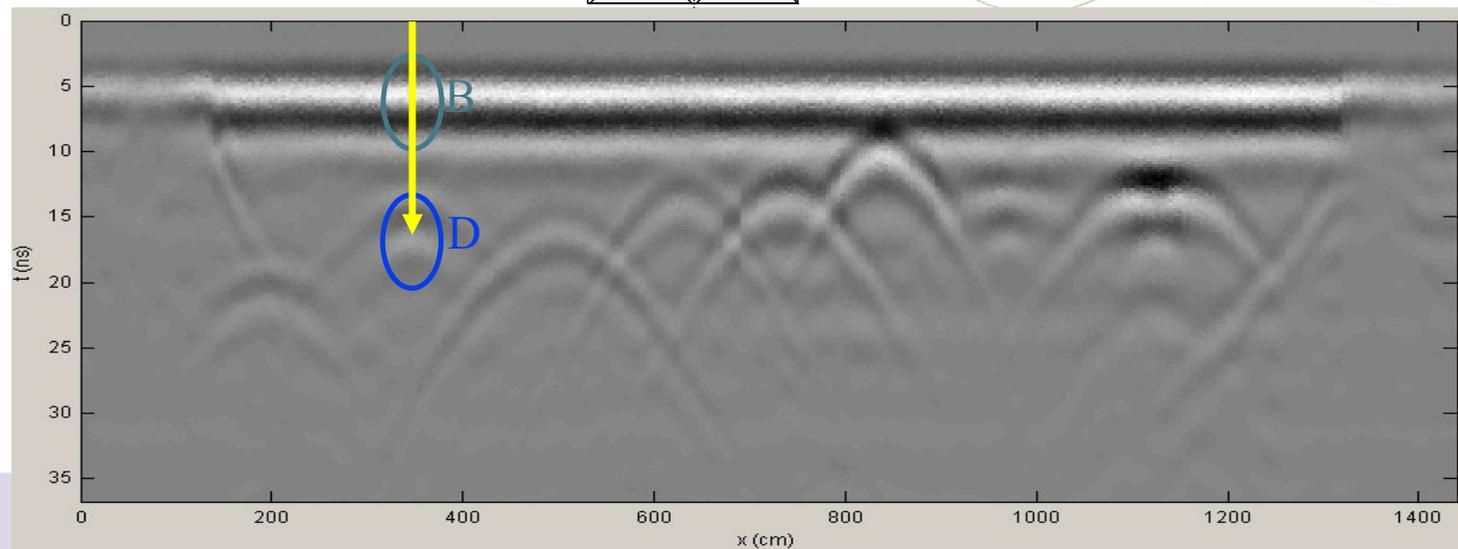
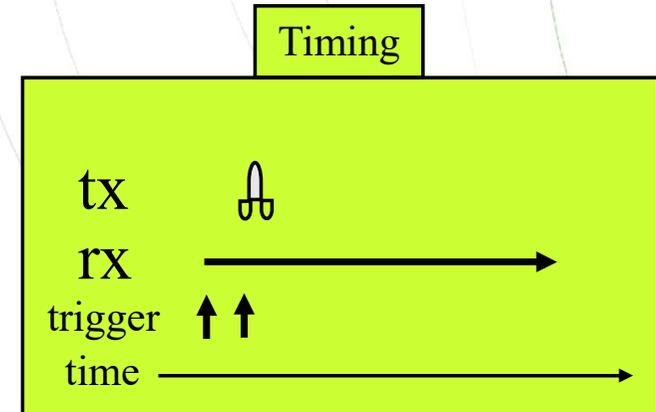
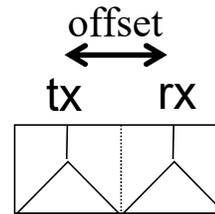
Data analysis and interpretation

Time calibration

- Time calibration moves the time scale so that zero time occurs when the tx is triggered.
- This time is obtained from the data by picking event B and

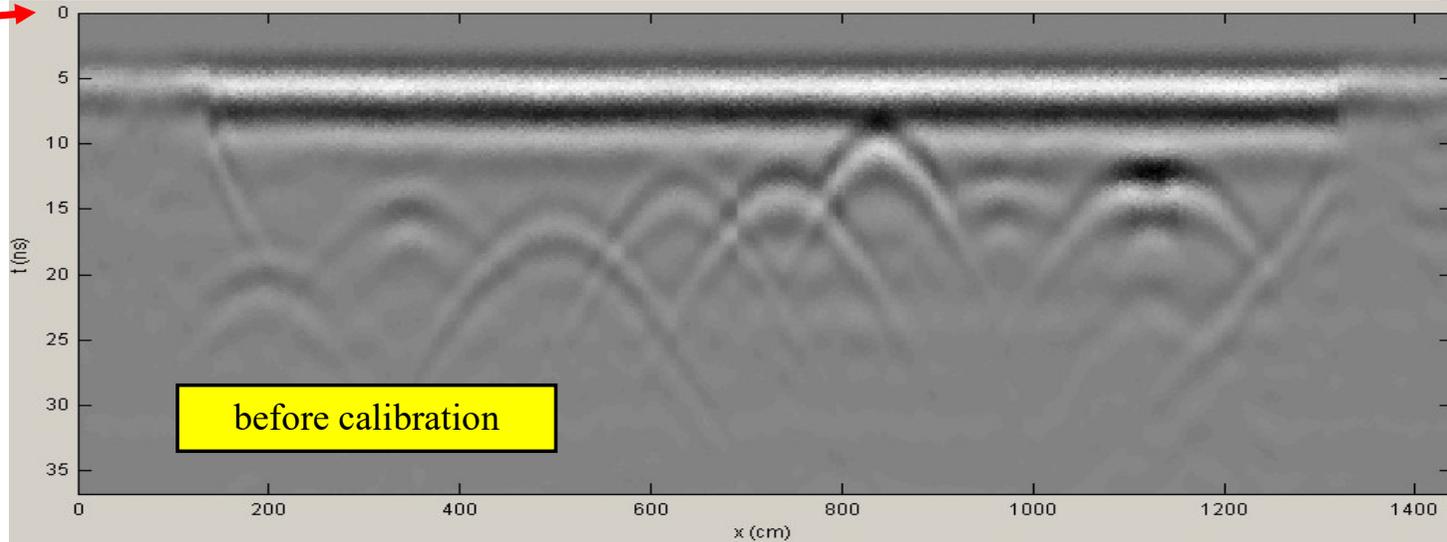
$$t_0 = t_B - \frac{\text{offset}}{c}$$

with $c = 30\text{cm/ns}$

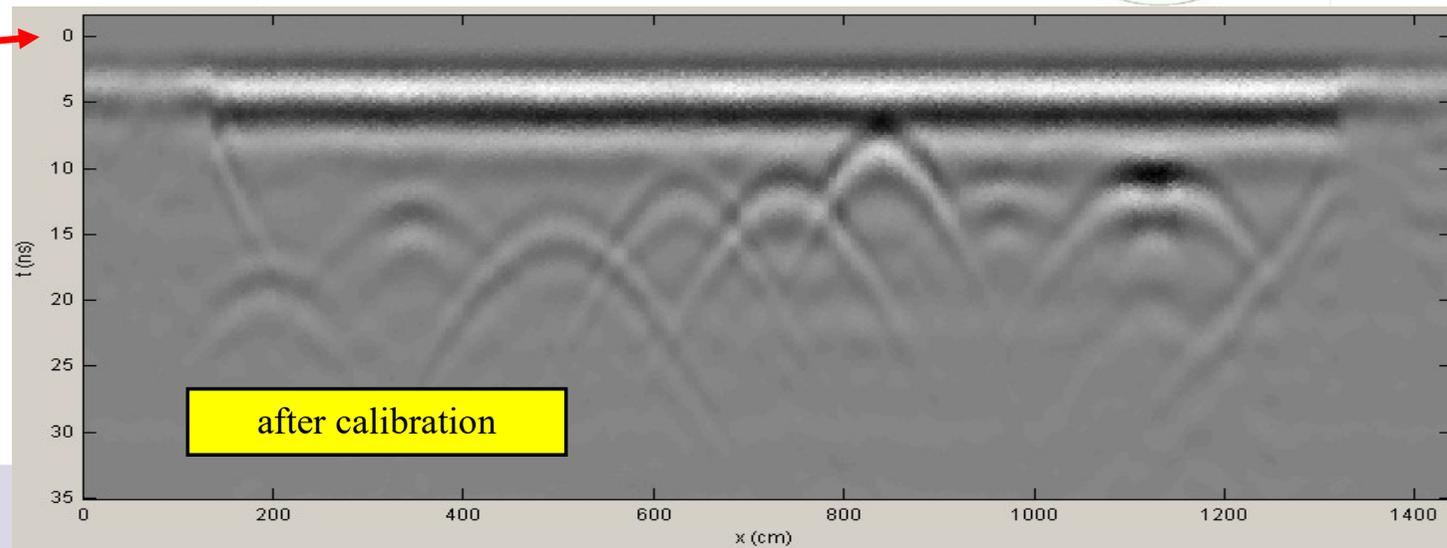


Data analysis and interpretation

time zero

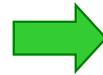


time zero



Spherical Exponential Compensation (SEC)

Because of spherical divergence



$$A(r) \propto \frac{1}{r}$$

Because of absorption

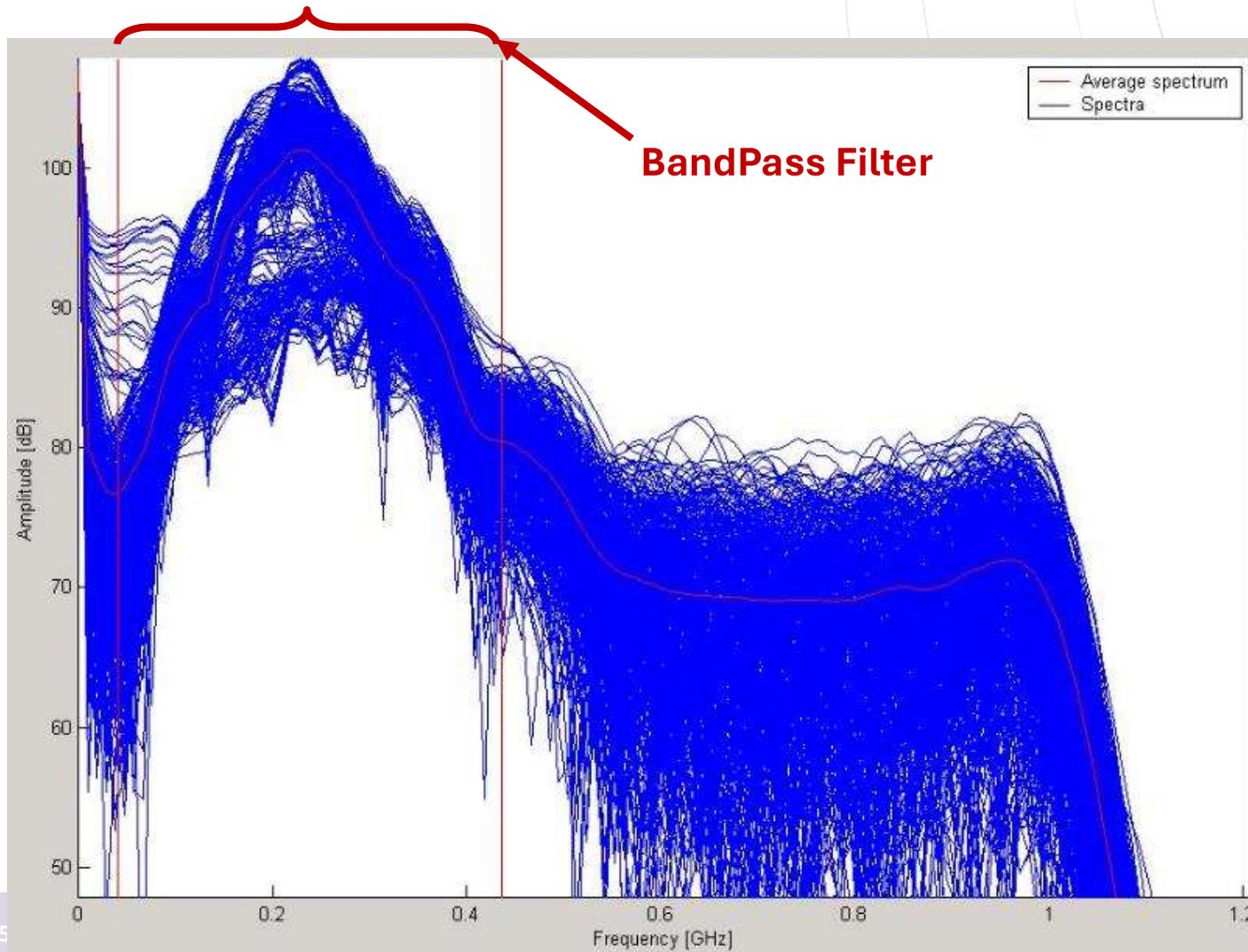


$$A(r) \propto e^{-\alpha^* r}$$

SEC compensation:

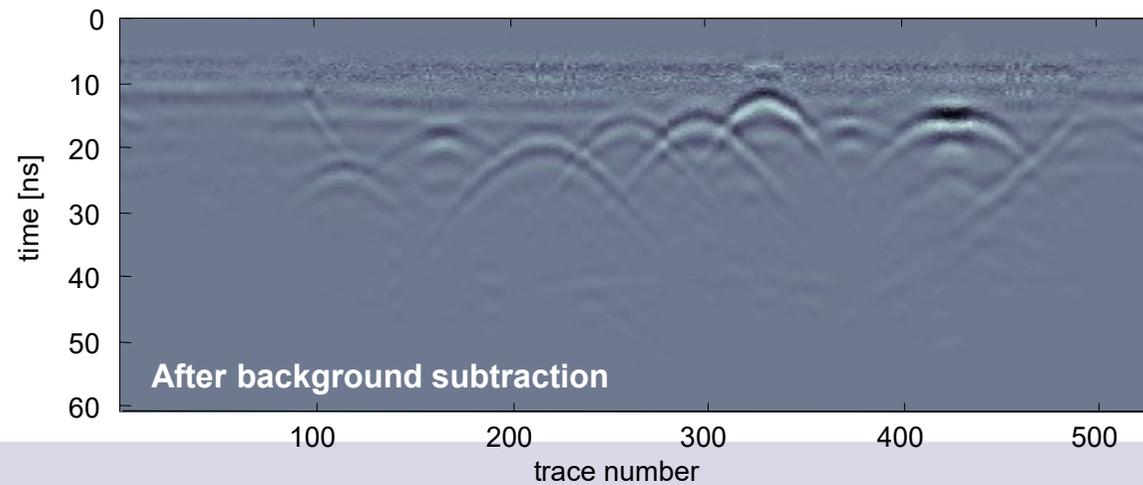
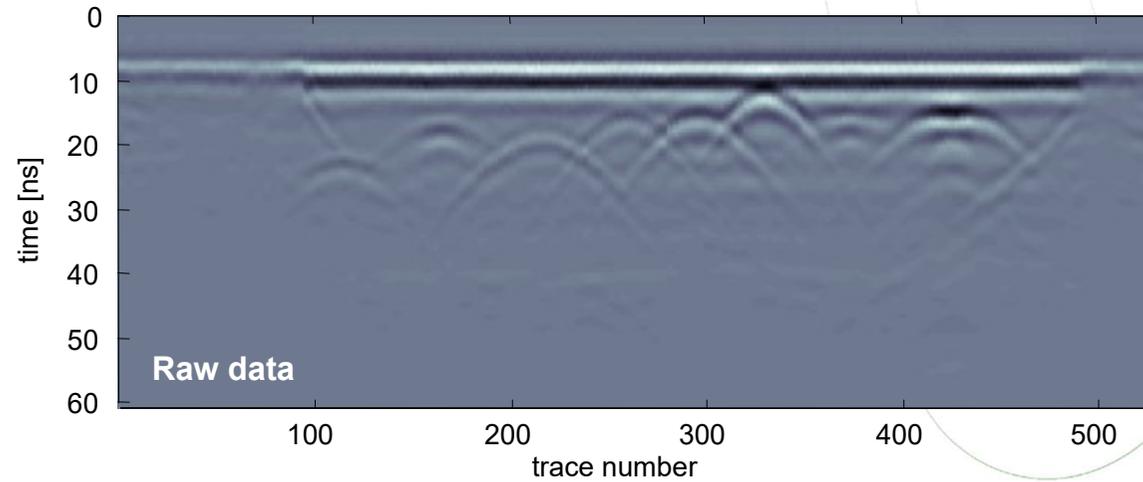
$$G(t) \propto r^* e^{\alpha^* r} \quad \longrightarrow \quad G(t) \propto v^* t^* e^{\alpha^* v^* t}$$

Data analysis and interpretation

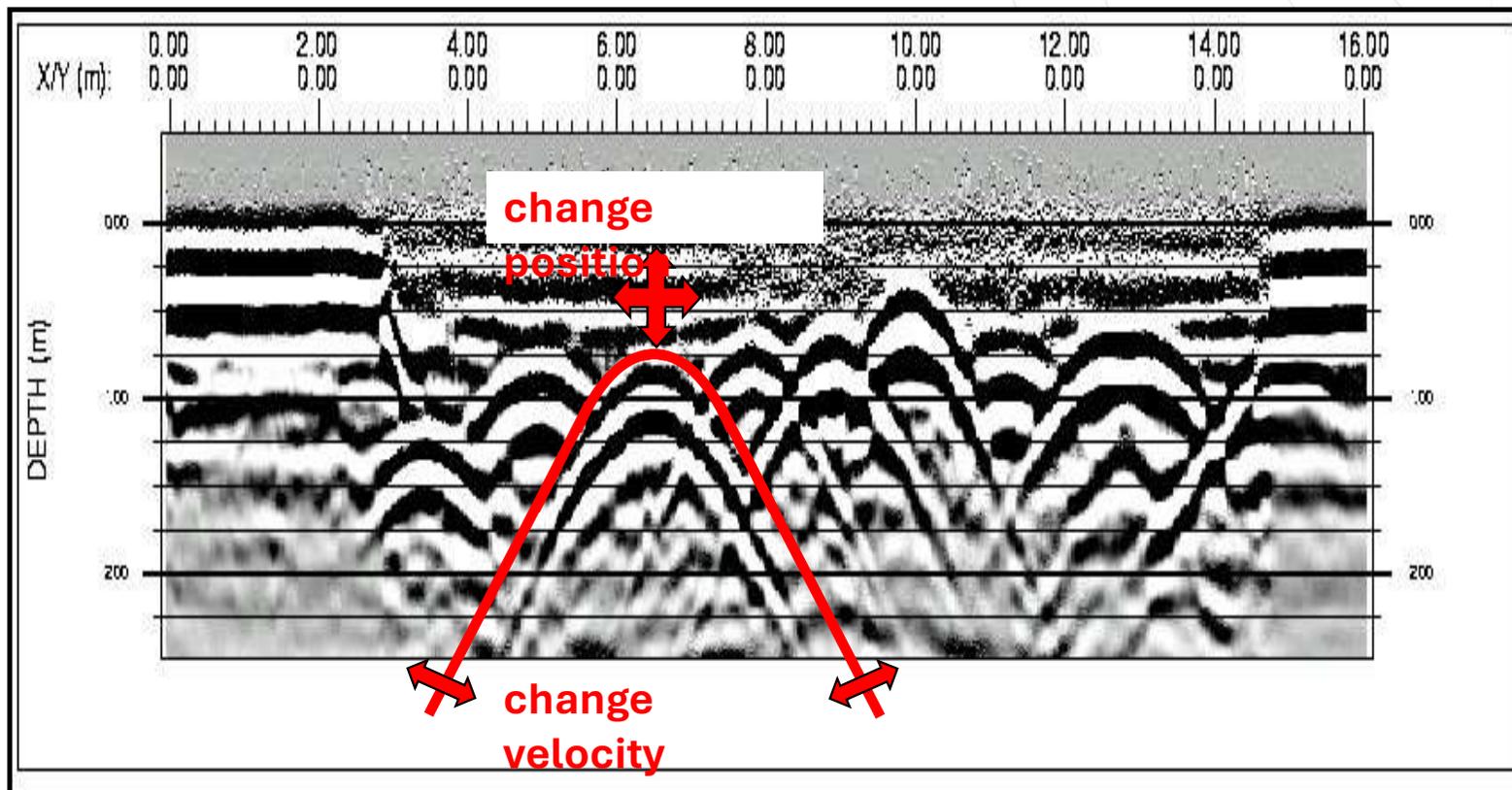


Data analysis and interpretation

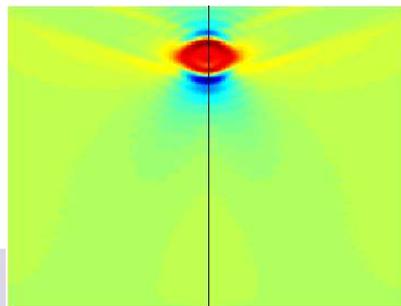
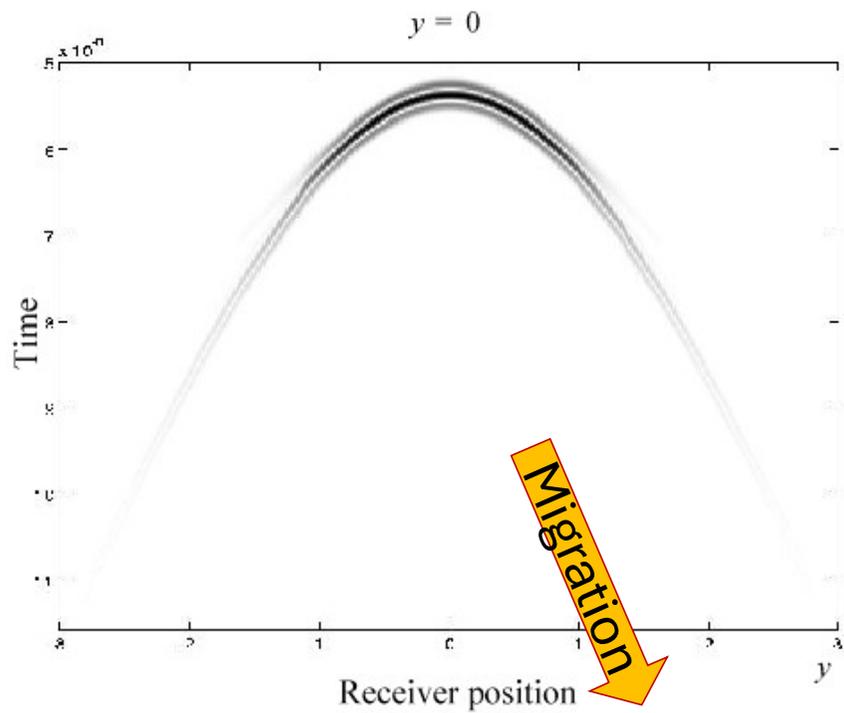
Background subtraction



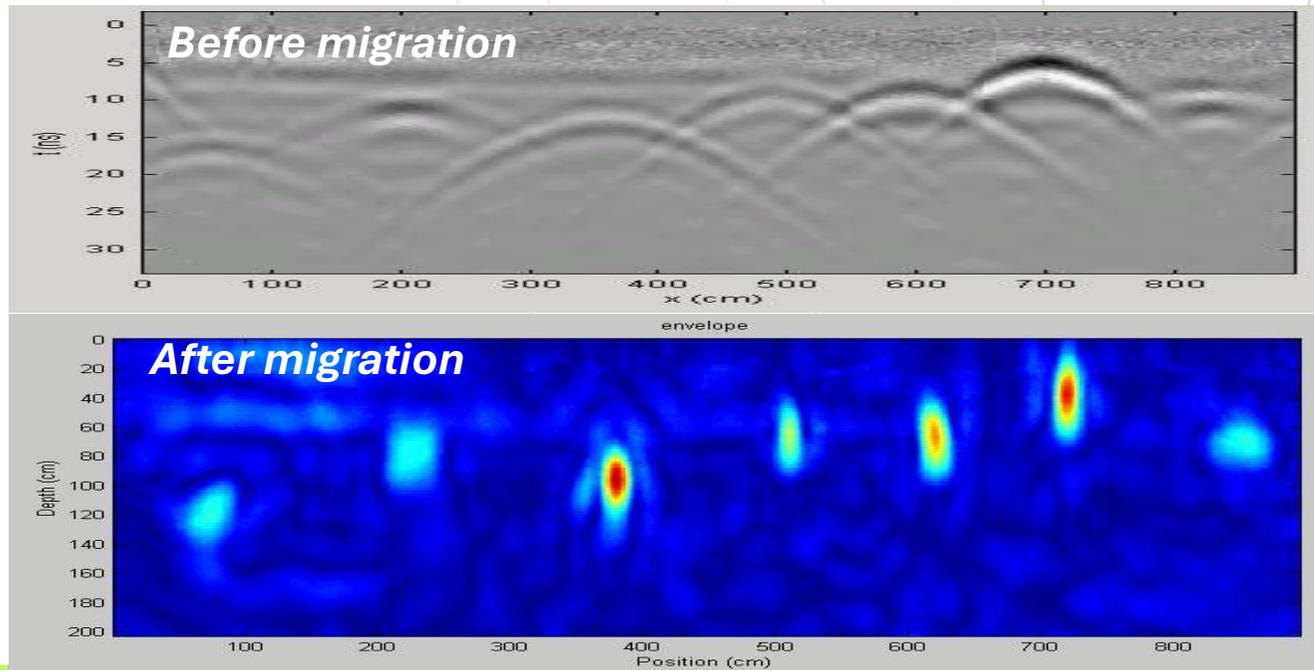
Velocity Analysis



Data analysis and interpretation



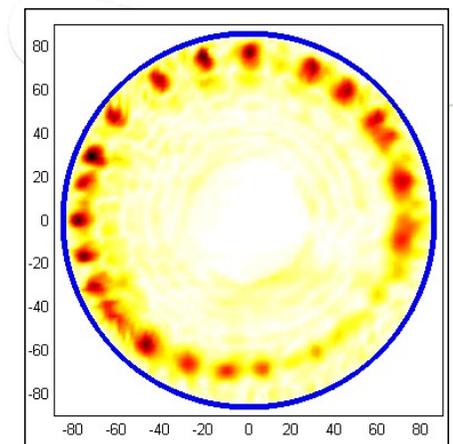
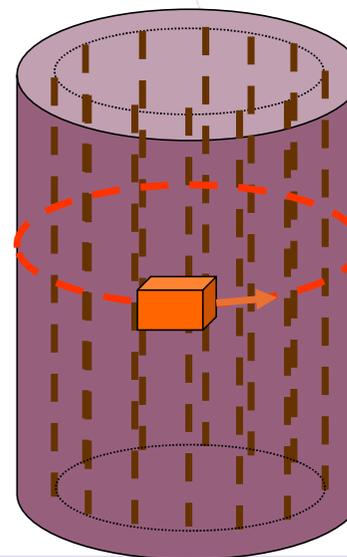
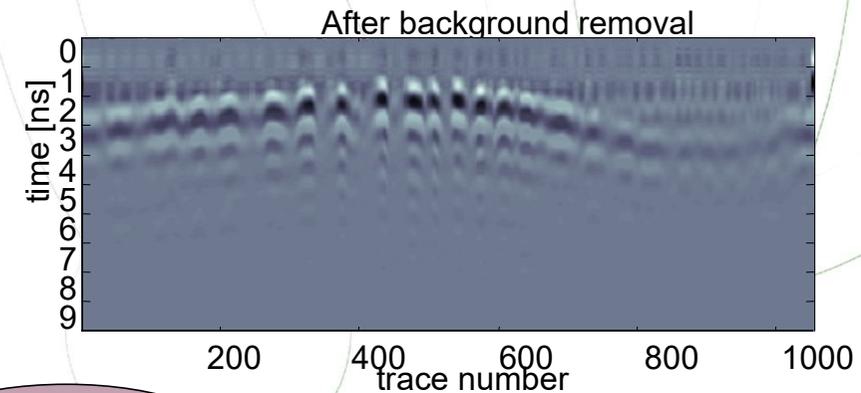
Migration



Applications

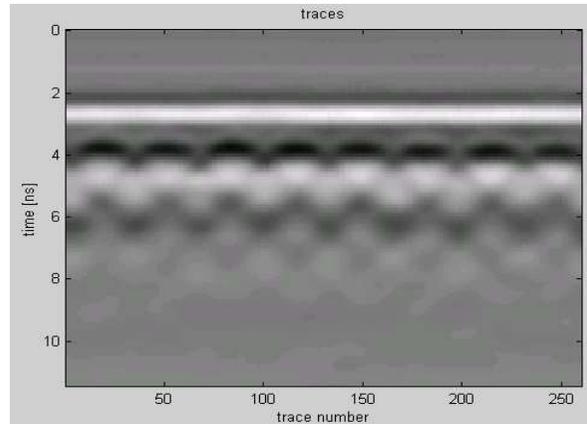
- Bedrock depth
- Water table depth
- Rock fractures
- Detection of urban subsurface utilities for safe excavations
- Highway and bridge maintenance
- Non-Destructive testing on buildings
- Glaciology
- Lake bottom mapping
- Mining
- Archaeology
- Forensic
- Humanitarian demining

Bar detection in reinforced concrete

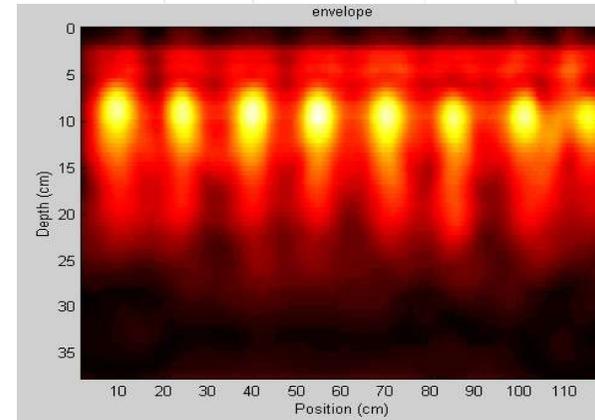


Example: bar detection in concrete

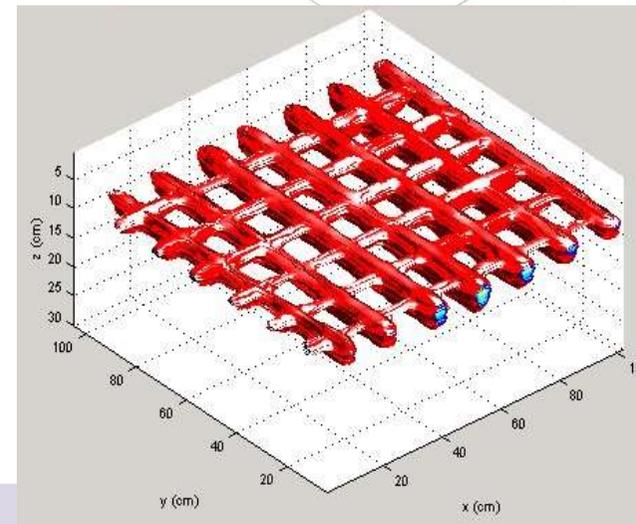
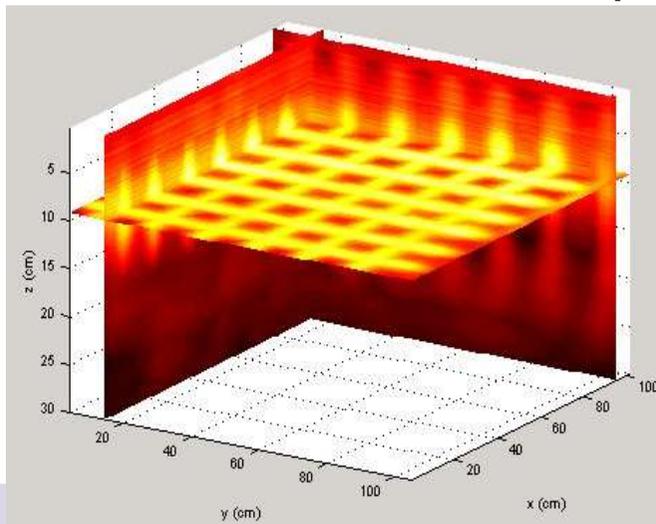
Raw data



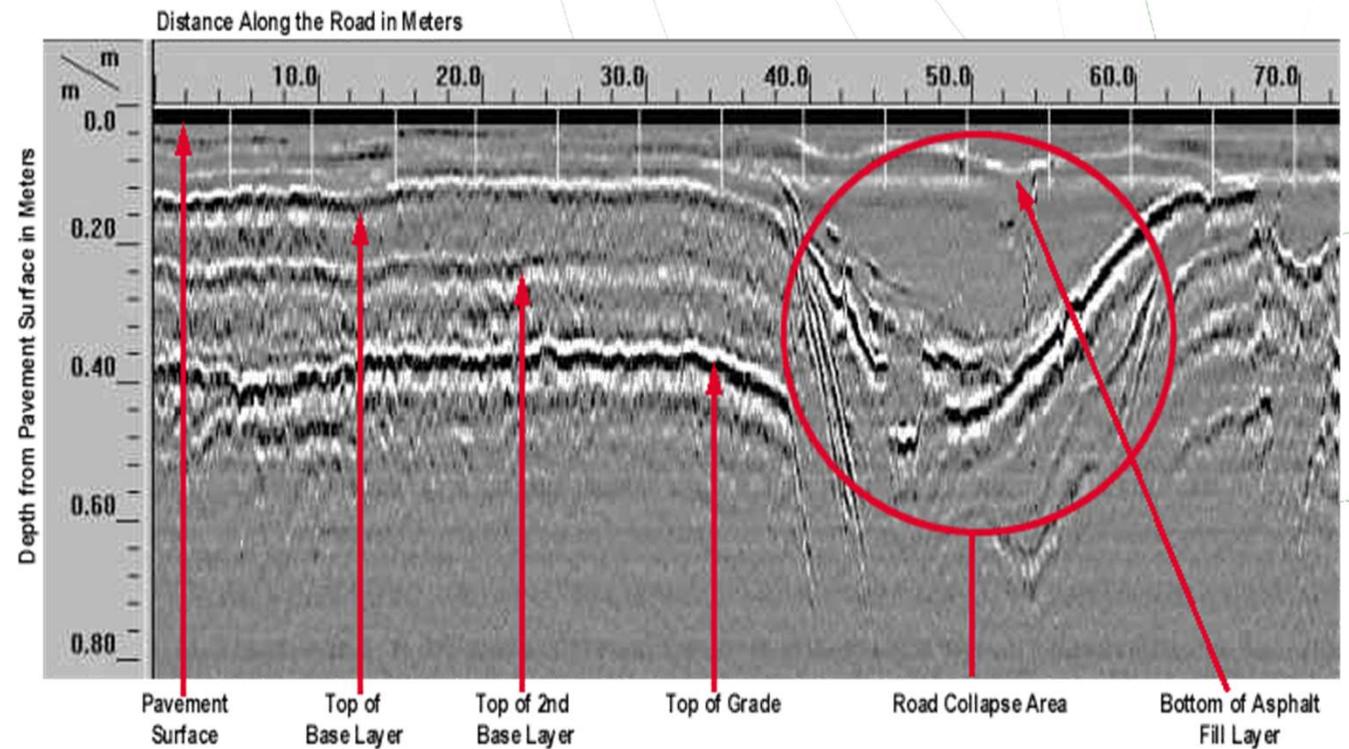
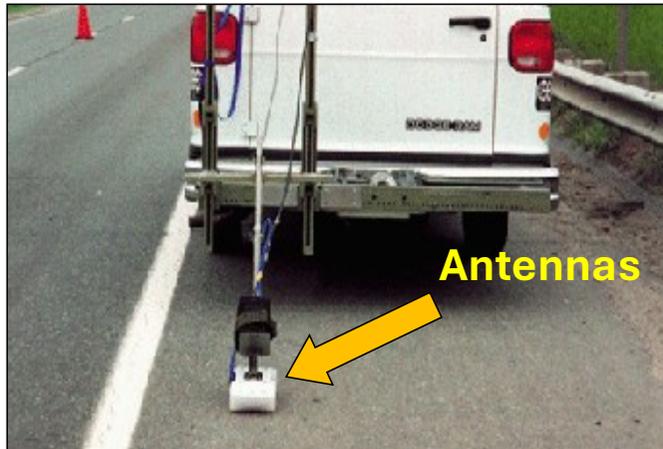
2D processed data



3D processed data

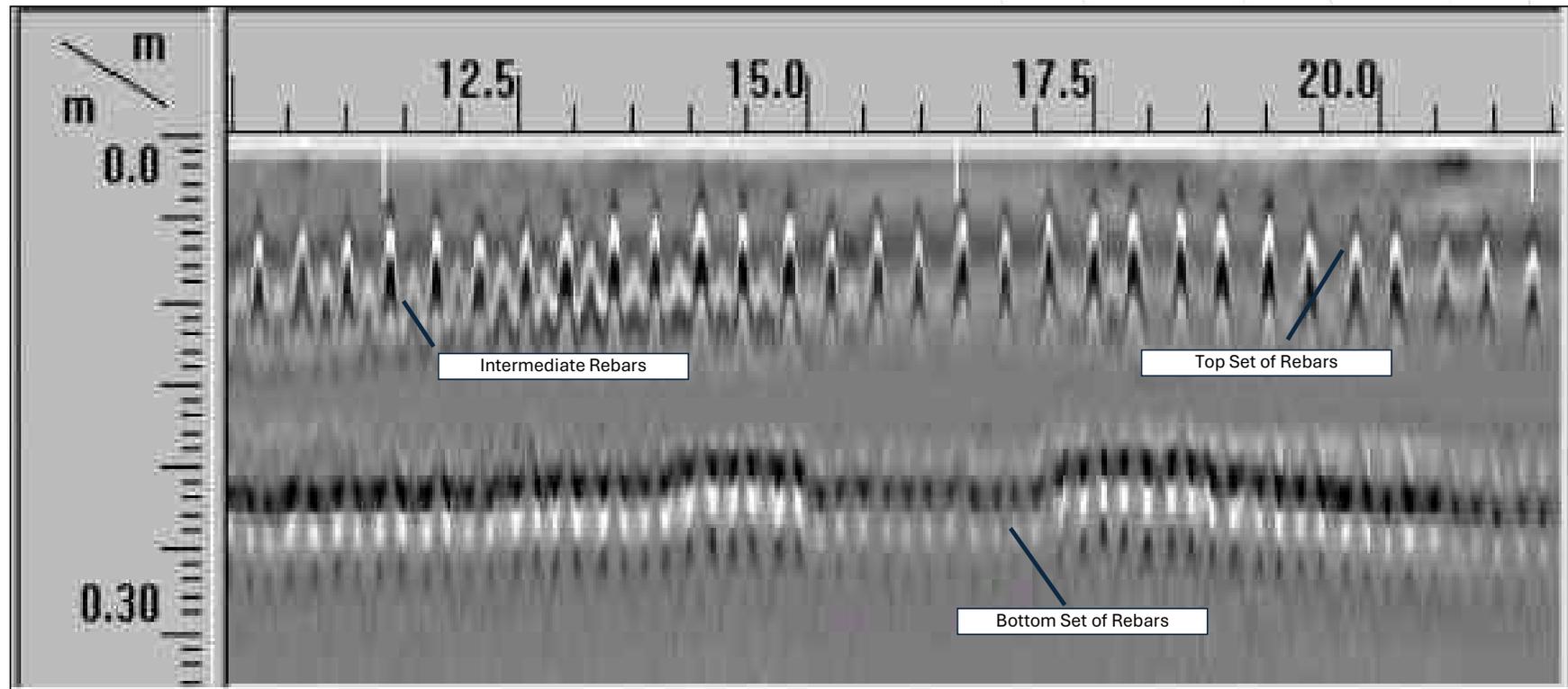


Example: bridge and highway inspections



Example: bridge and highway inspections

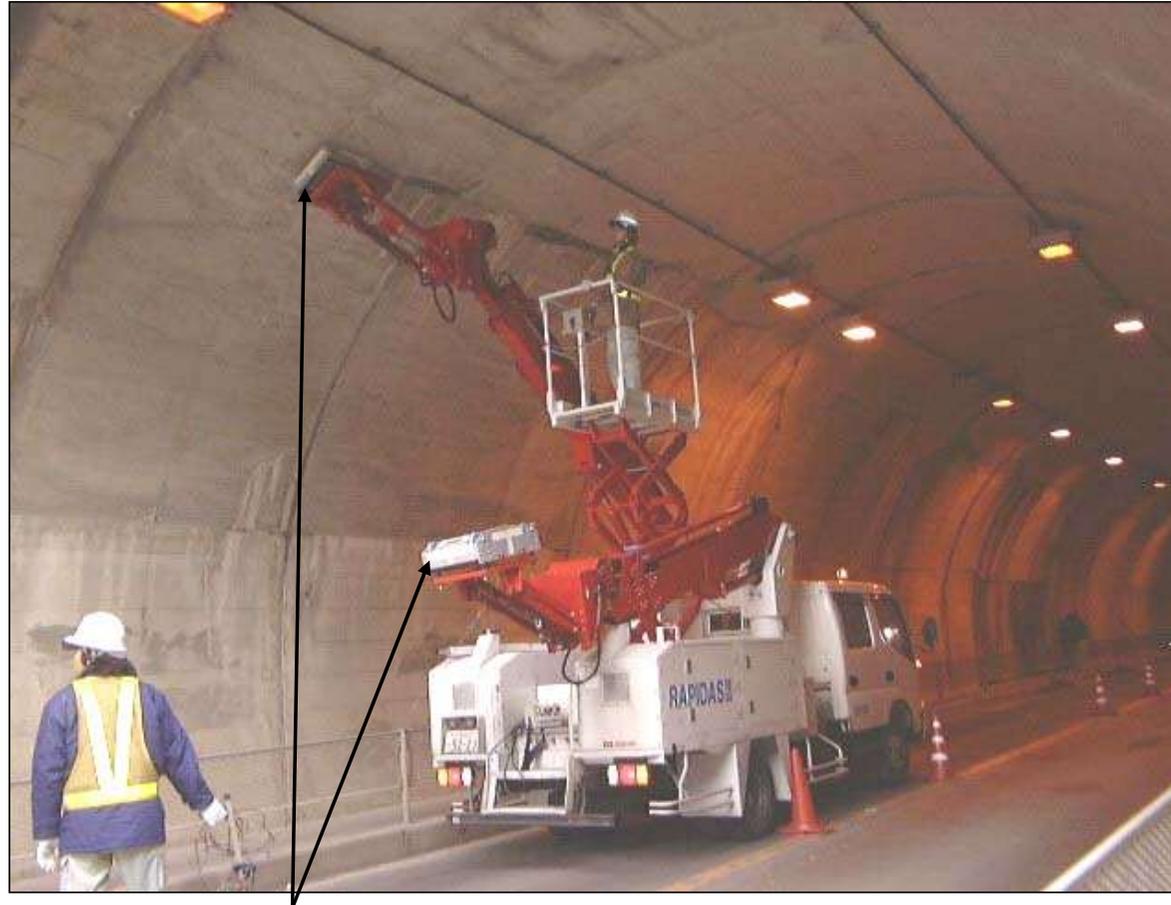
Location and depth of Rebars as part of a concrete slab investigation.



Note that the intermediate rebars were found to be missing on the right side of this section.

Example: tunnel inspections

OYO's (Japan) highway tunnel inspection vehicle "RAPIDAS"

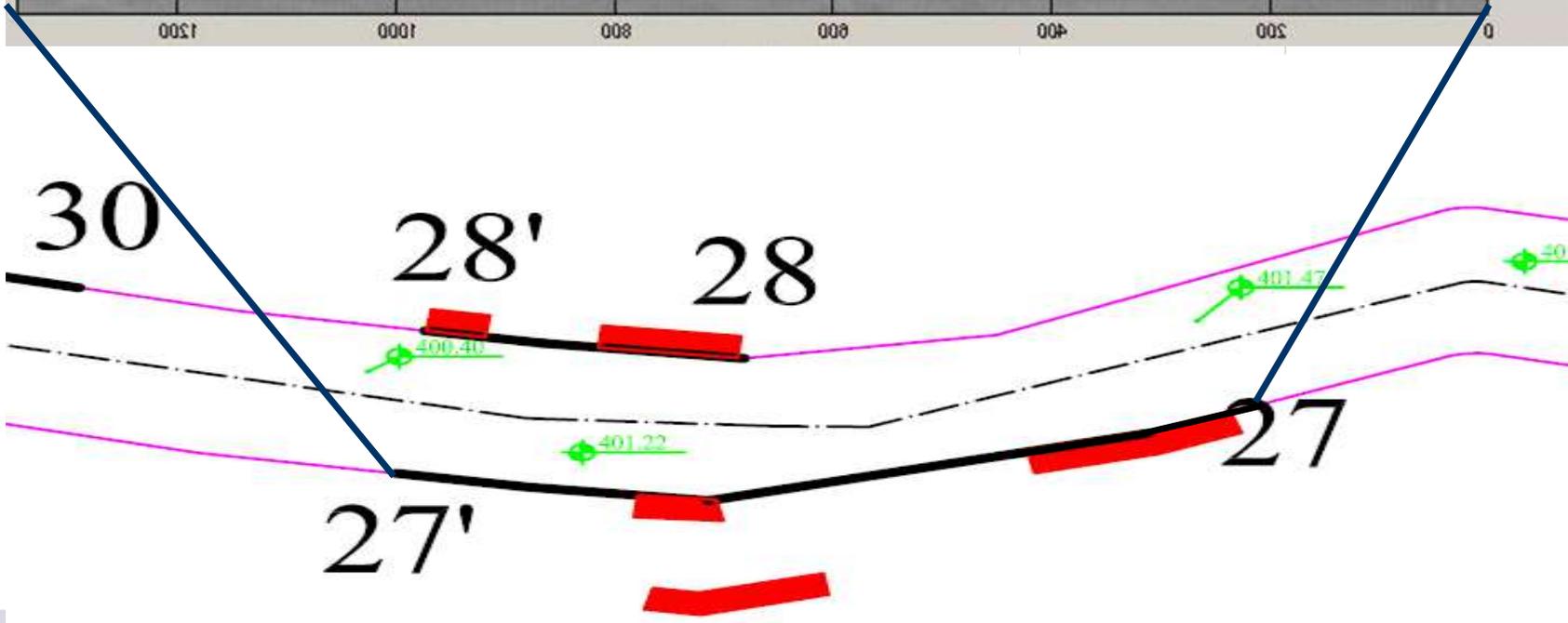
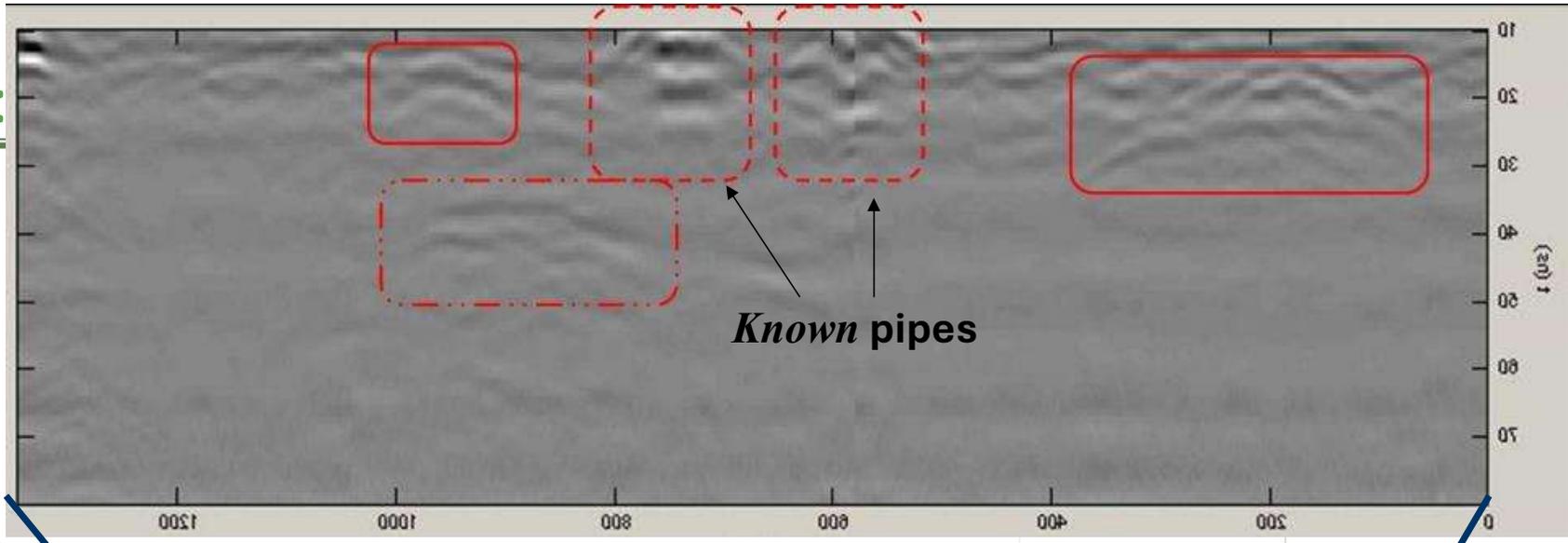


400 MHz or 900 MHz antenna

Example: tunnel inspections (a water tunnel)

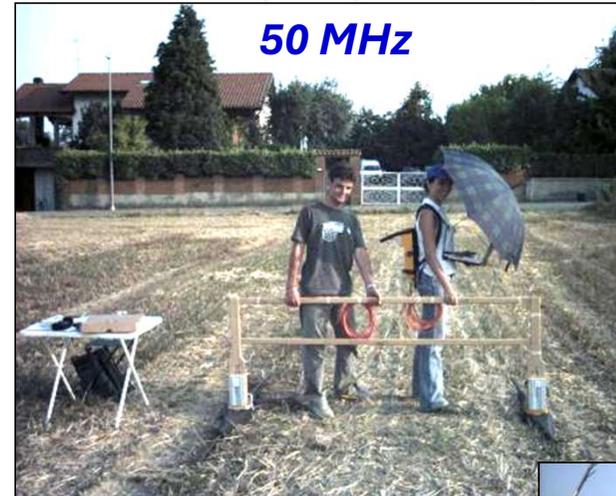


Example:



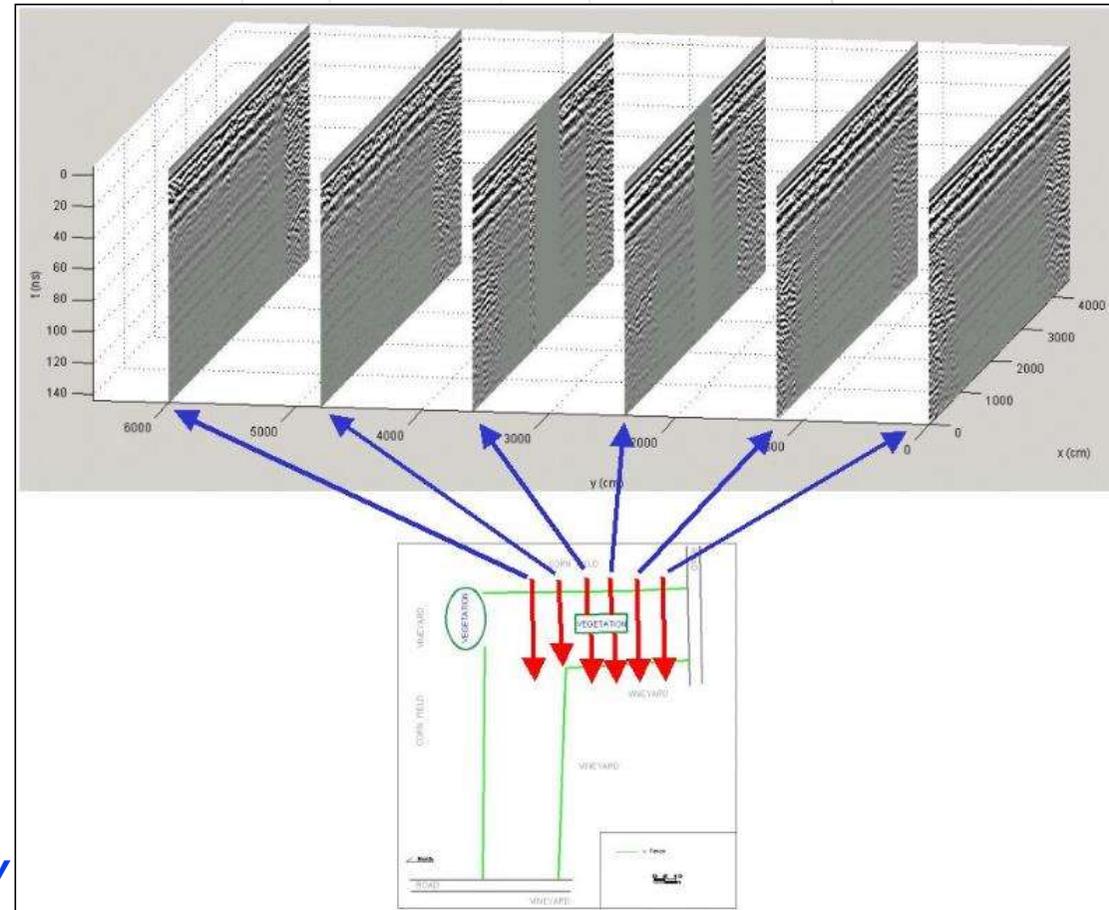
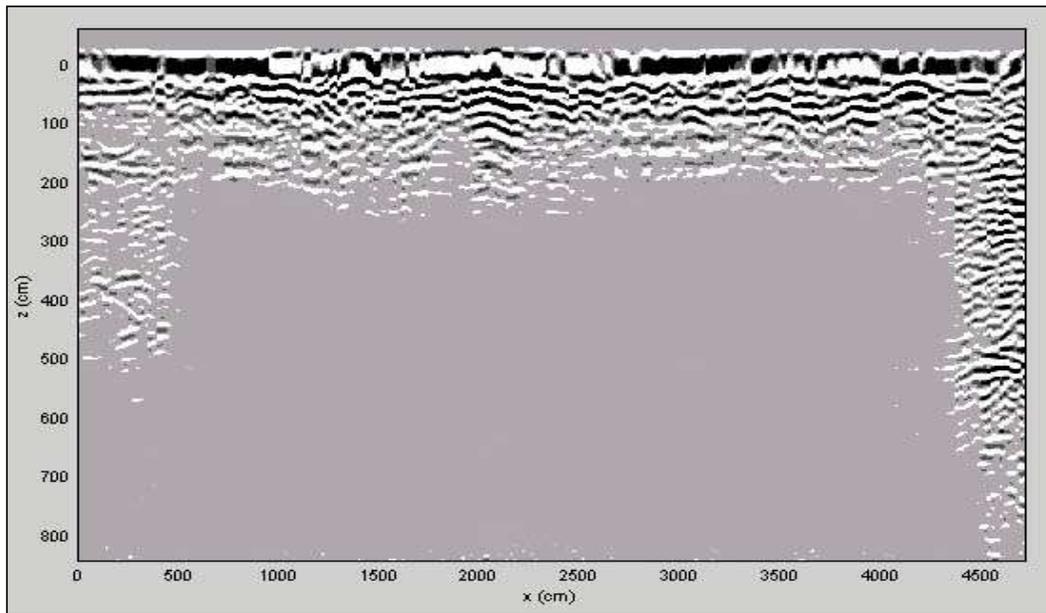
Example: landfills

Investigations on an industrial landfill (contaminations from metals and hydrocarbons)



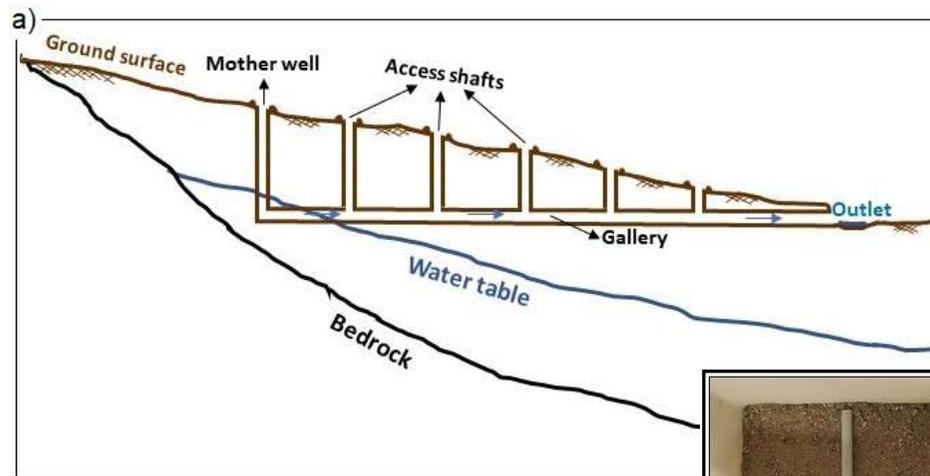
Example: landfills

250 MHz data



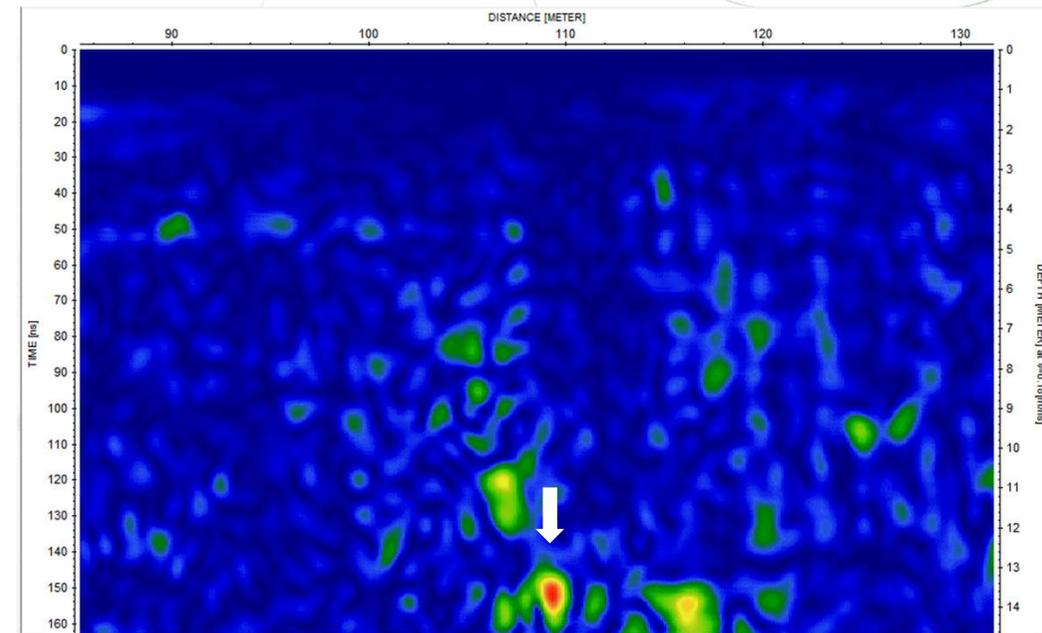
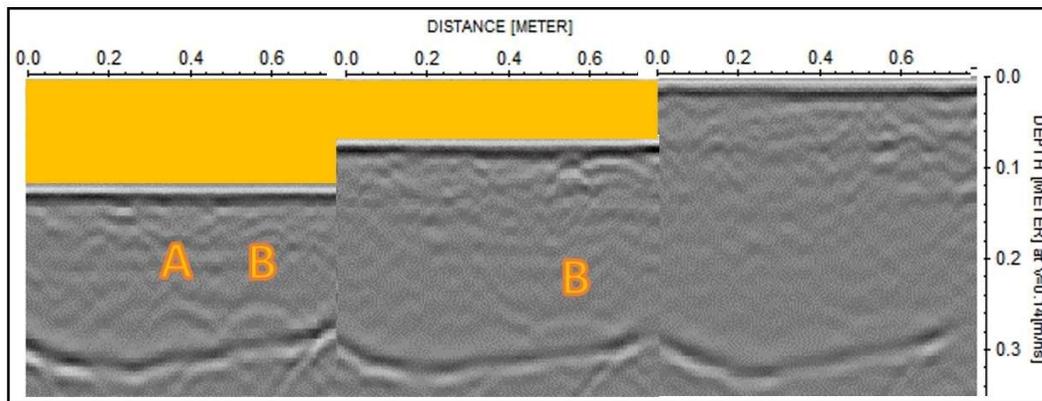
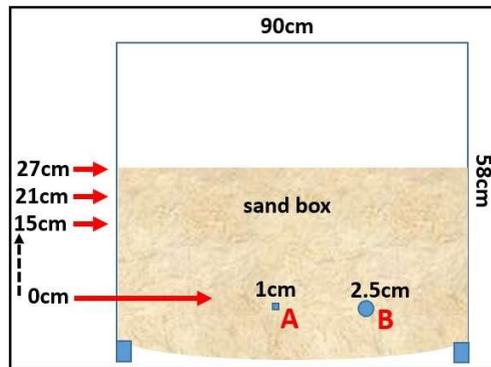
High absorption due to the conductive landfill body

Example: qanat



Example: qanat

Targets buried in the sand with VWC=8%



GPR applications in stone production

Quarry

Blocks

- ✓ Detecting the depth to layers.
- ✓ Determining main discontinuities and defects (faults, fractures, voids, intrusions).

- ✓ Exploring smaller defects (fractures, voids, intrusions).
- ✓ Monitoring the repair condition.



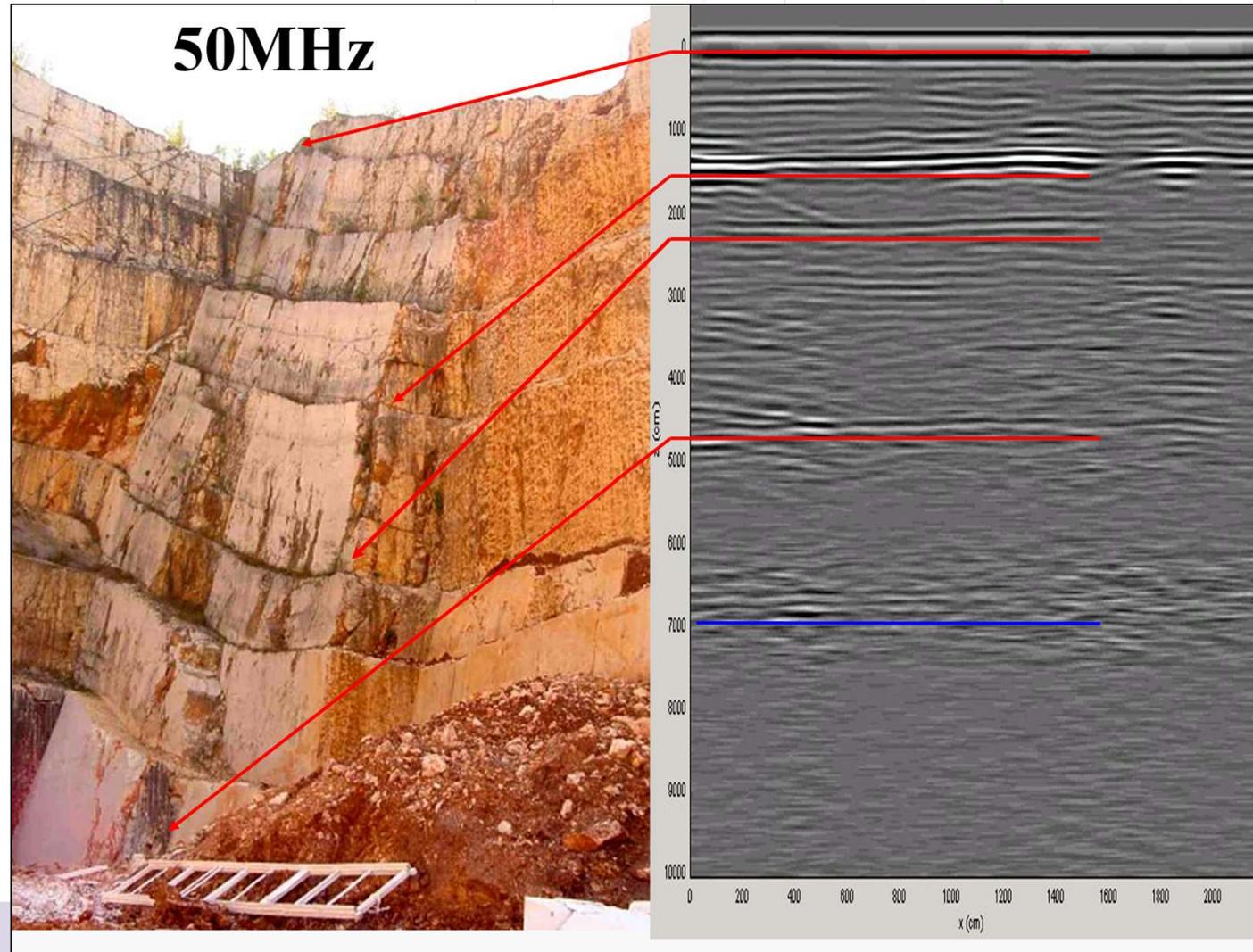
Example: quarries

Investigations in a limestone quarry

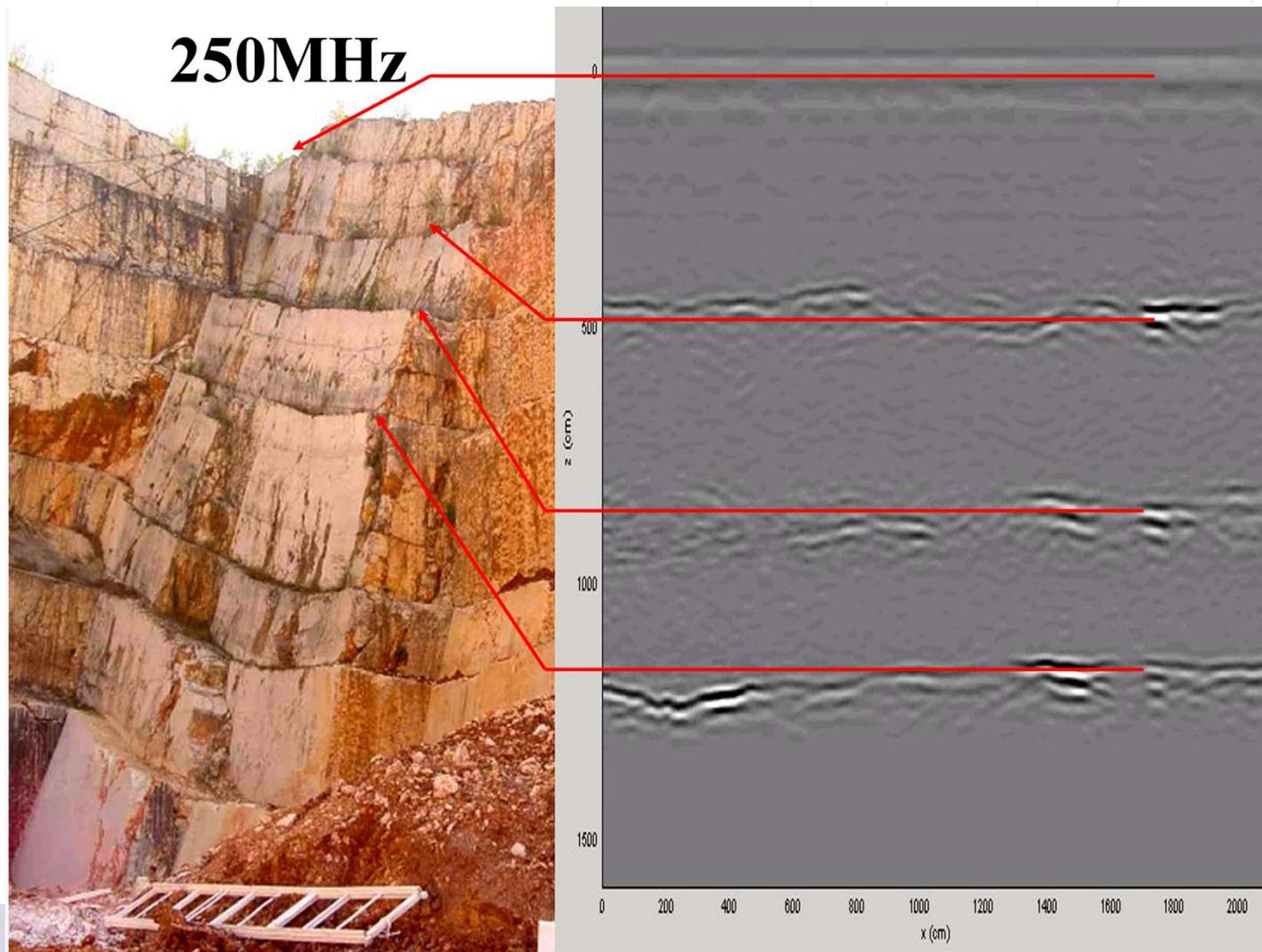


Example: quarries

Acquisitions with the 50MHz antenna



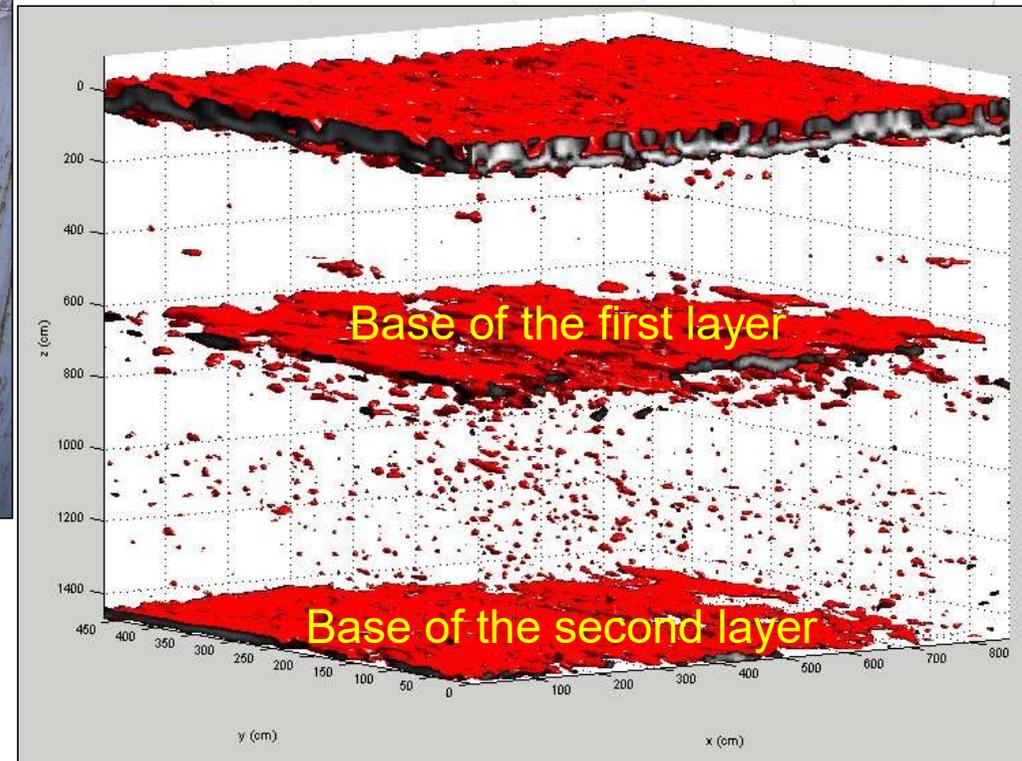
Example: quarries



Example: quarries

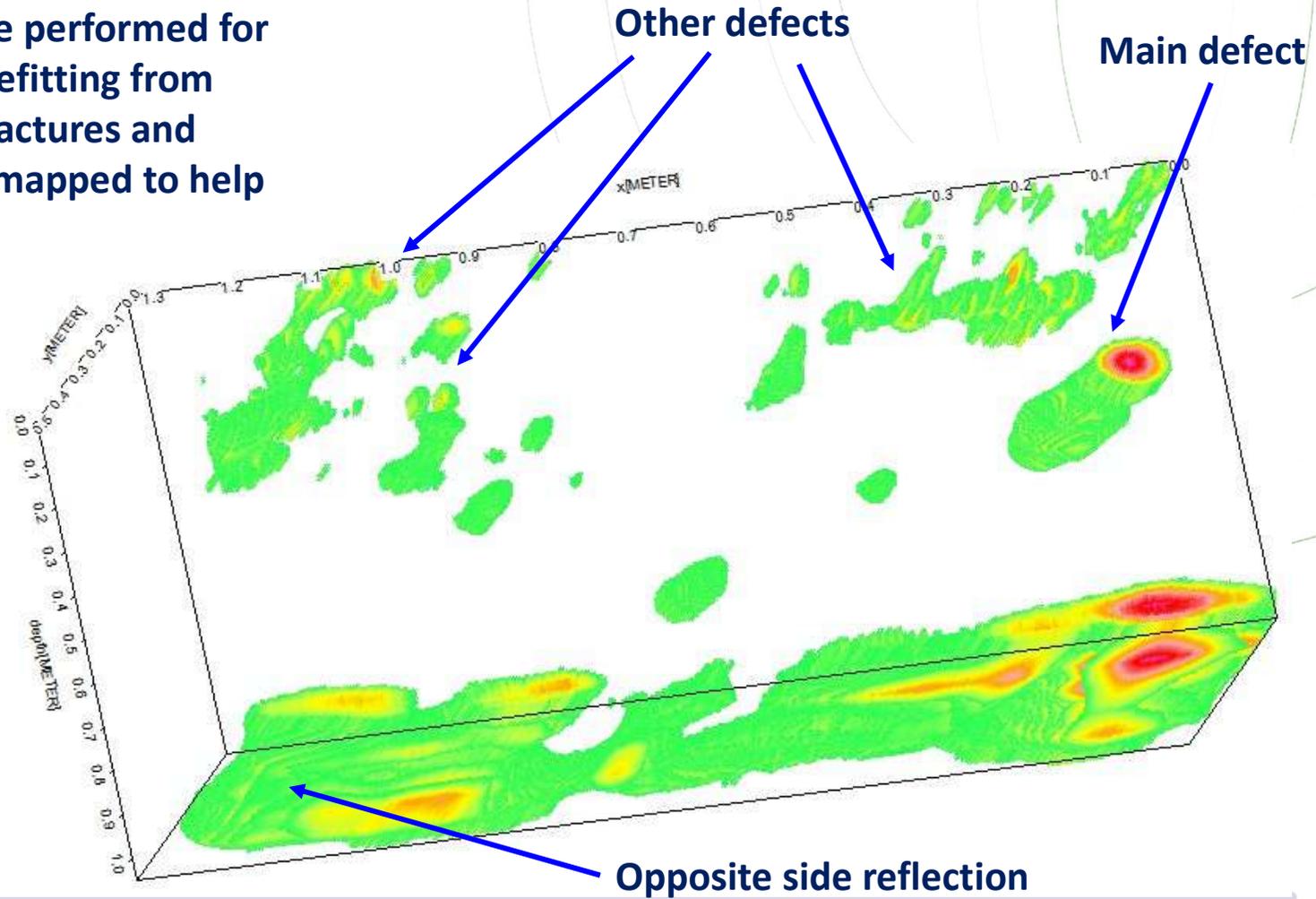


250 MHz data



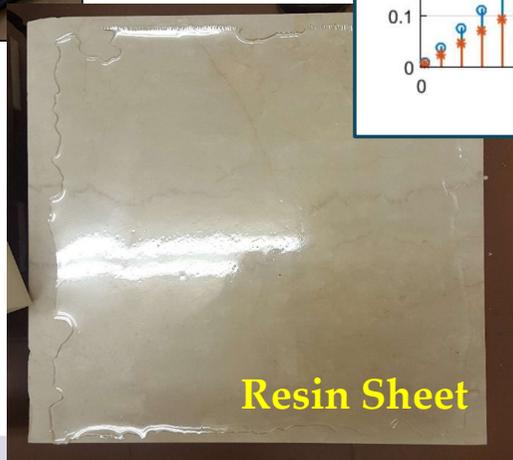
Example: quarries

High-frequency measurements can be performed for the quality control of the blocks. Benefitting from better resolution at this stage, thin fractures and internal defects of the blocks can be mapped to help improving the slab production.

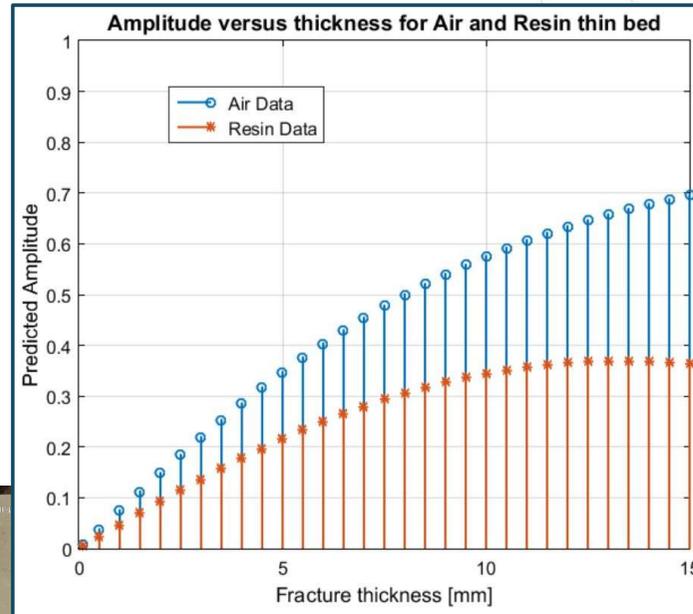


Example: quarries

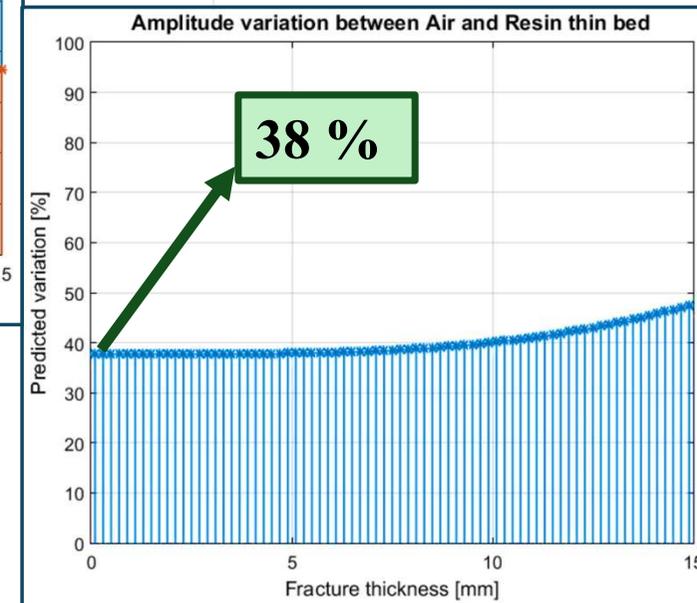
Time-lapse GPR to check the repair condition of fractures



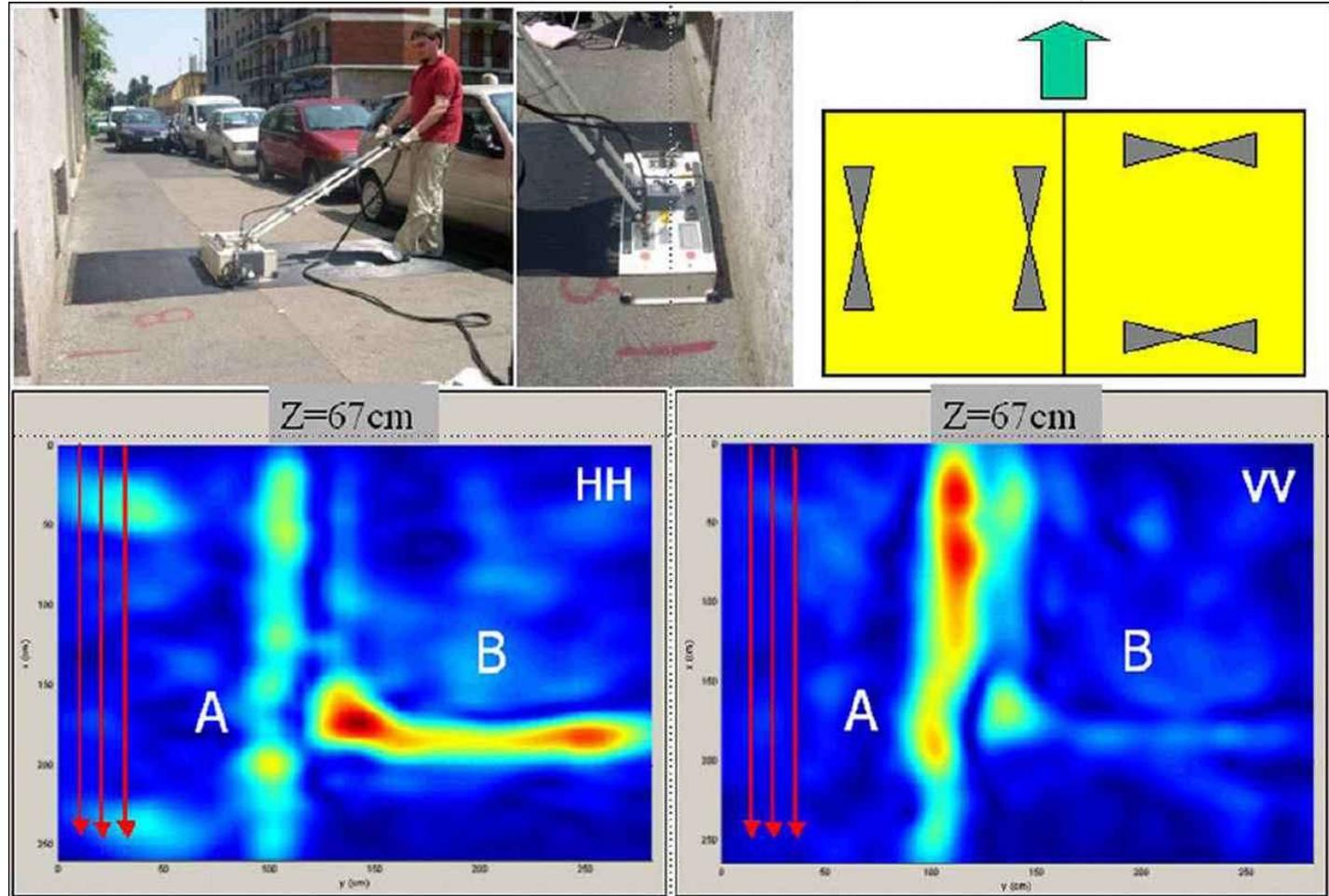
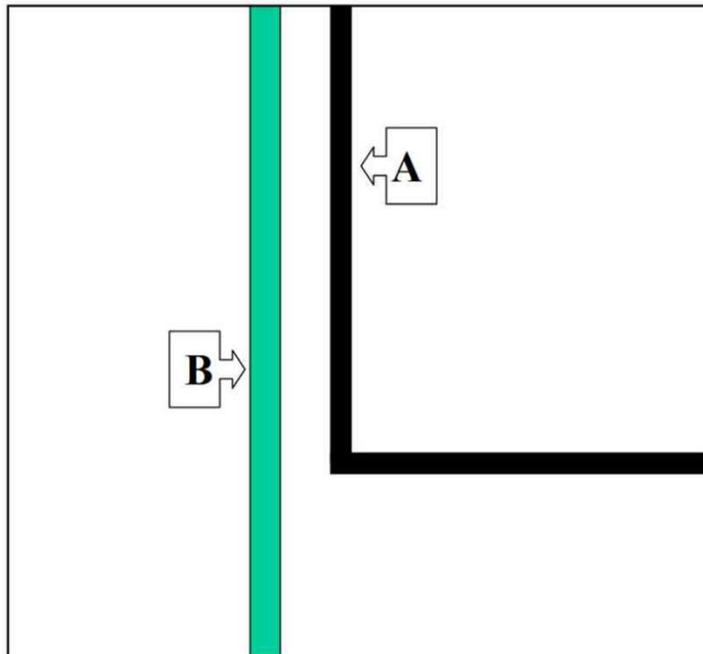
Resin Sheet



Analytical model



Example: utility detection

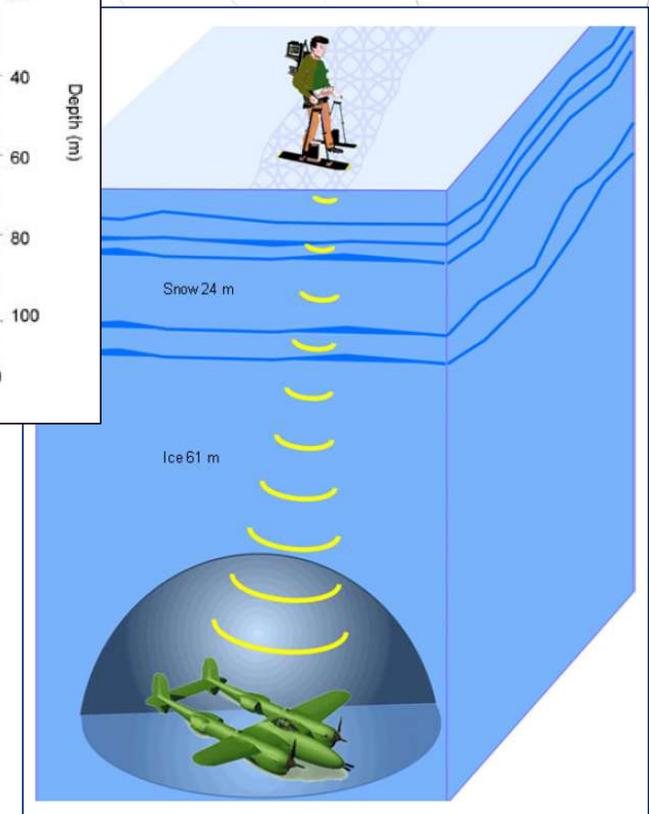
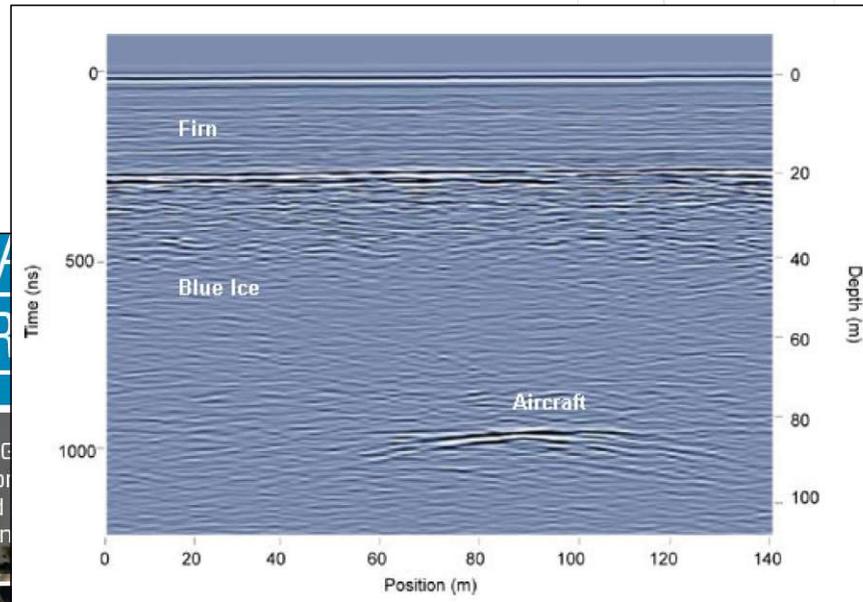


Example: ice and snow

Mt. Everest summit expedition (IDS, 2004)



Example: ice and snow



Example: ice and snow





Geophysical methods in geoscience and near surface geophysics - Ground Penetrating Radar

Pisa, 22 January 2025

THANKS!

Azadeh Hojat (azadeh.hojat@polimi.it)

IR0000032 – ITINERIS, Italian Integrated Environmental Research Infrastructures System
(D.D. n. 130/2022 - CUP B53C22002150006) Funded by EU - Next Generation EU PNRR-
Mission 4 "Education and Research" - Component 2: "From research to business" - Investment
3.1: "Fund for the realisation of an integrated system of research and innovation infrastructures"

