



Landslide forecasting and warning at slope scale

Advanced technologies for monitoring and prediction of ground instabilities
Firenze, 27-30 January 2025

IR0000032 – ITINERIS, Italian Integrated Environmental Research Infrastructures System

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Mission 4 "Education and Research" - Component 2: "From research to business" - Investment
3.1: "Fund for the realisation of an integrated system of research and innovation infrastructures"



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NextGenerationEU

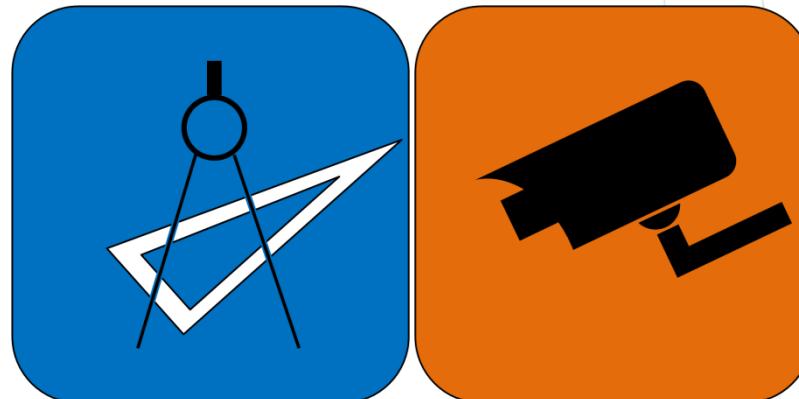
Ministero
dell'Università
e della Ricerca



Early Warning Systems

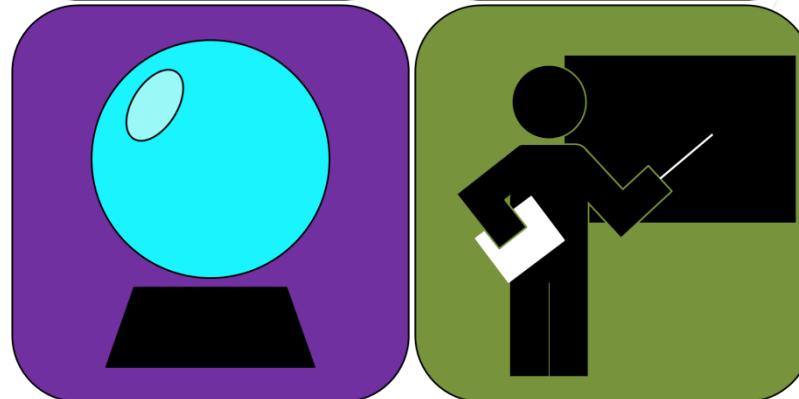
1. Design:

- Geological knowledge
- Risk scenarios
- Design criteria
- Choice of geo-indicators



3. Forecasting:

- Data interpretation
- Comparison with thresholds
- Forecasting methods
- Warning



2. Monitoring:

- Instruments installation
- Data collecting
- Data transmission
- Data elaboration

4. Education:

- Risk perception
- Safe behaviours
- Response to warning
- Population involvement

Intrieri et al. (2013)

Forecast

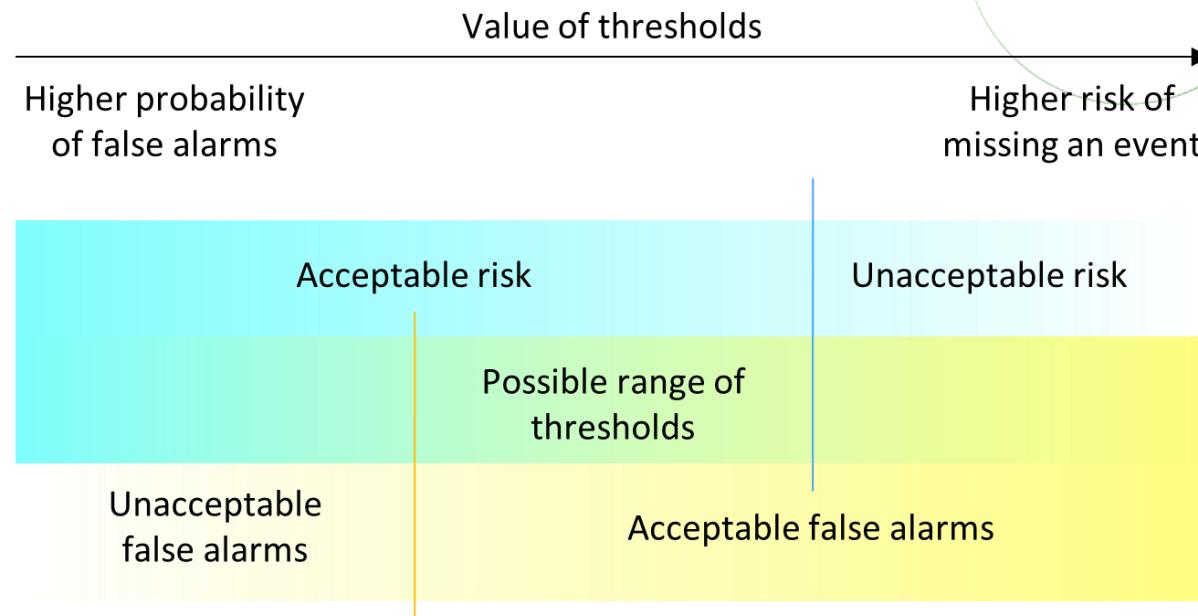
Determination of the time, place and magnitude of the single most significant movement episode of the object of monitoring

Structural interventions



EWS Principles

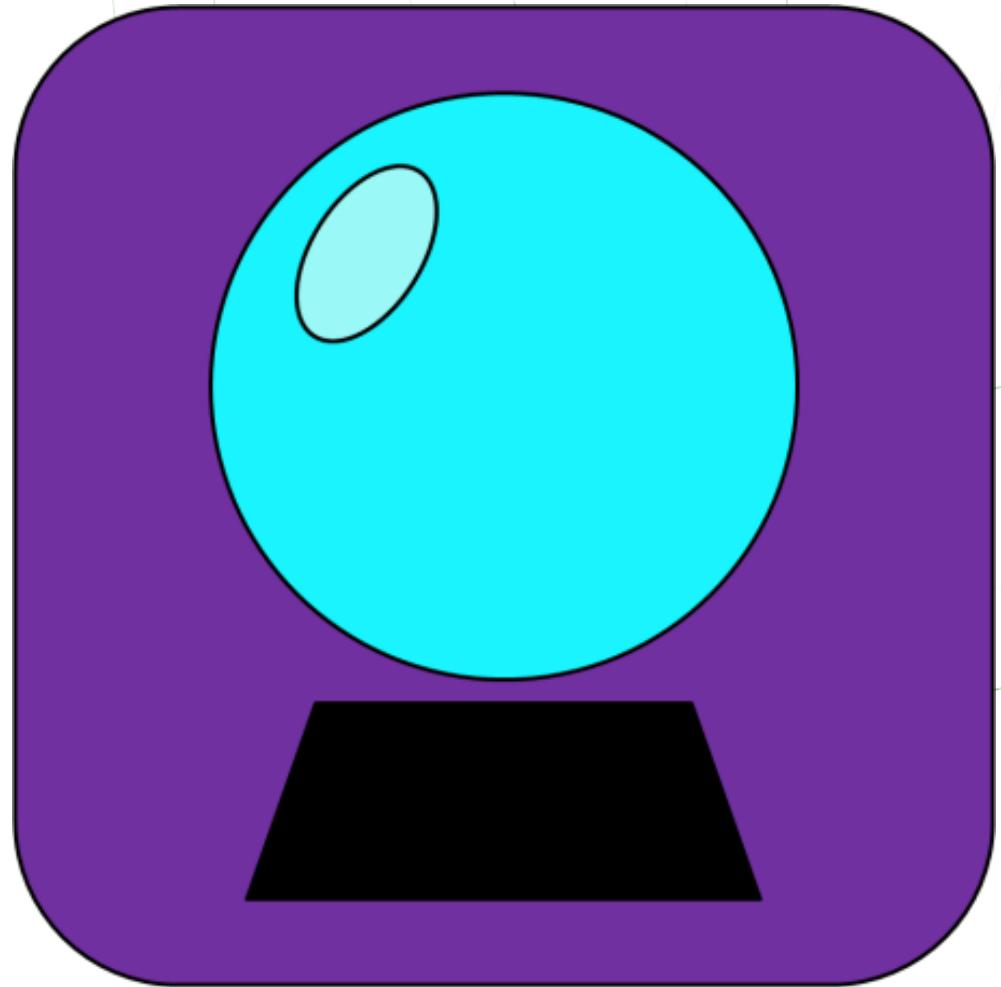
- Site-specific: There is no such thing as a universal EWS
- Simplicity: avoid confusion, time loss and too many warning levels
- Earliness: it is relative to the landslide behavior
- Redundancy: some events are critical for the slope and the instruments
- Risk acceptability: depends on risk scenarios and culture



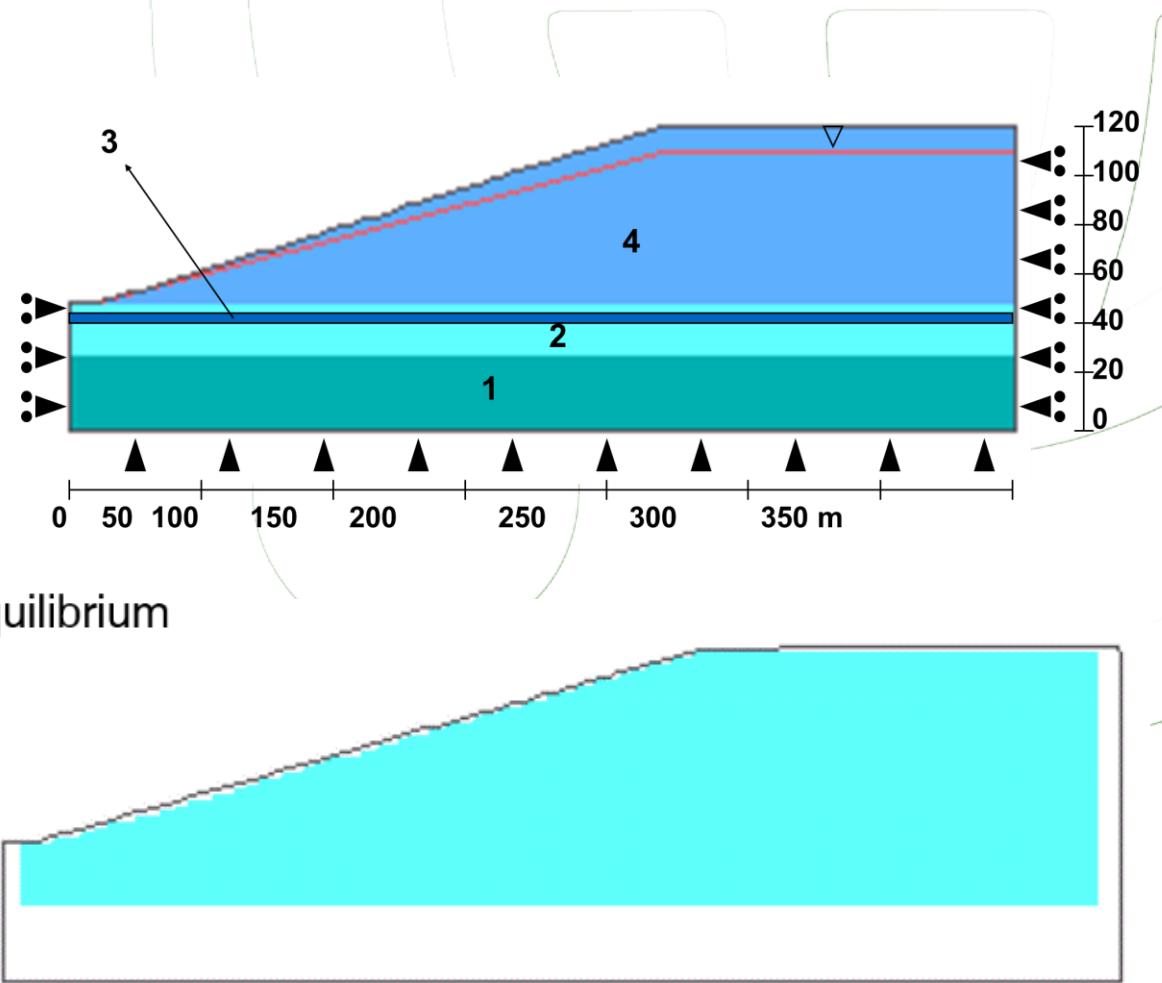
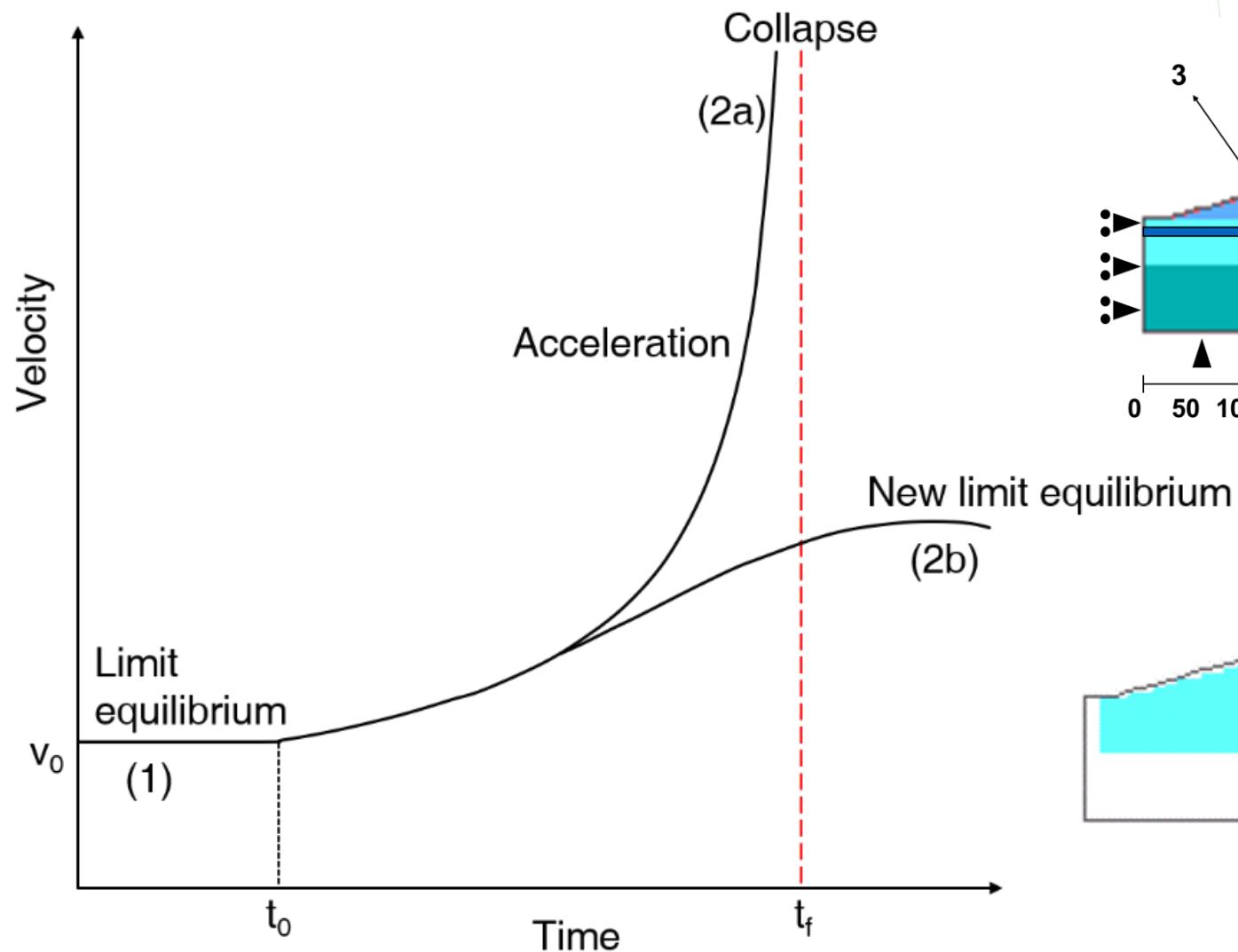
Nadim & Intrieri (2011)

Forecasting methods

- Rainfall based
- Porewater pressure
- Acoustic emissions
- Rockfall frequency
- Kinematic based (monitoring)**



Pre-paroxistic acceleration

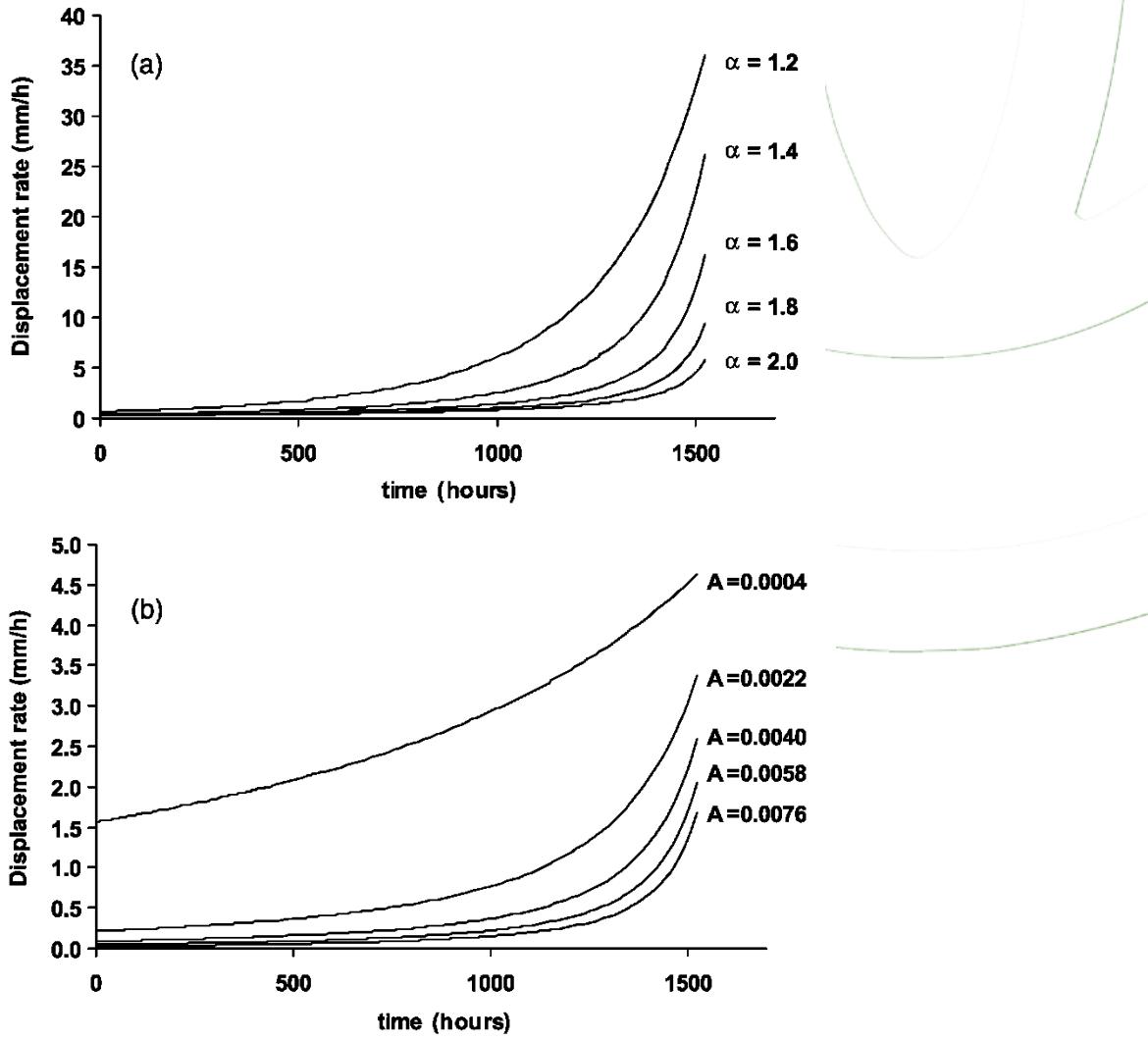


Power law relationship between **acceleration** and **velocity** before failure, tested on laboratory physical models

$$\frac{d^2x}{dt^2} = A \left(\frac{dx}{dt} \right)^\alpha$$

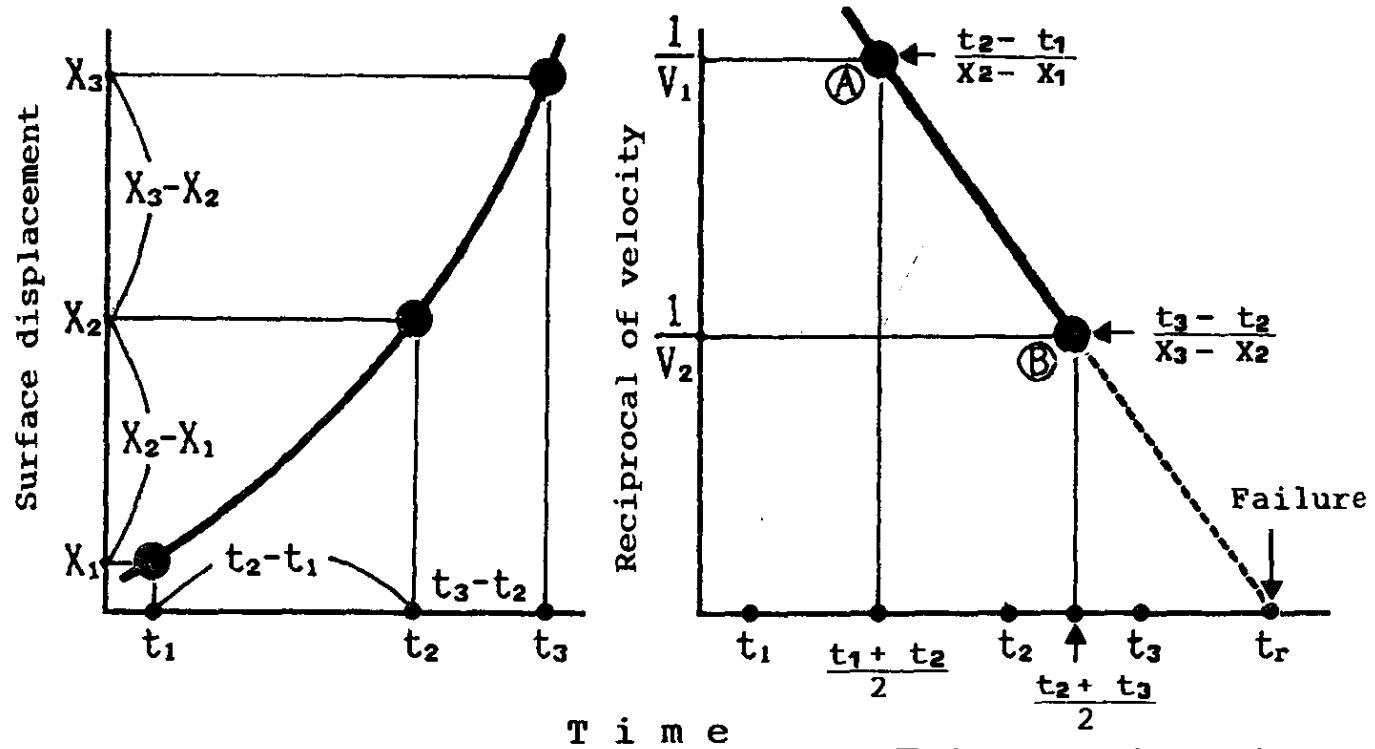
for $\alpha > 1$:

$$(t_f - t_i) = \frac{(v_f)^{1-\alpha} - (v_i)^{1-\alpha}}{A(1-\alpha)}$$

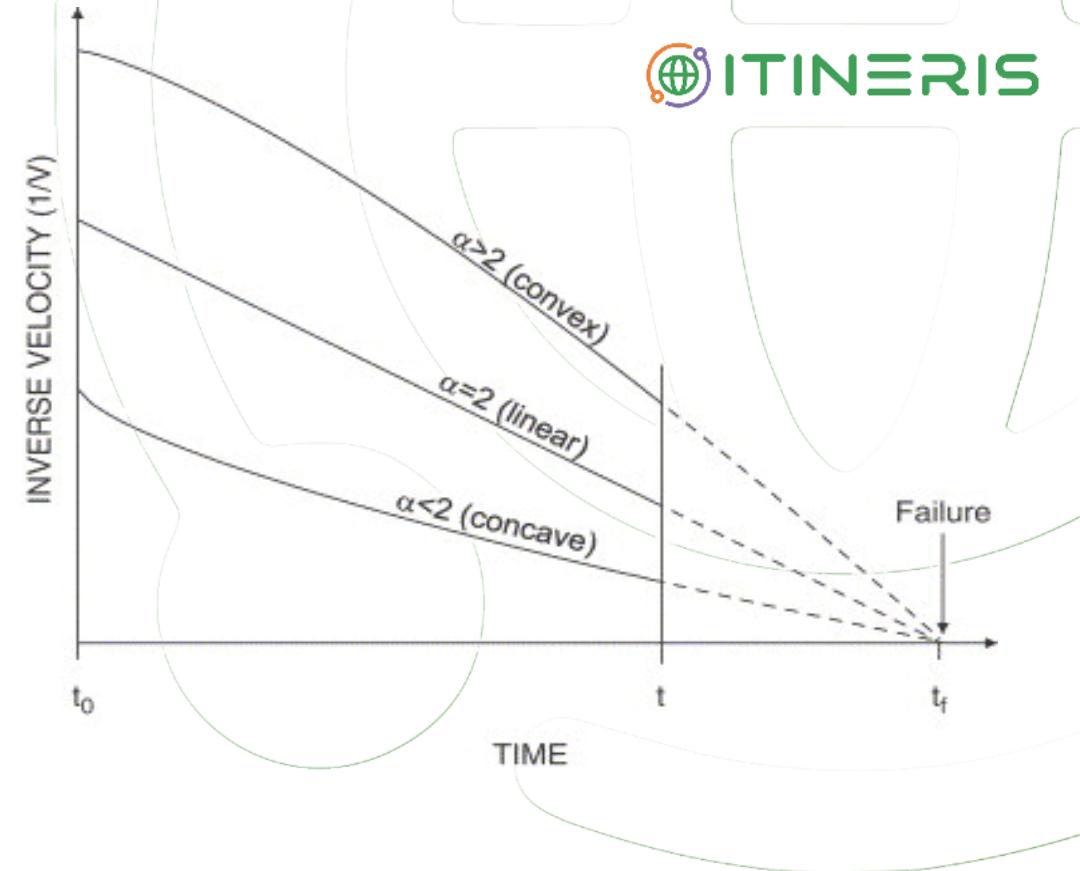


Inverse velocity method

$$v_f = \infty \Rightarrow \frac{1}{v_i} = [A(\alpha - 1)]^{\frac{1}{\alpha-1}} (t_f - t)^{\frac{1}{\alpha-1}}$$

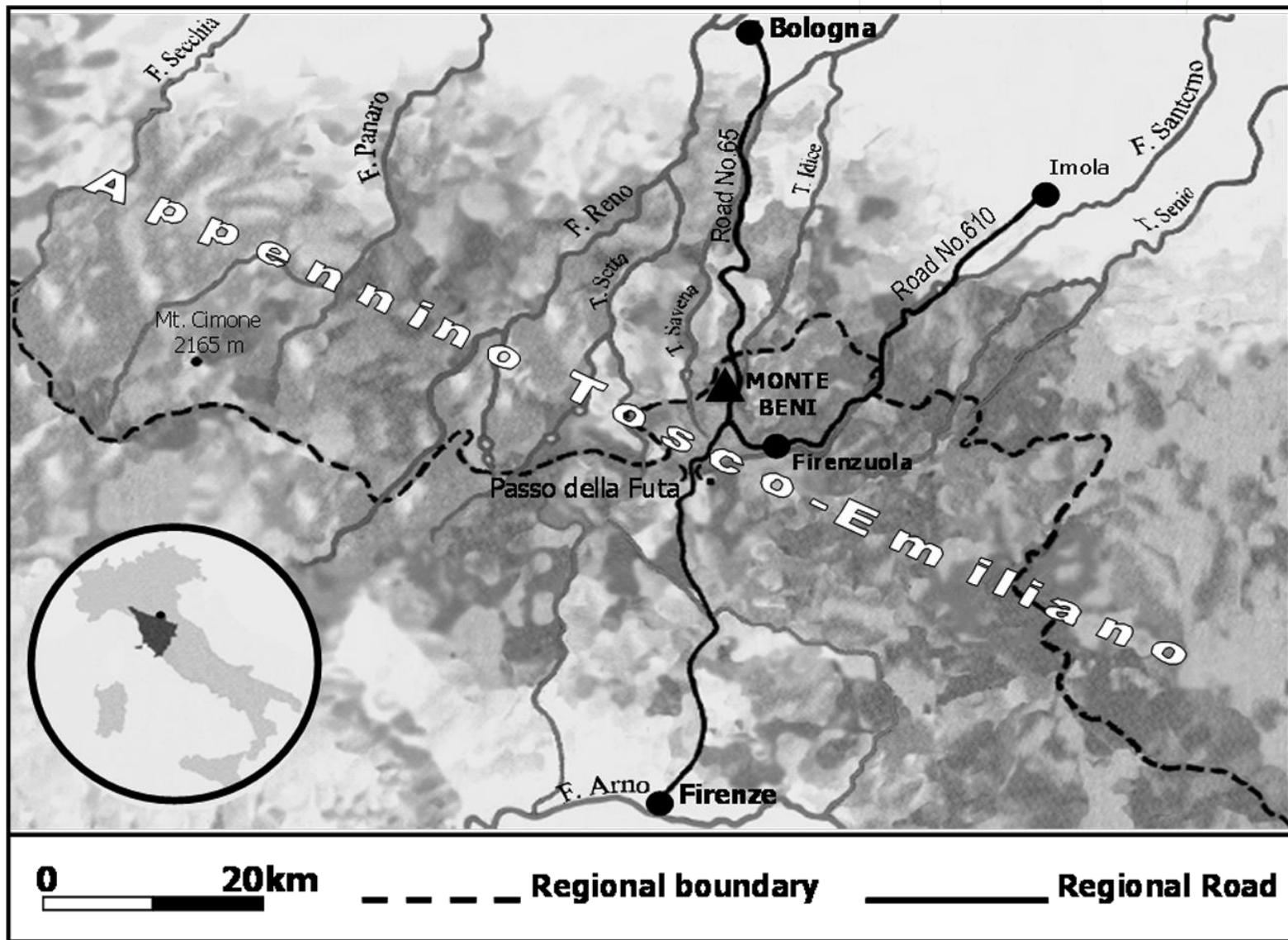


Fukuzono (1985)

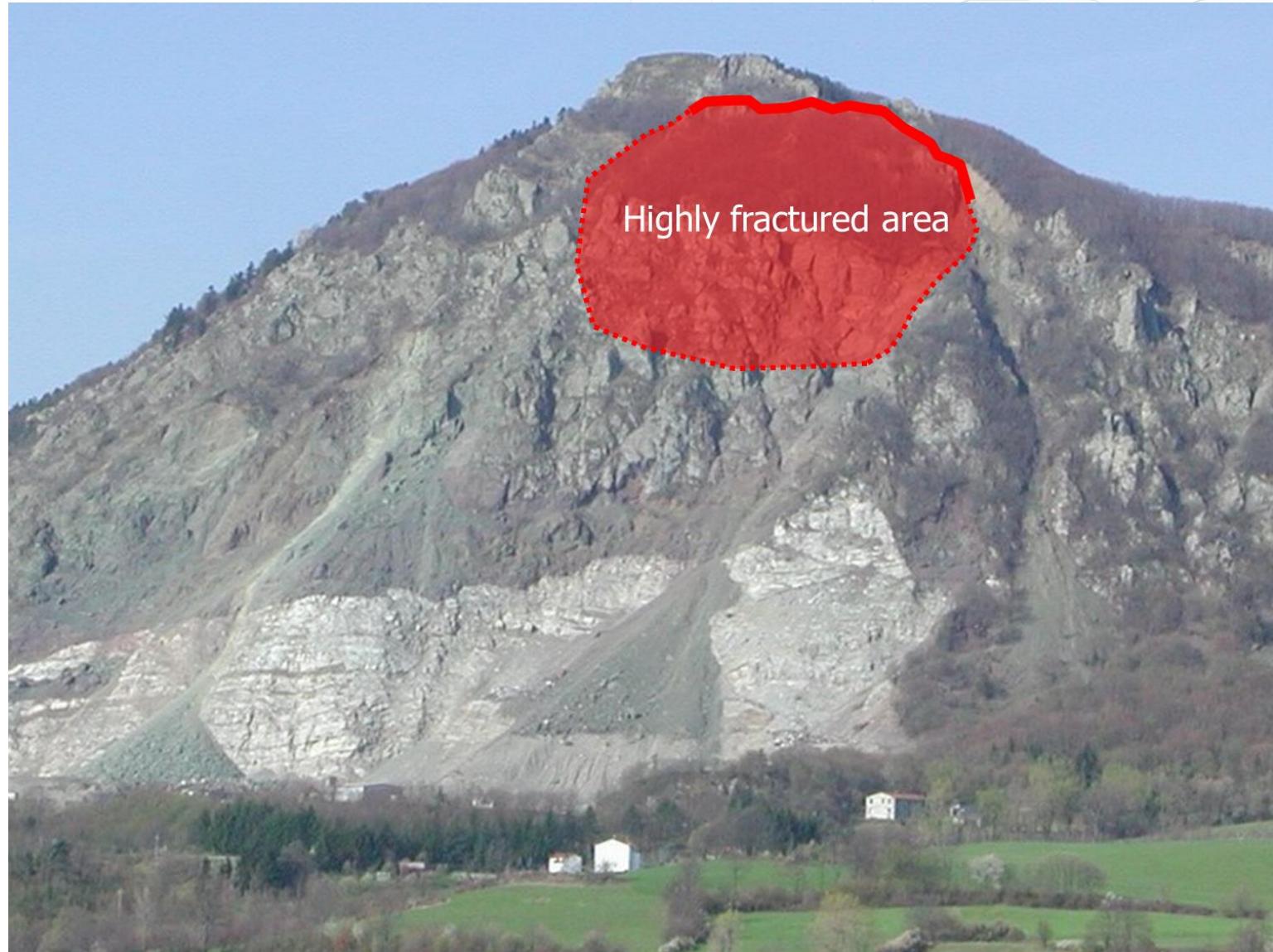


If $\alpha = 2$:
 $\mathbf{V^{-1} = A(t_f-t)}$
HYPERBOLA

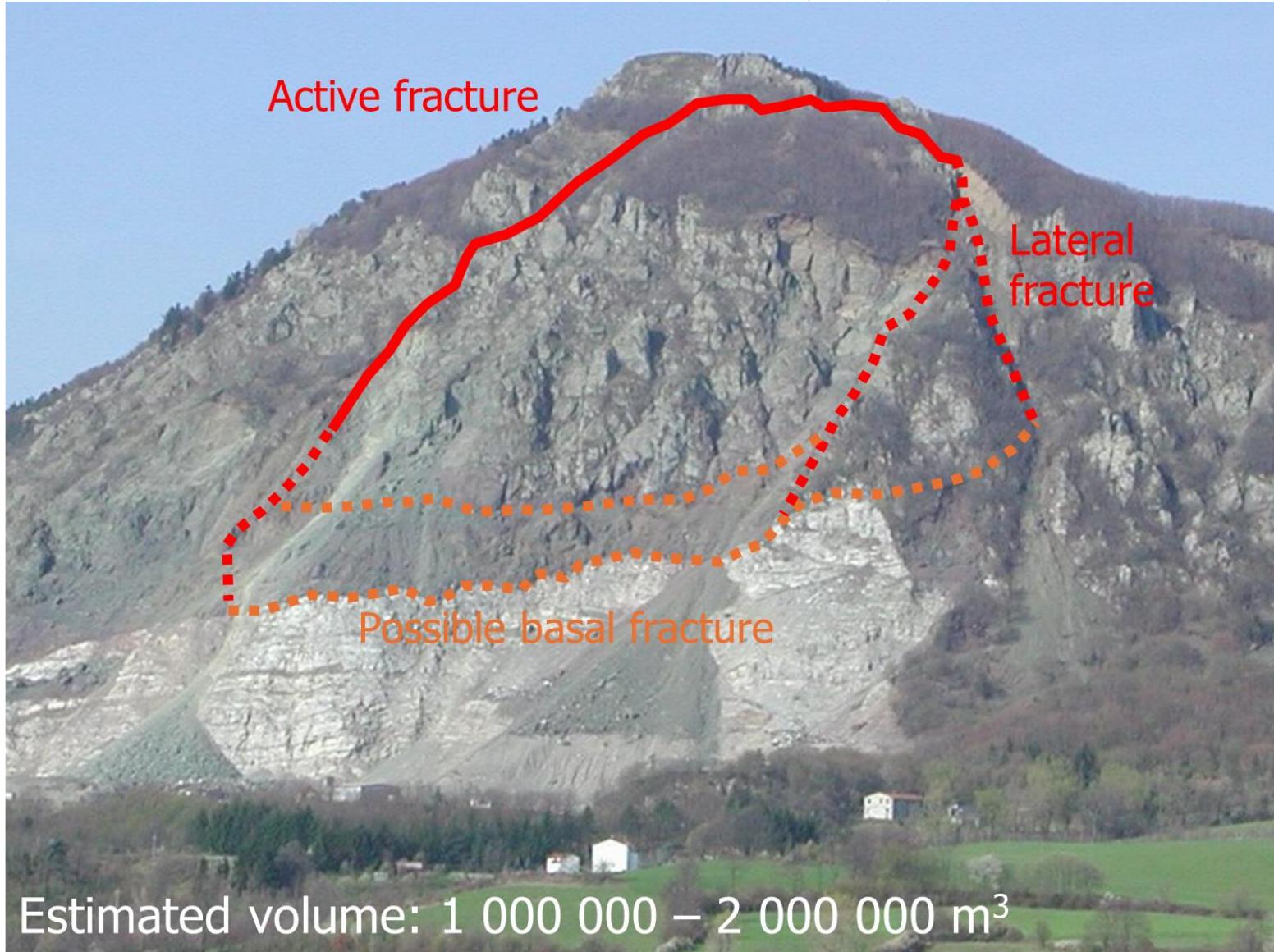
Case study: the Montebeni landslide



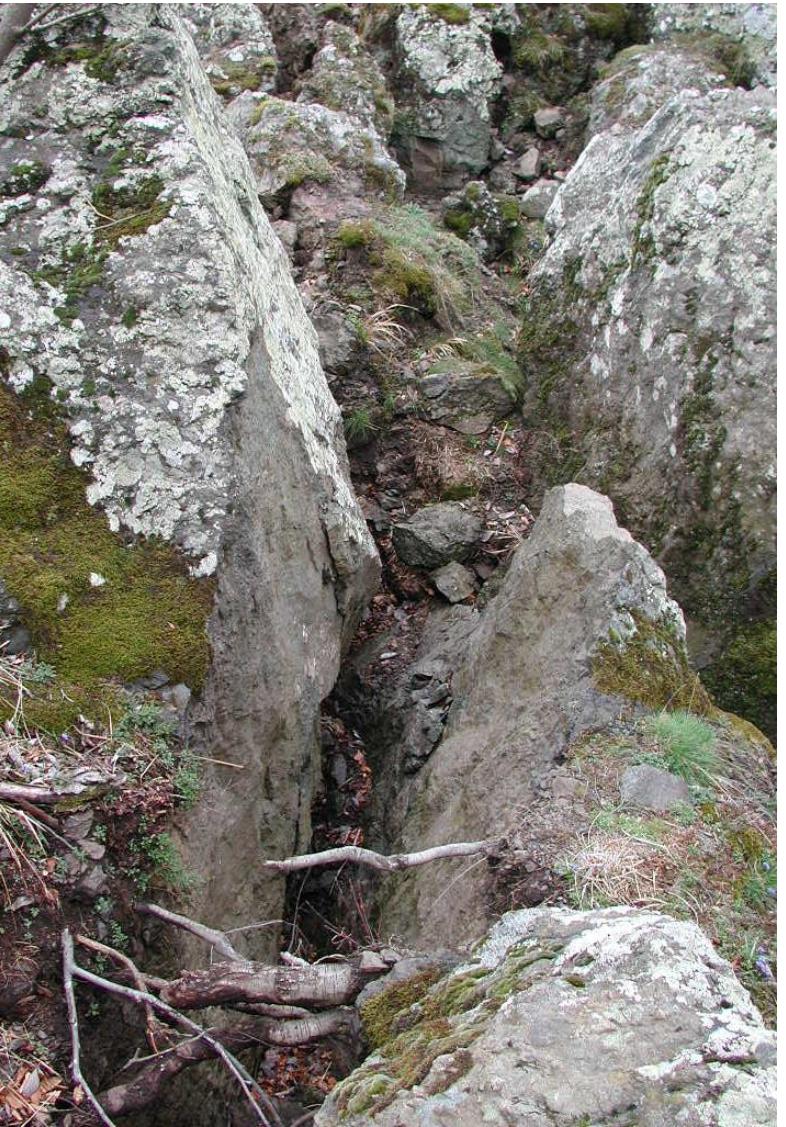
- ⌚ Kinematic Analysis
- ⌚ Rockfall simulations



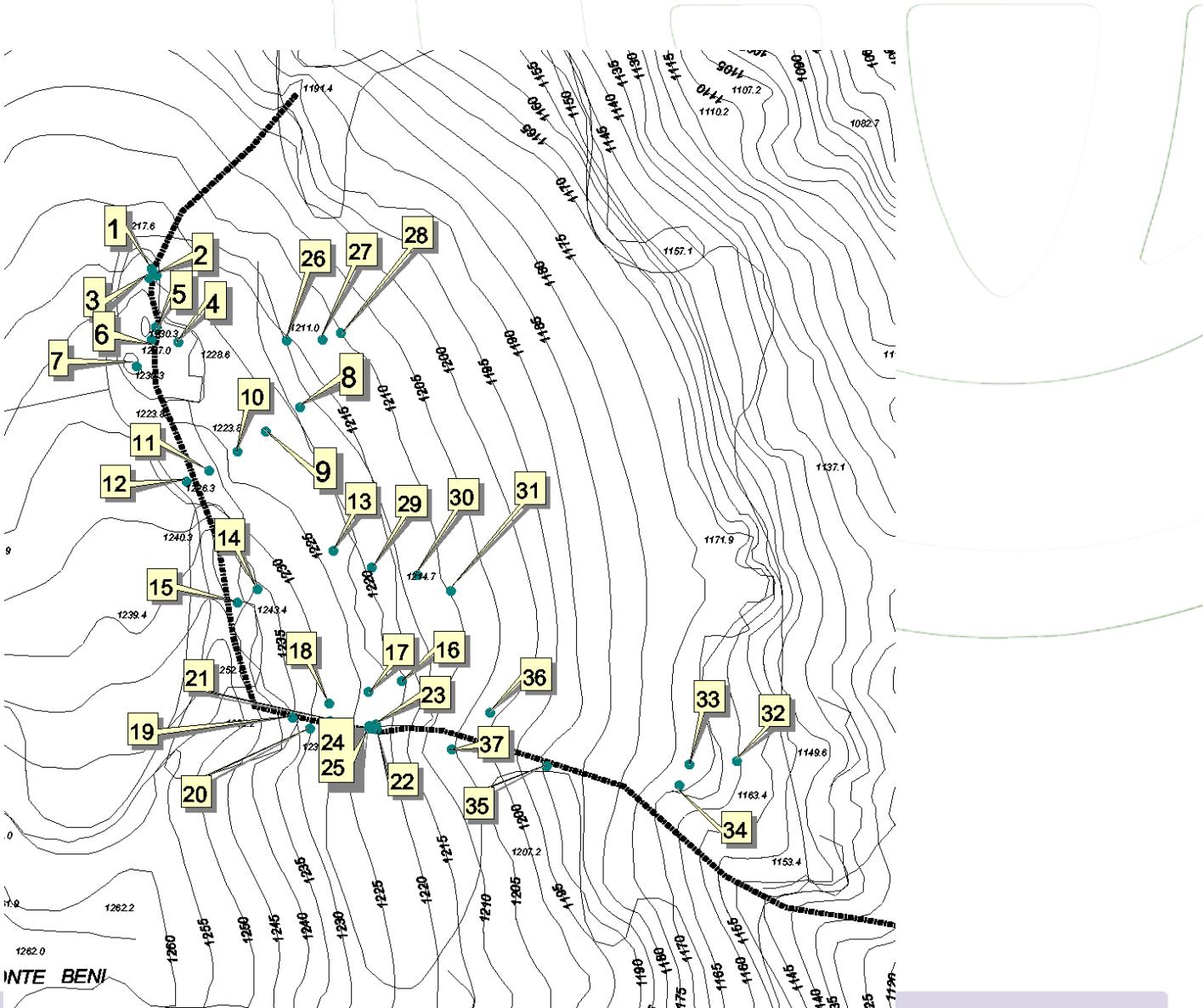
April, 2002



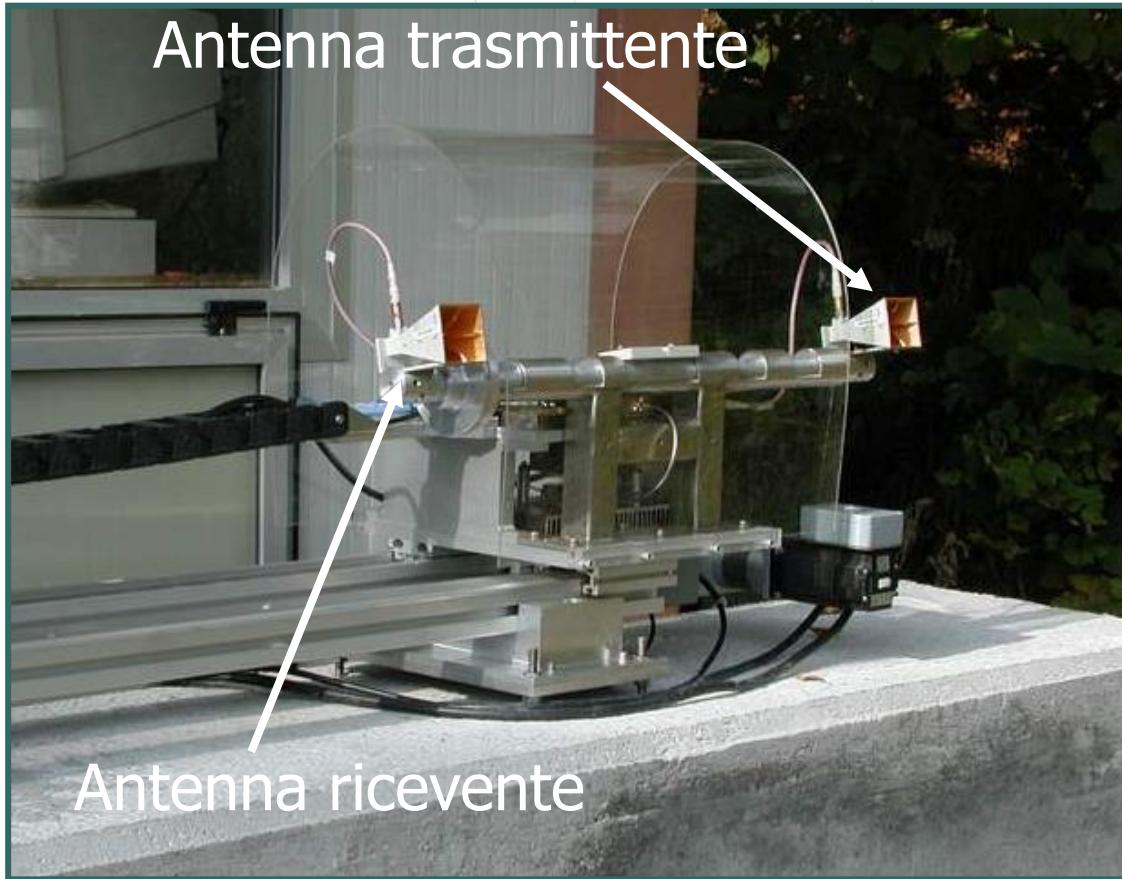
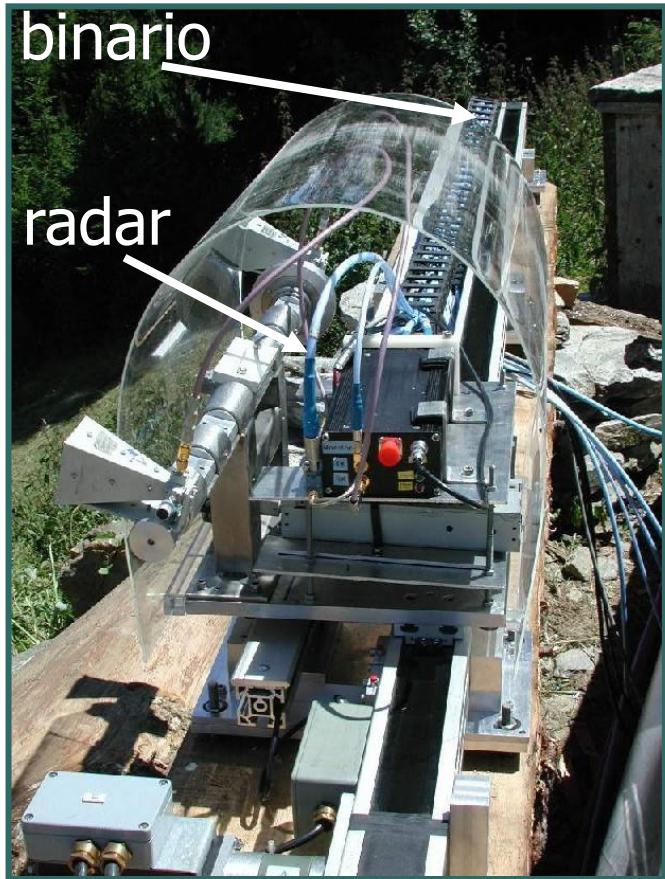
Upper fracture



Distometric monitoring



GB-InSAR monitoring



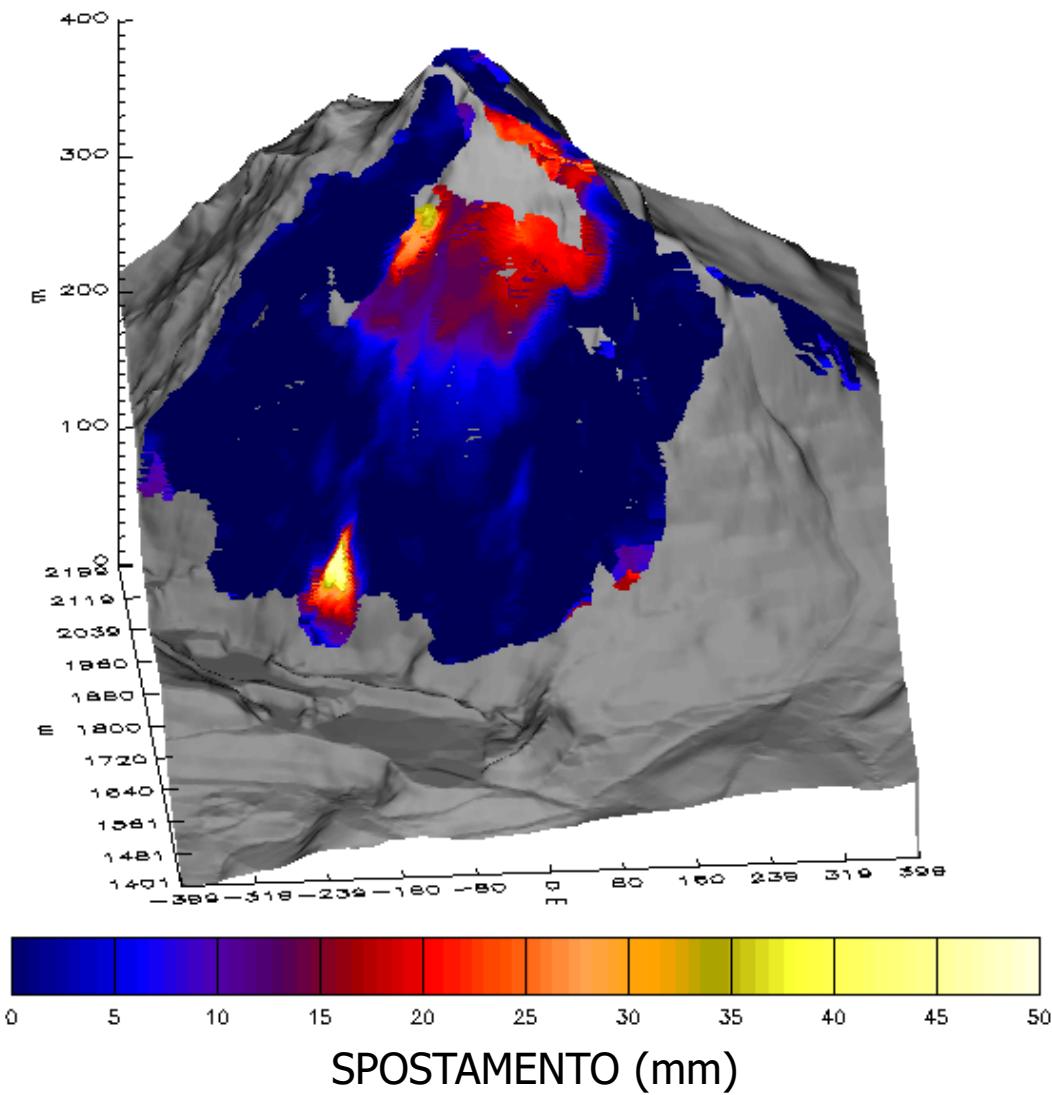
Commissione Europea
Centro Comune di Ricerca – Ispra
Istituto per la Sicurezza del Cittadino



Atmospheric conditions



GB-InSAR cumulated displacement



Start: 8/5/2002 13:59
End: 13/5/2002 18:12

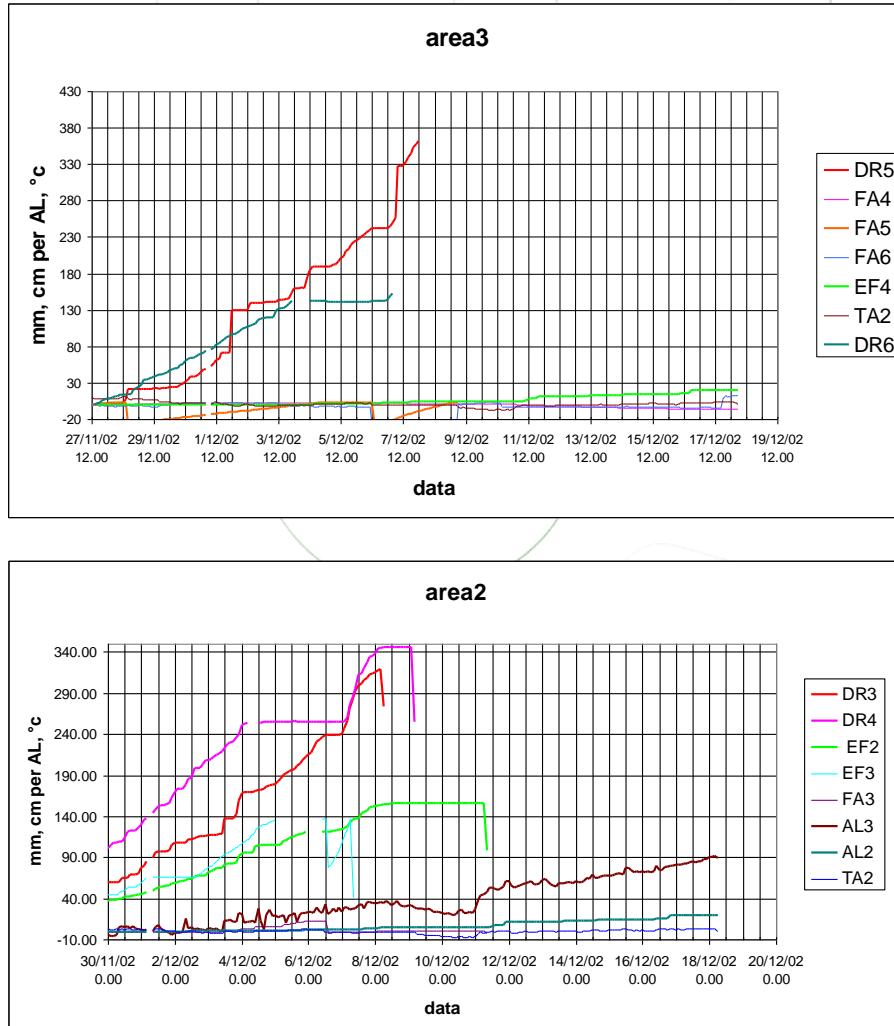
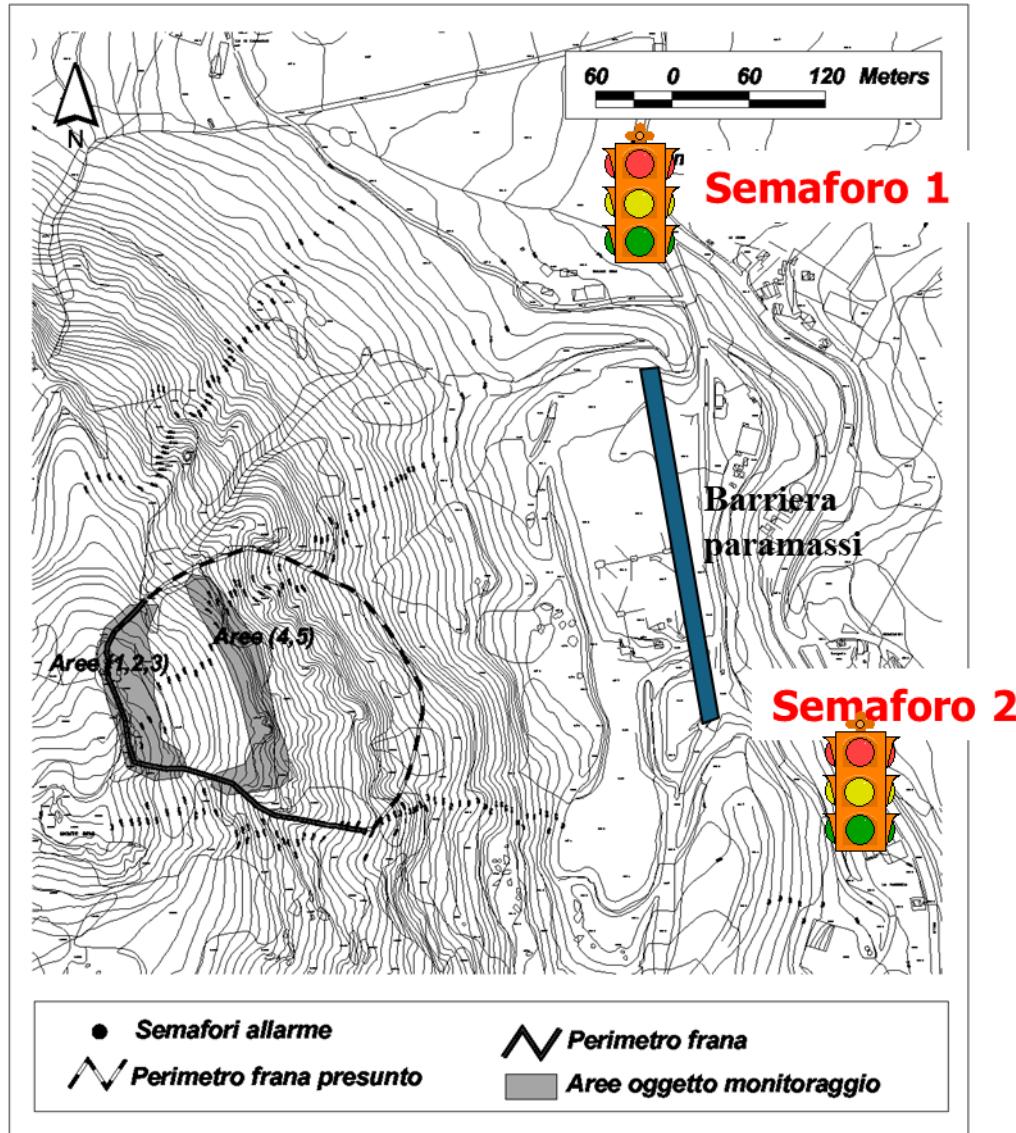
Intervallo di tempo:
124 h

Tempo di acquisizione:
40 min

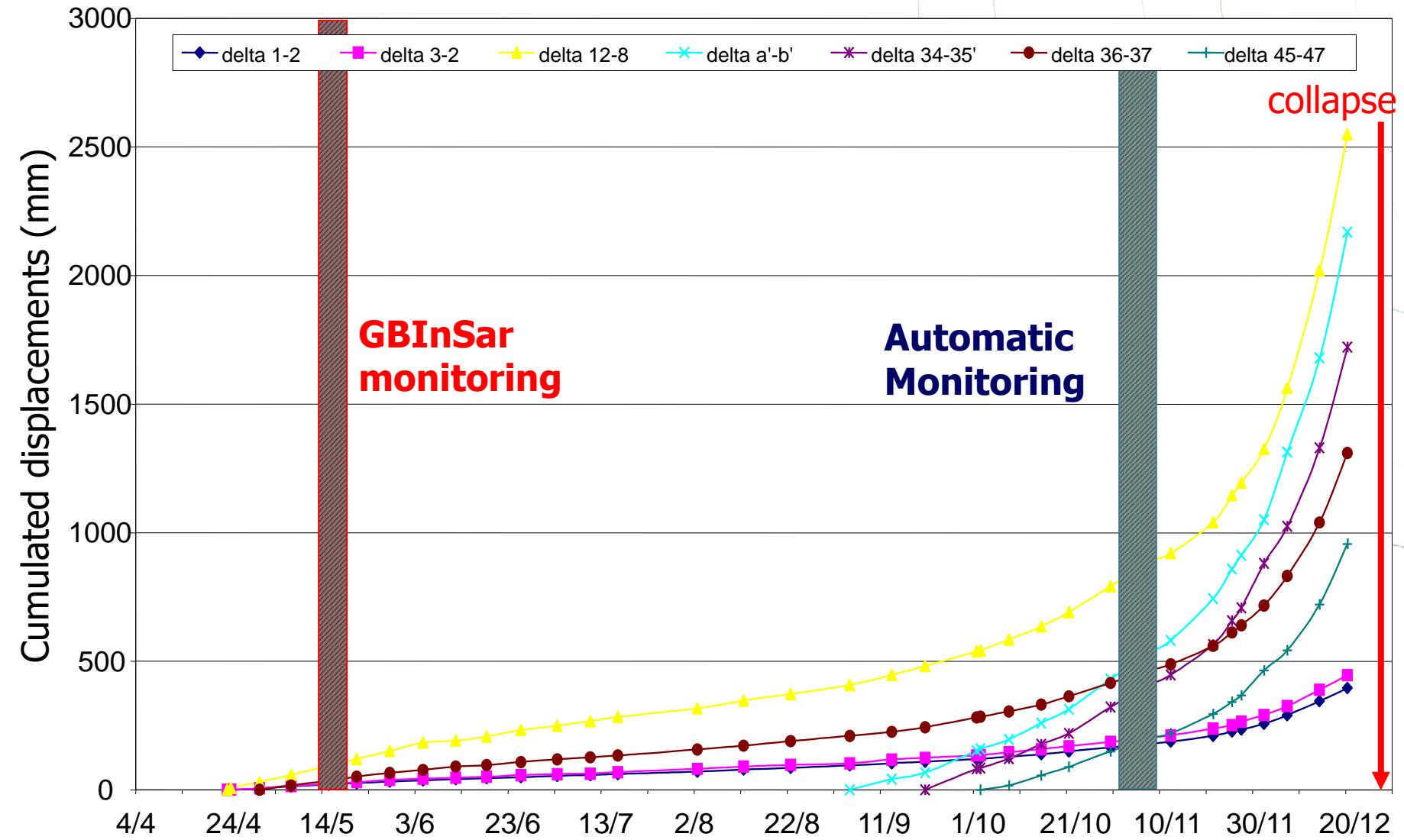
Velocità massima:
0.48 mm/h

Velocità media:
0.16 mm/h

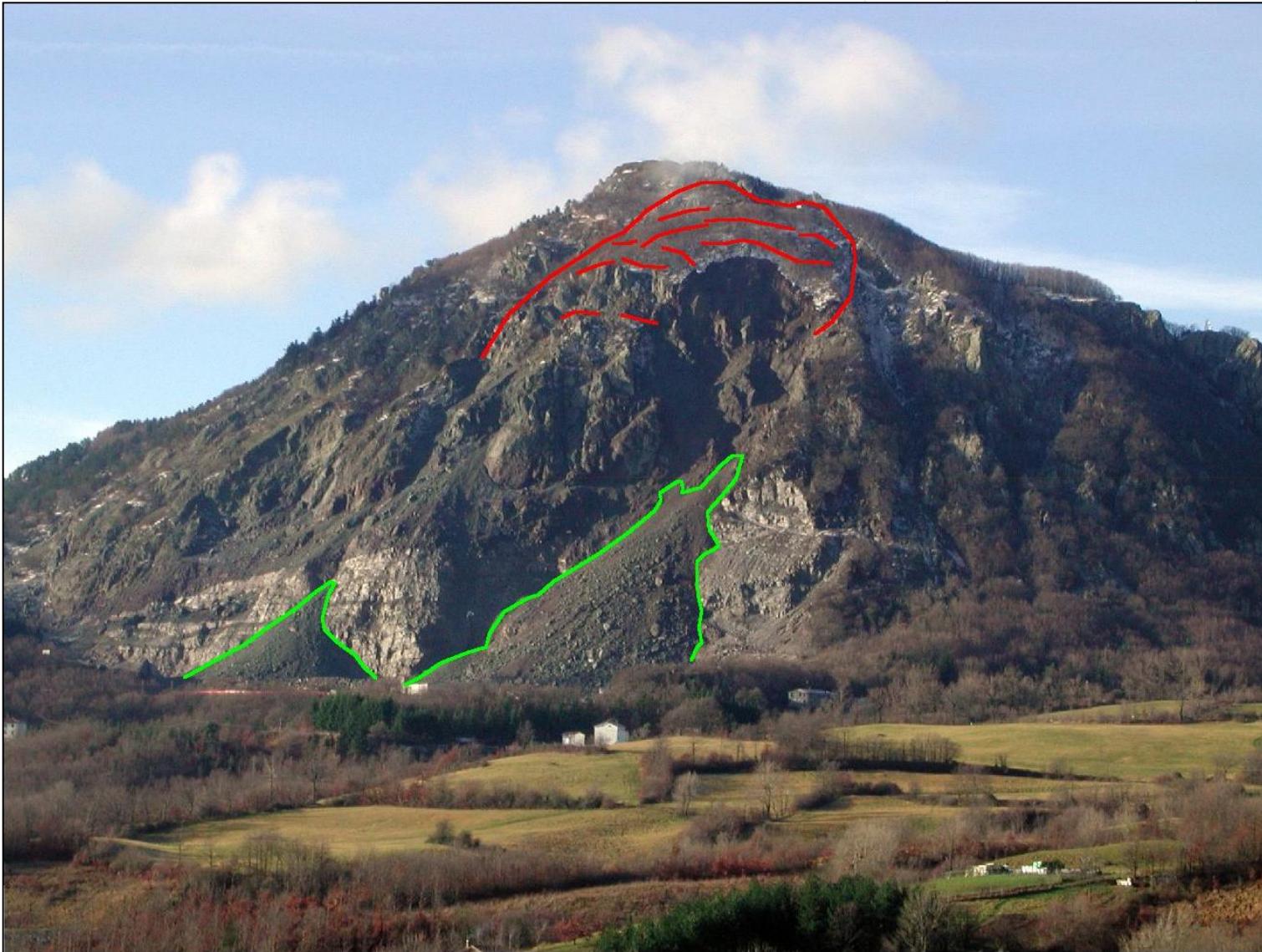
Emergency management



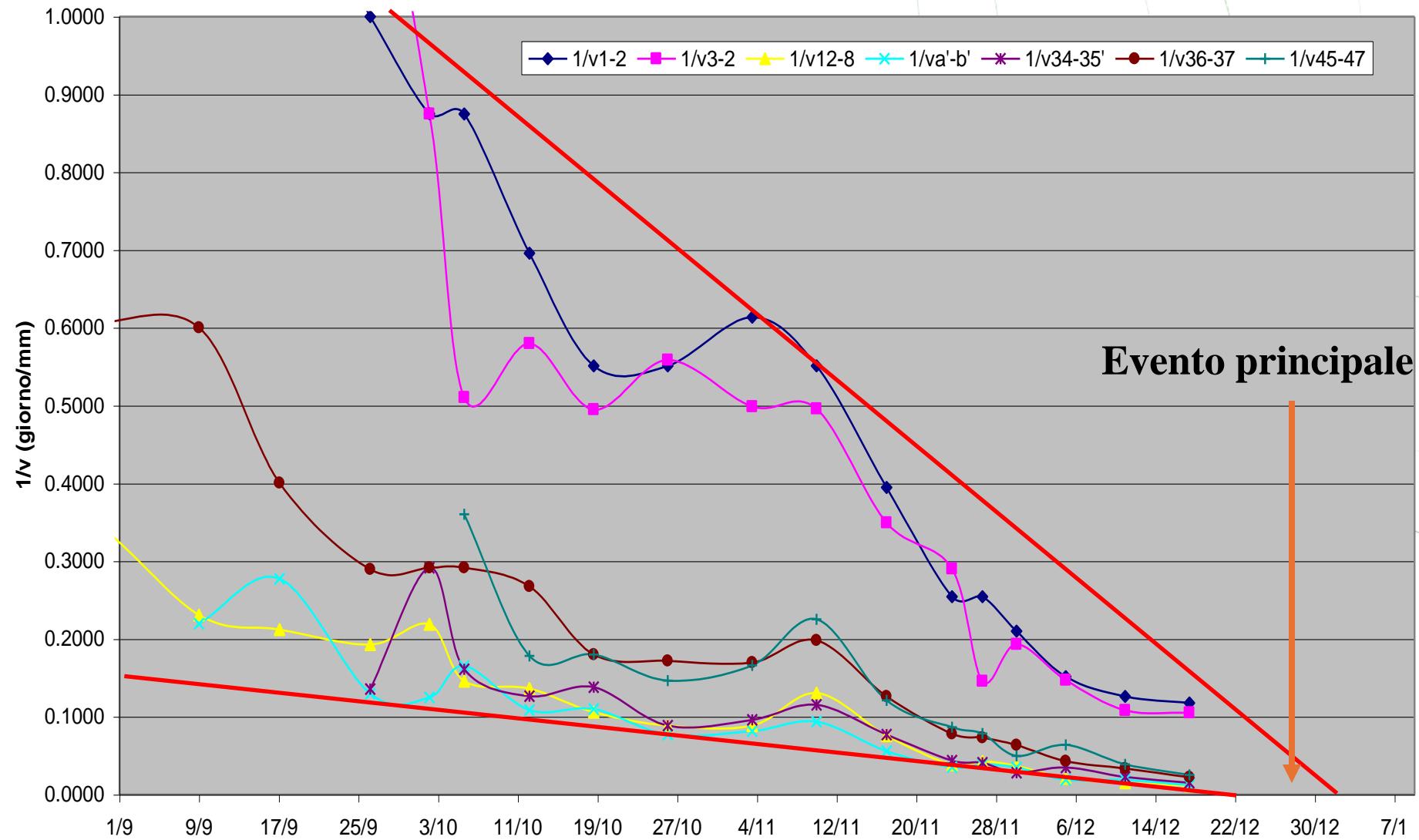
Monitoring - summary



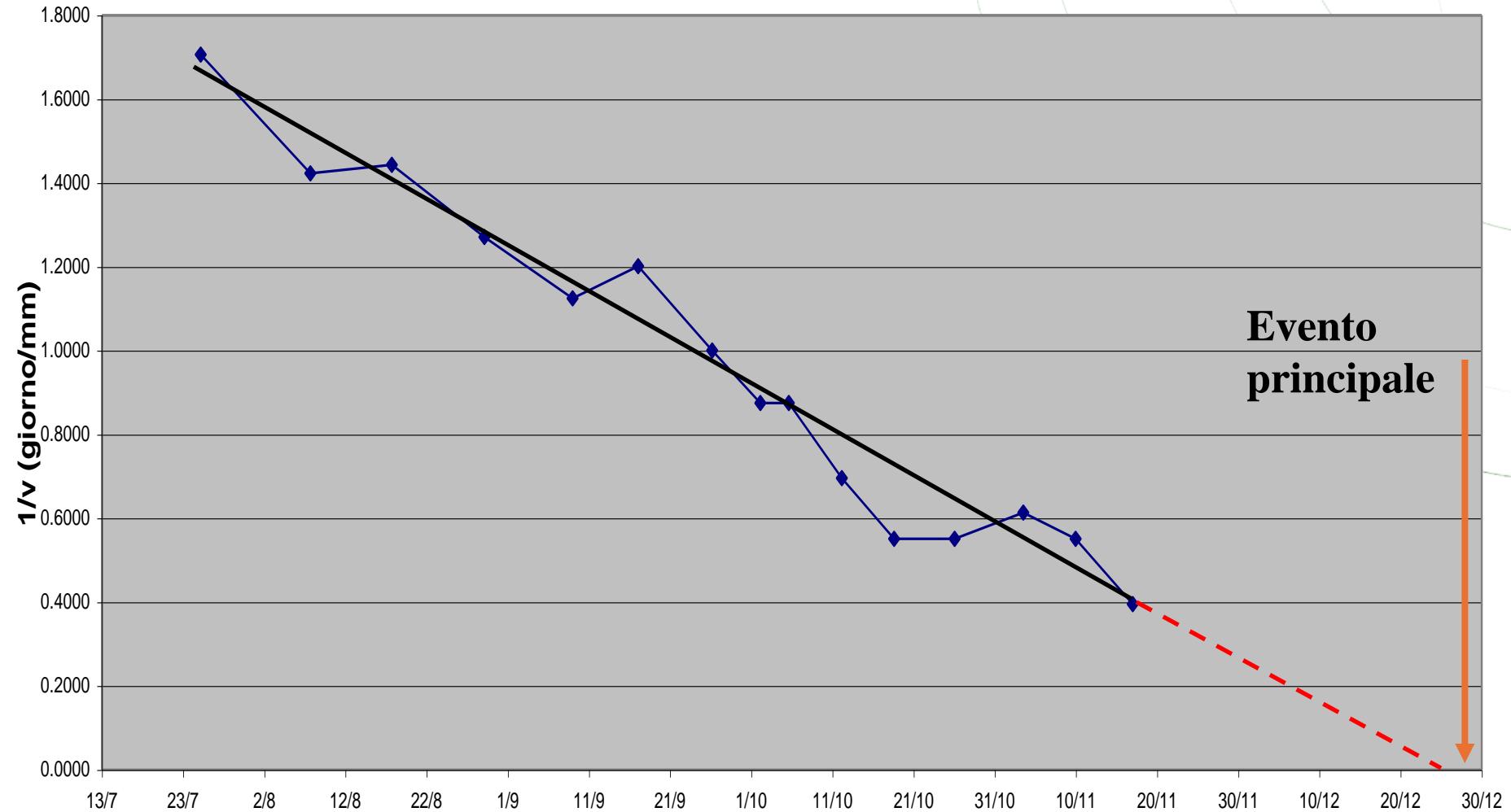
15/12/2002 event



Time of failure forecast



Time of failure forecast – baseline 1-2



- “... la frana, fino ad oggi sensibile alle precipitazioni meteoriche, sembra avere subito questa accelerazione in modo indipendente dalle precipitazioni...” (lettera del Prof. Canuti al Sindaco di Firenzuola, 26/11/02).
- “... il temuto collasso della “massa grande” è ormai prossimo: porre attenzione che nelle festività natalizie sia rispettata l’ordinanza di evacuazione.” (lettera del Prof. Canuti al Sindaco di Firenzuola, 23/12/02).
- “... la “massa grande” collasserà entro i primi giorni di gennaio 2003.” (Presentazione del Prof. Canuti alla Commissione Monte Beni del 27/12/02).

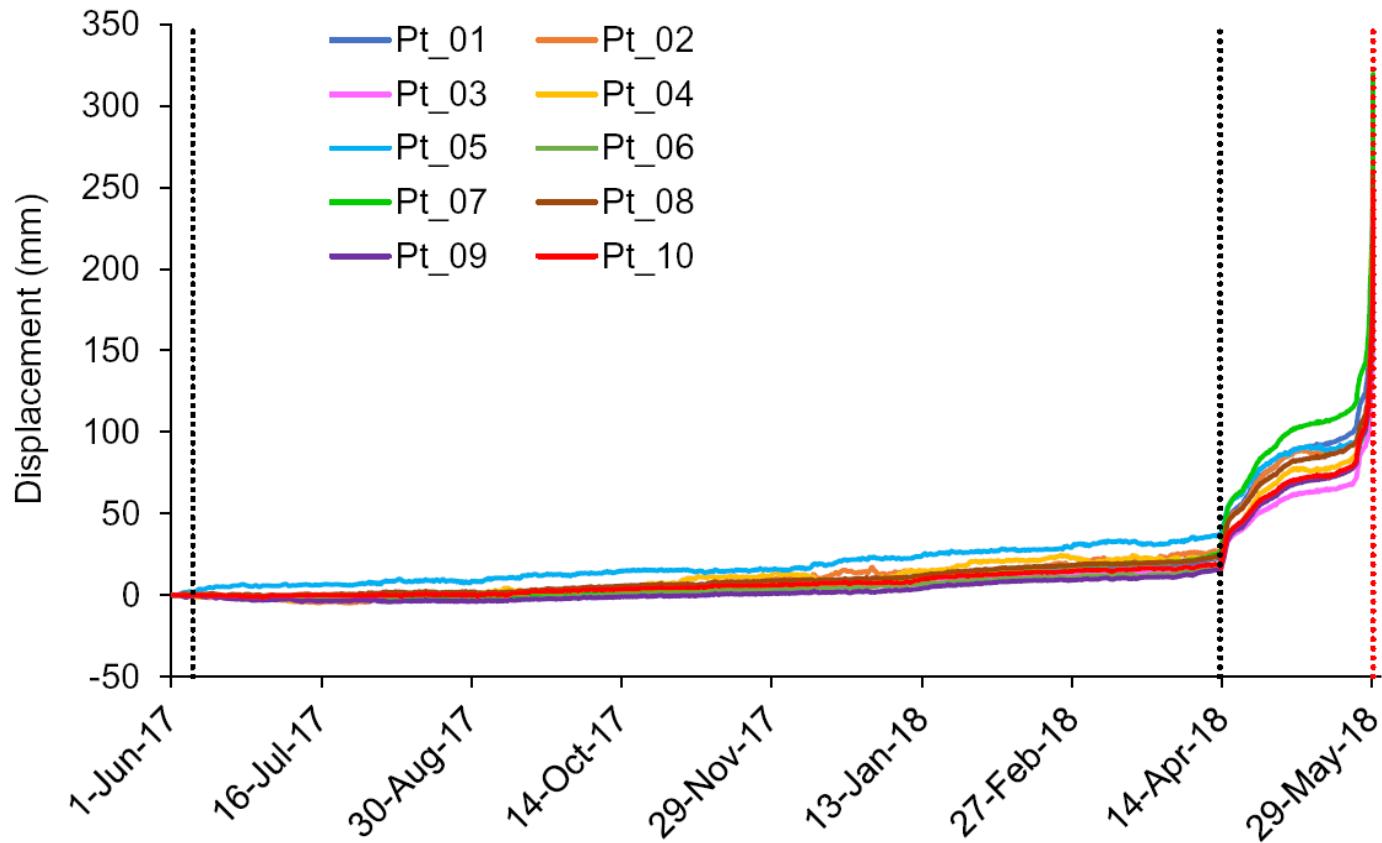
28/12/2002 landslide



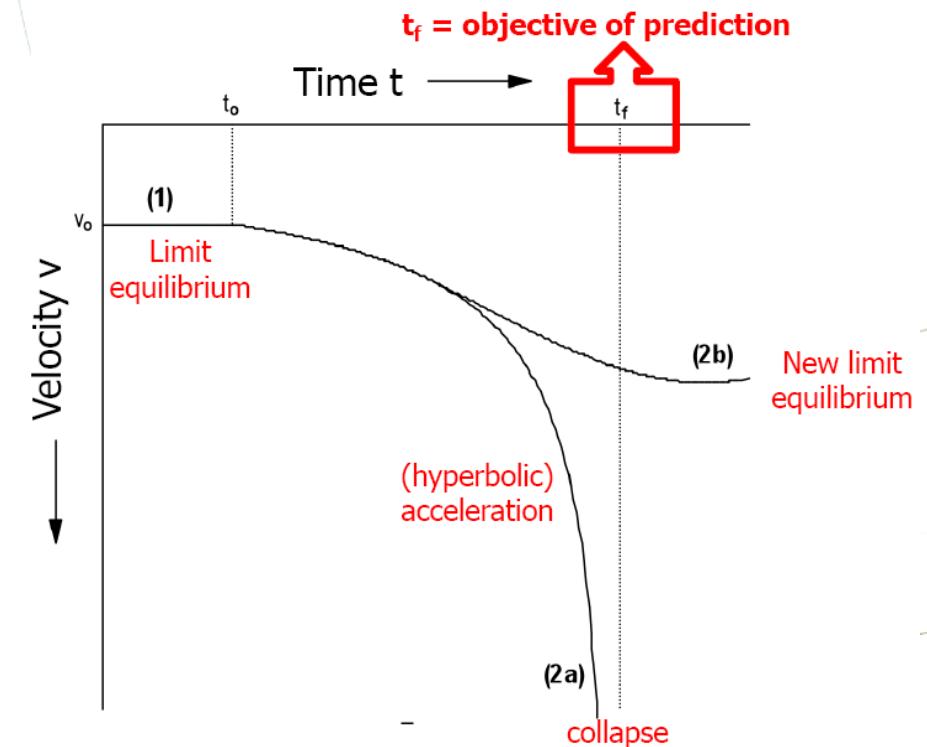
Gallivaggio landslide



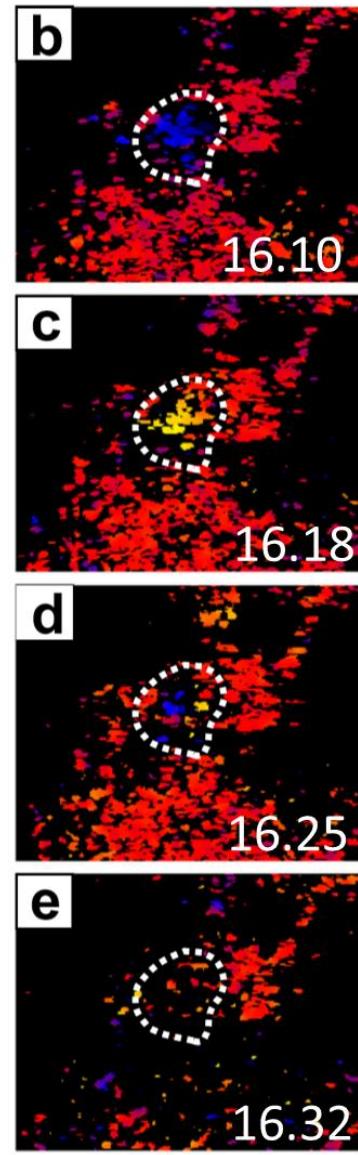
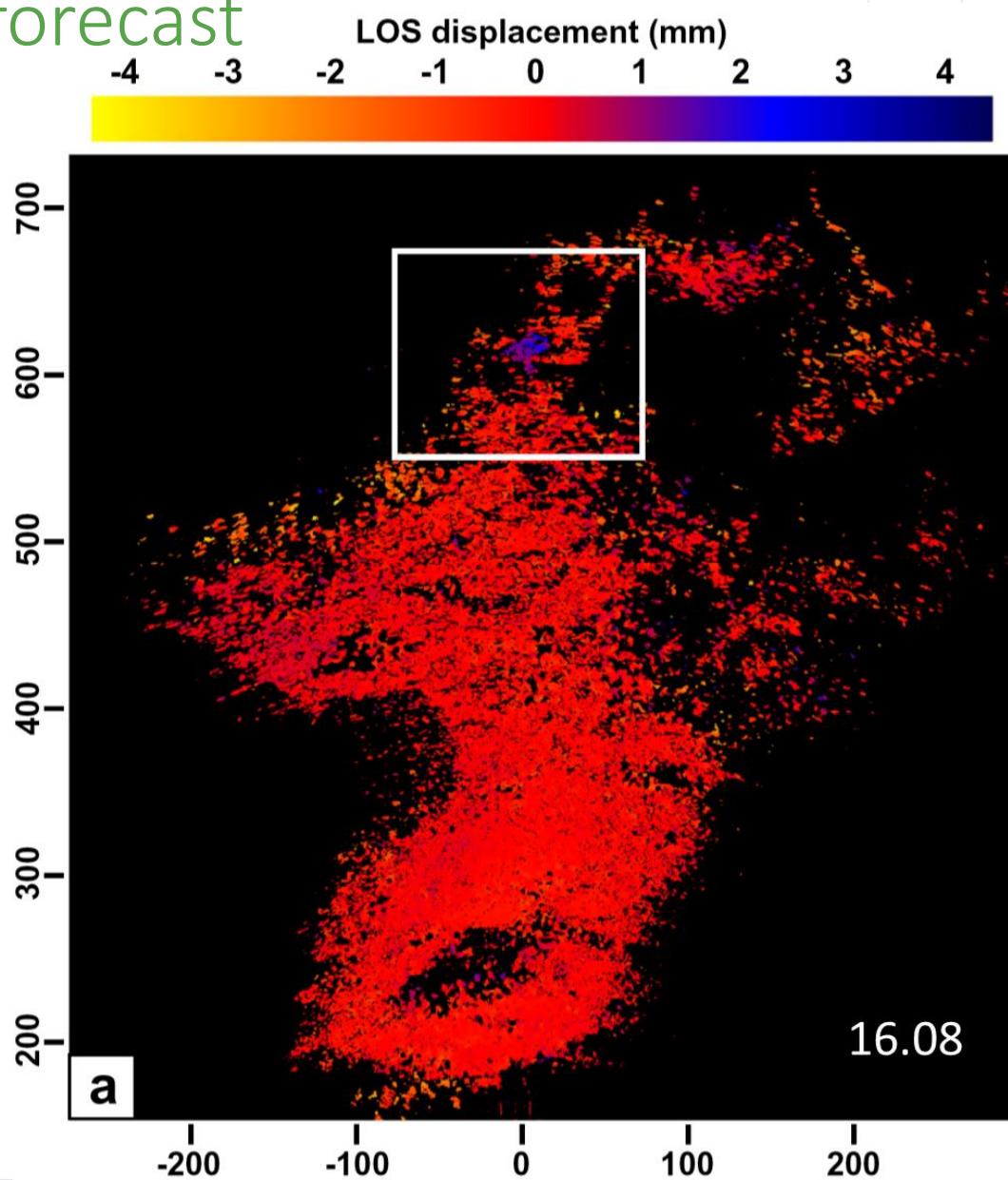
Time of failure forecast



Carlà et al., 2019

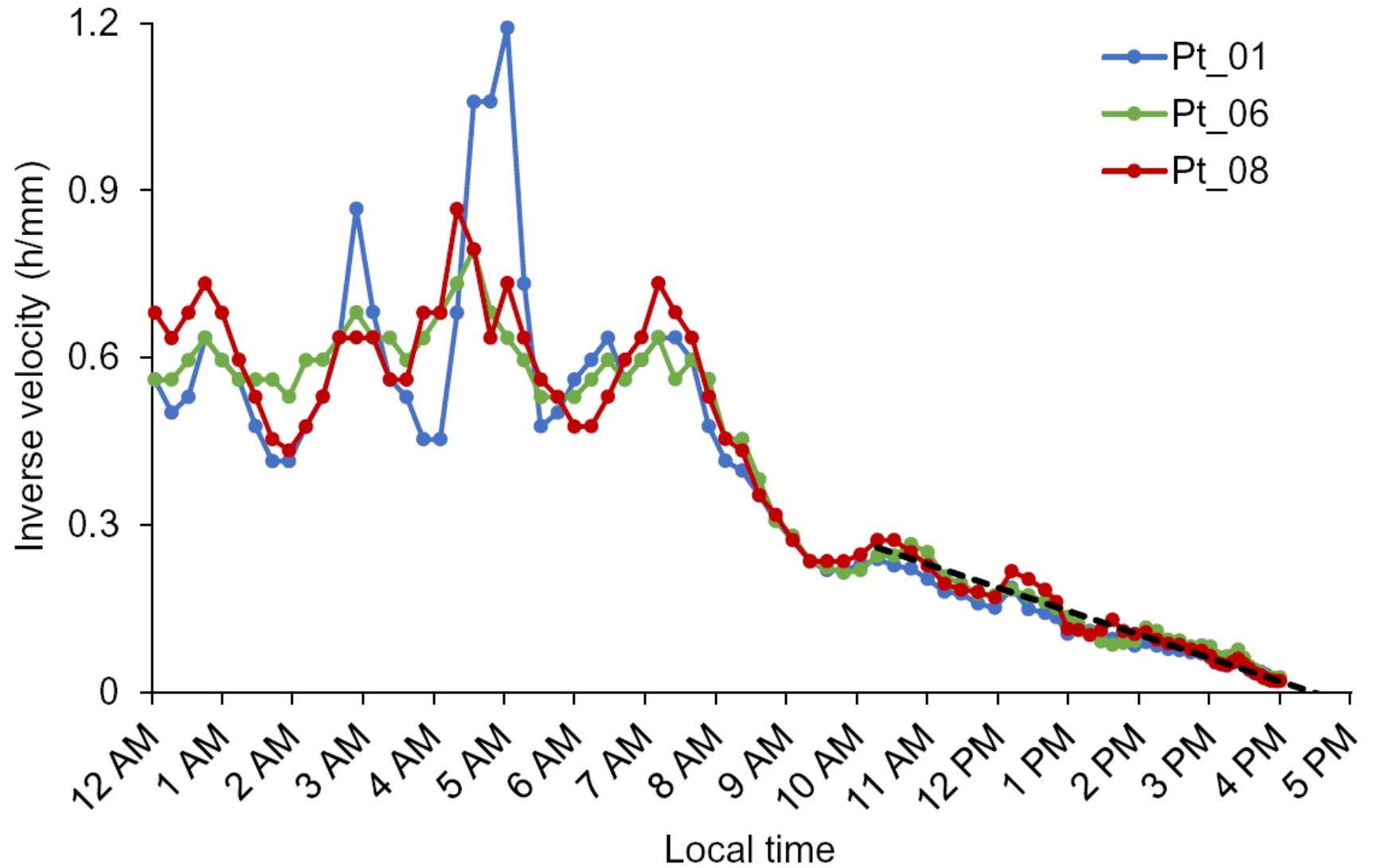


Time of failure forecast



Carlà et al., 2019

Time of failure forecast



Rock collapse



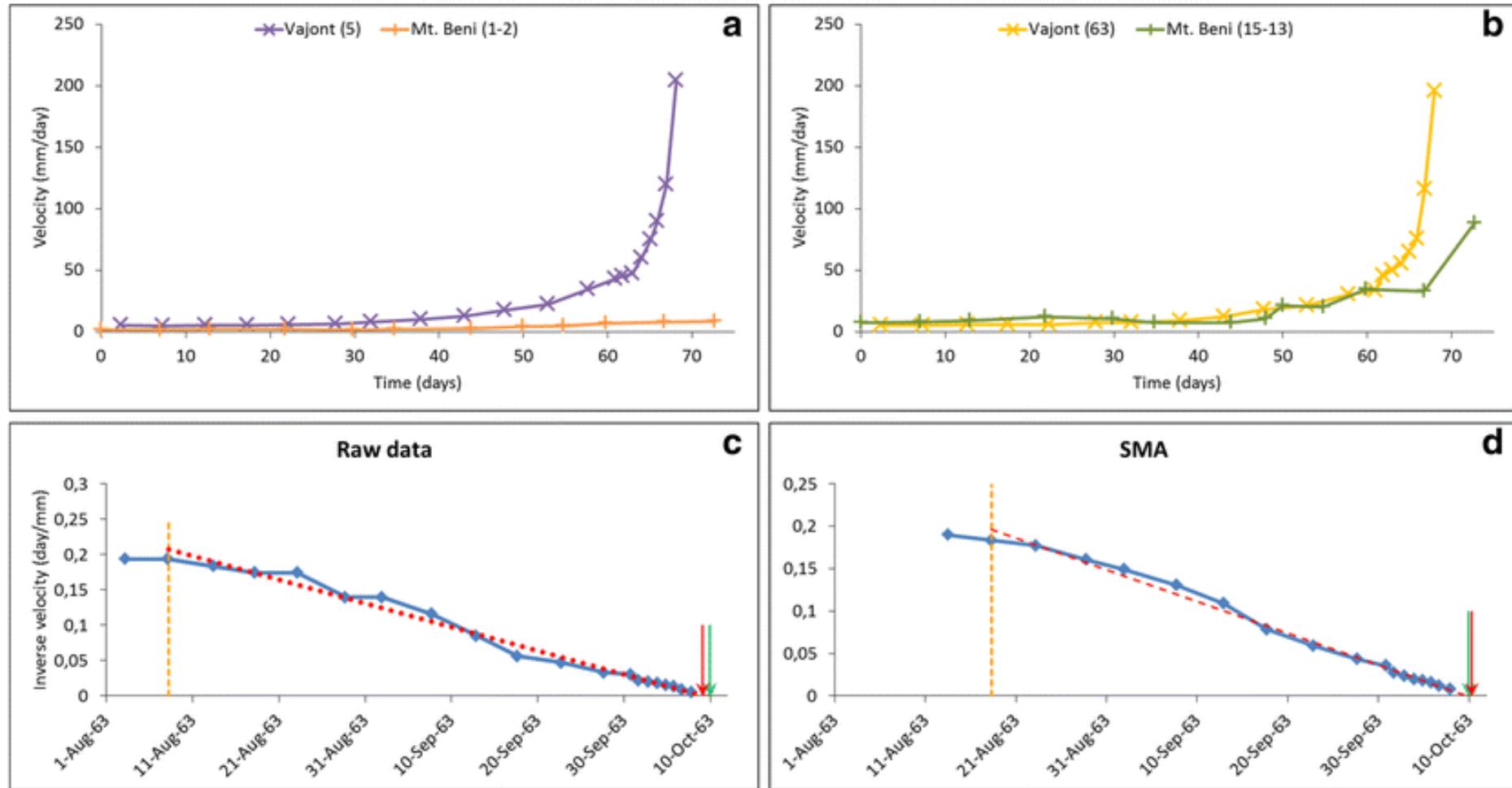
Mt. Toc (Vajont)



Mt. Toc (Vajont)

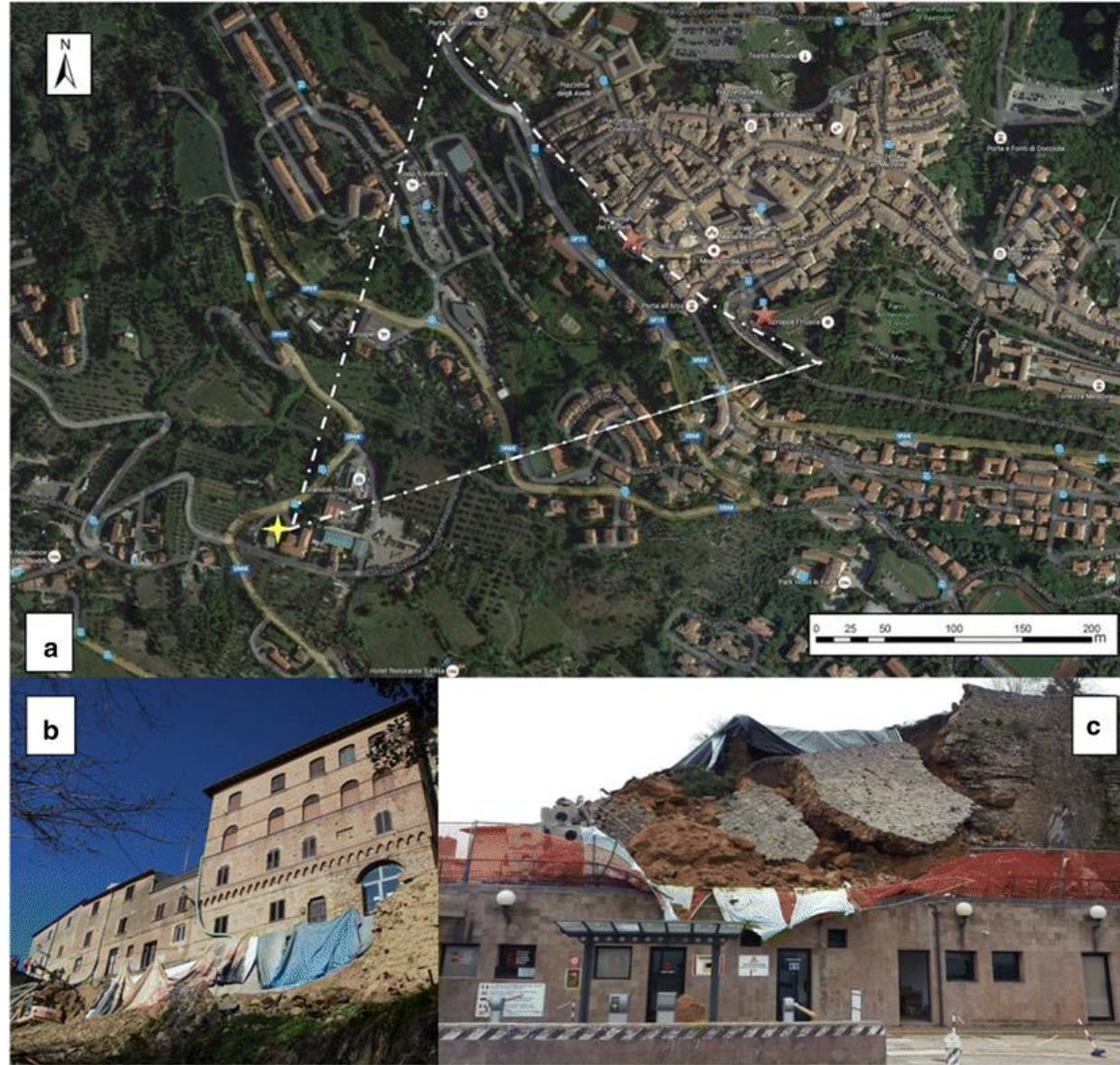
DISPLACEMENT RATES AND INVERSE VELOCITY ANALYSIS - BENCH MARK 63 (VAJONT)

— Inv. vel. ← Actual failure ← Predicted failure — Onset Of Acceleration



Carlà et al., 2017

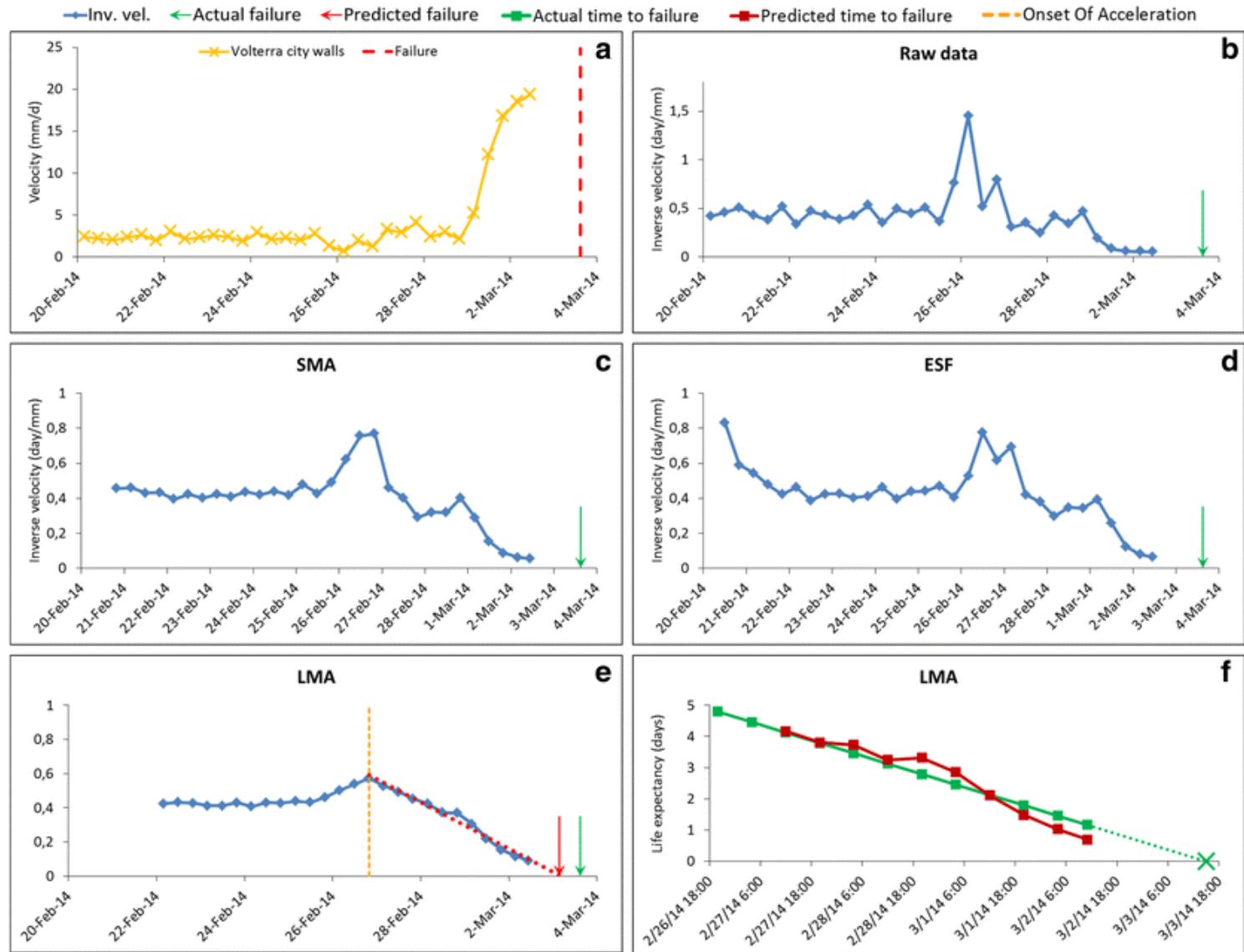
Volterra medieval city wall



Carlà et al., 2017

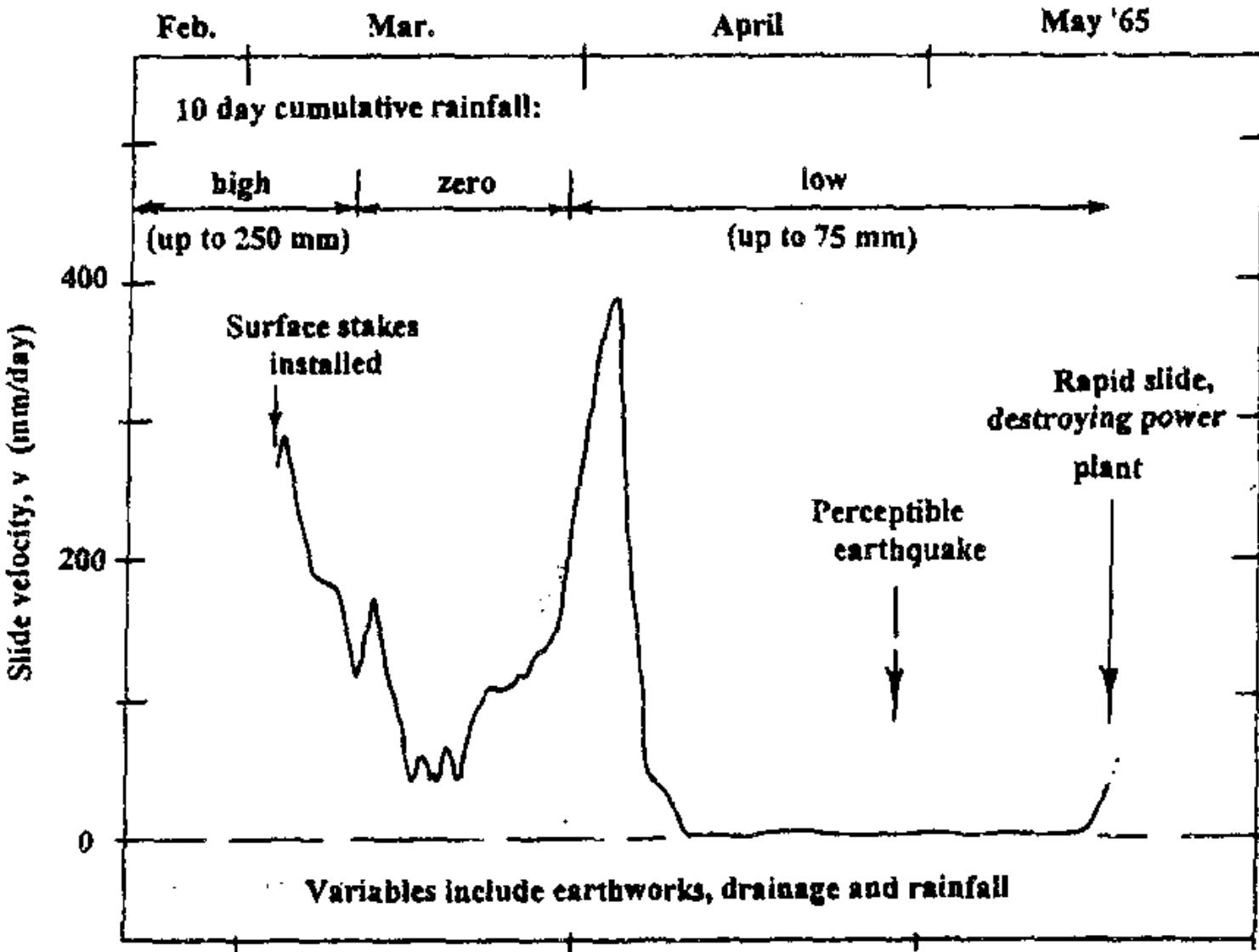
Volterra medieval city wall

DISPLACEMENT RATES AND INVERSE VELOCITY/LIFE EXPECTANCY ANALYSES – VOLTERRA CITY WALLS



Carlà et al., 2017

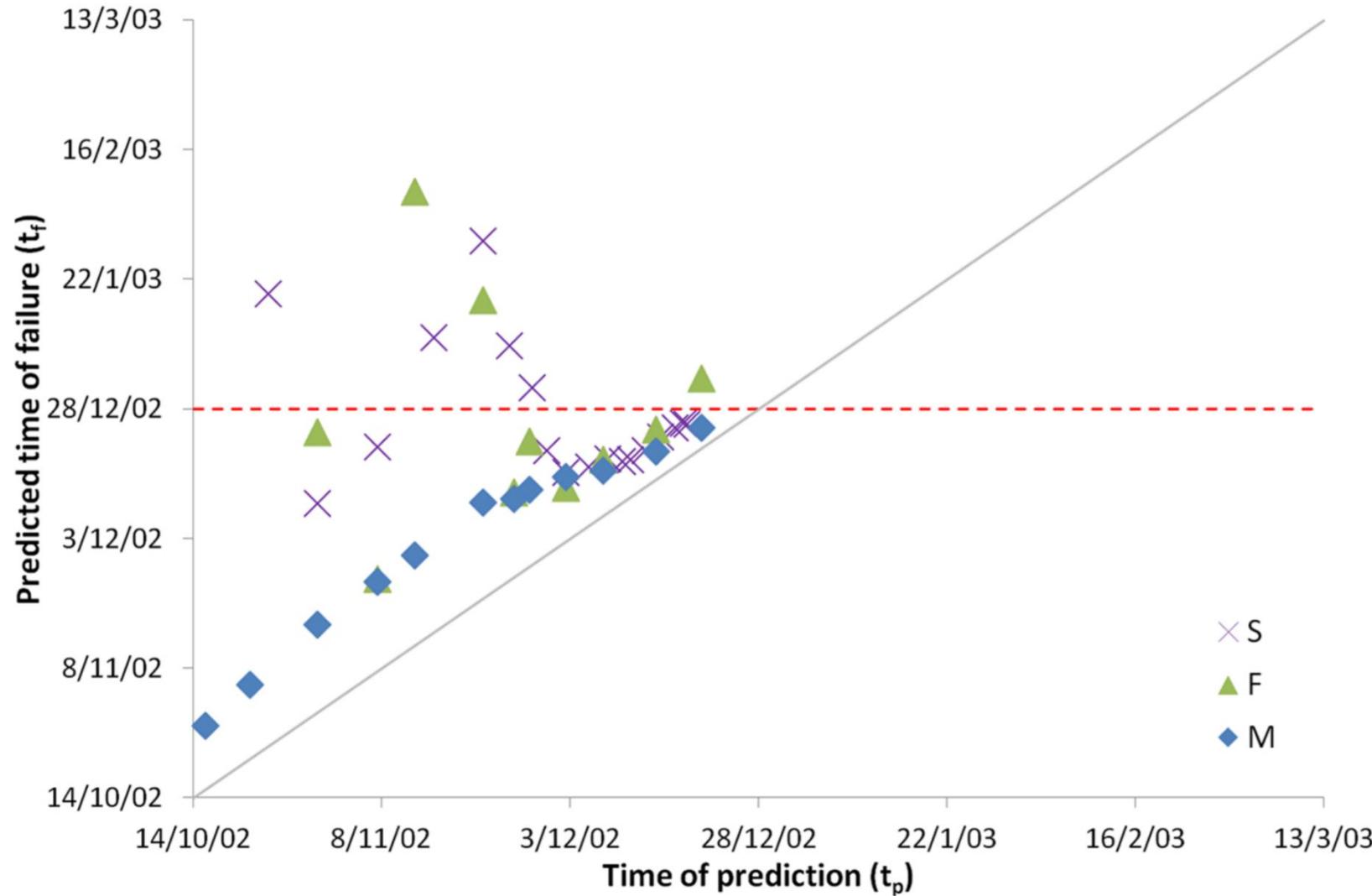
Unexpected failure



- Measurement error
- Random noise
- Local movements
- Anthropic activity
- Earthquakes
- Meteorologic factors
- Structural constraints
- Ductile Behaviour
- Invalid assumptions

Hutchinson (2001)

Probabilistic approach



Thershols and actions

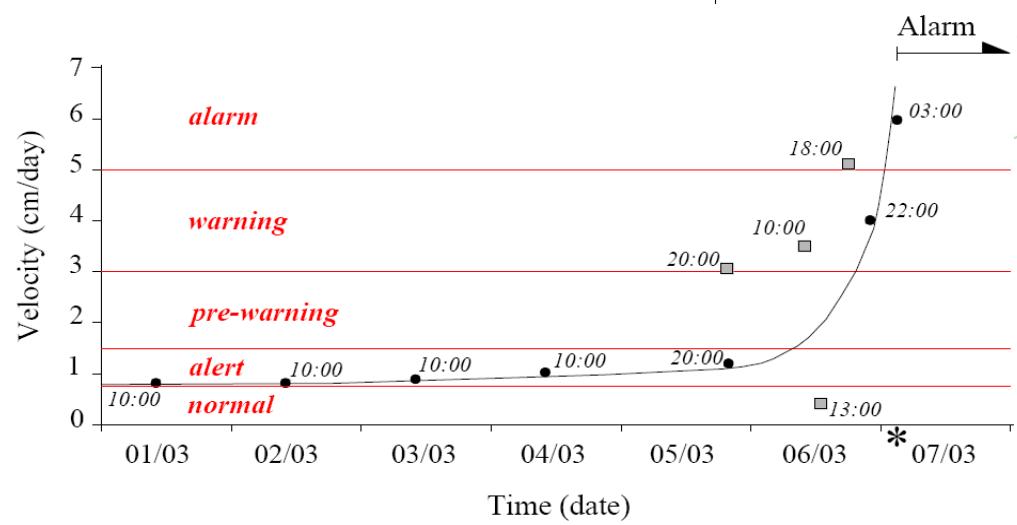
NOTHING SPECIAL	BE AWARE	BE PREPARED	TAKE ACTION
Stable or constant velocity	Start of acceleration	Sustained acceleration	Asymptotic acceleration
Weekly reports	Daily reports	Hourly reports	Continuos reports
			

Site-specific empirical thresholds

Alert level	Velocity (cm/day)	Status	Monitoring
0	$v < 0.2$	Normal	1/month
0	$0.2 < v < 0.4$	Normal	1/10days
0	$0.5 < v < 1.5$	Normal	1/day
1	$0.5-1 < v < 1.5-3$	Alert	1/day
2	$1-2.5 < v < 3-5$	Pre-warning	1/day
3		Warning	1/day

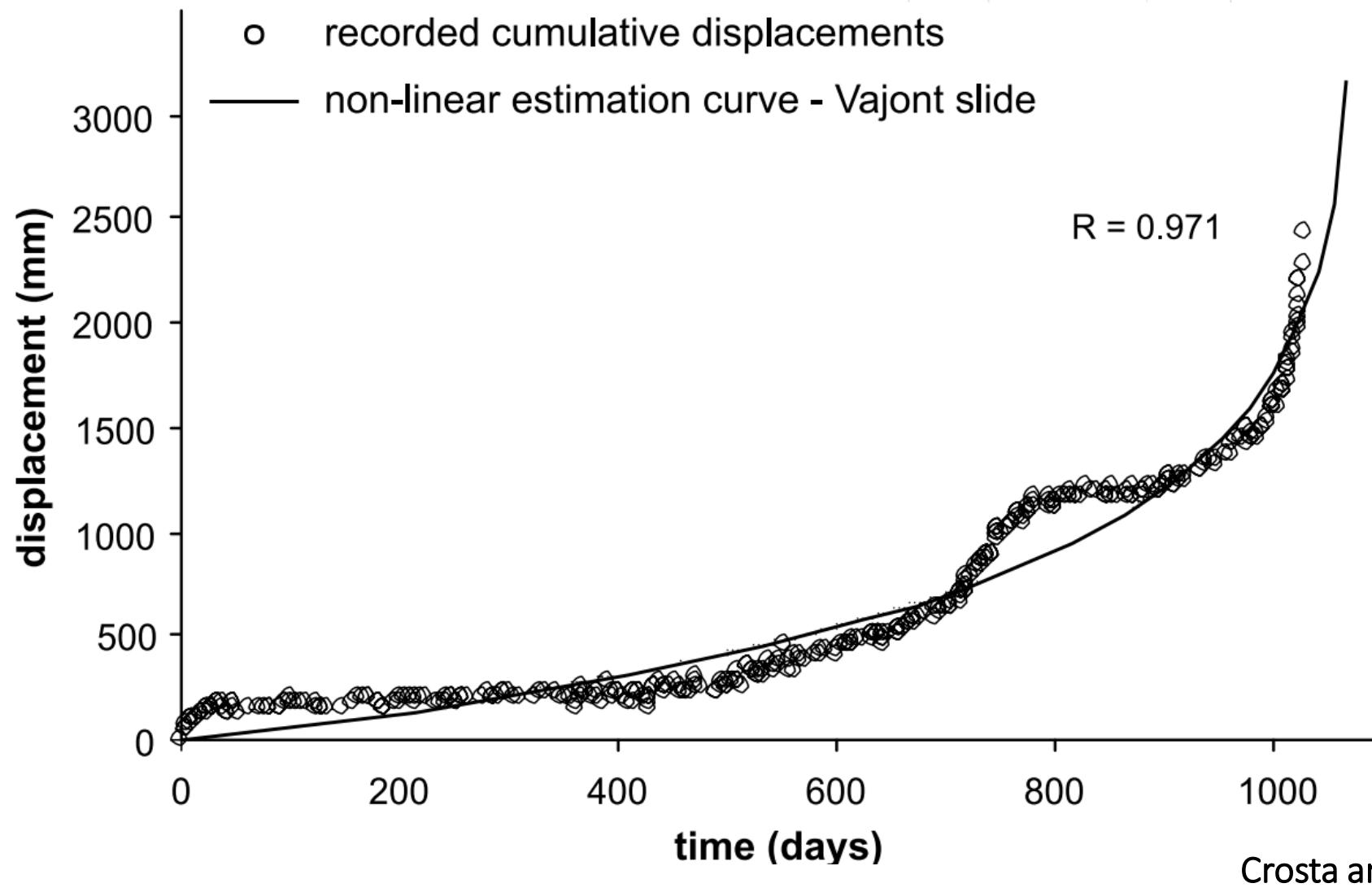
(Oboni, 1988)

Status	Maximum punctual velocity (cm/day)
Normal	$v < 0.75$
Alert	$0.75 \leq v < 1.5$
Pre-warning	$1.5 \leq v < 3.0$
Warning	$3.0 \leq v < 5.0$
Alarm	$5.0 \leq v$

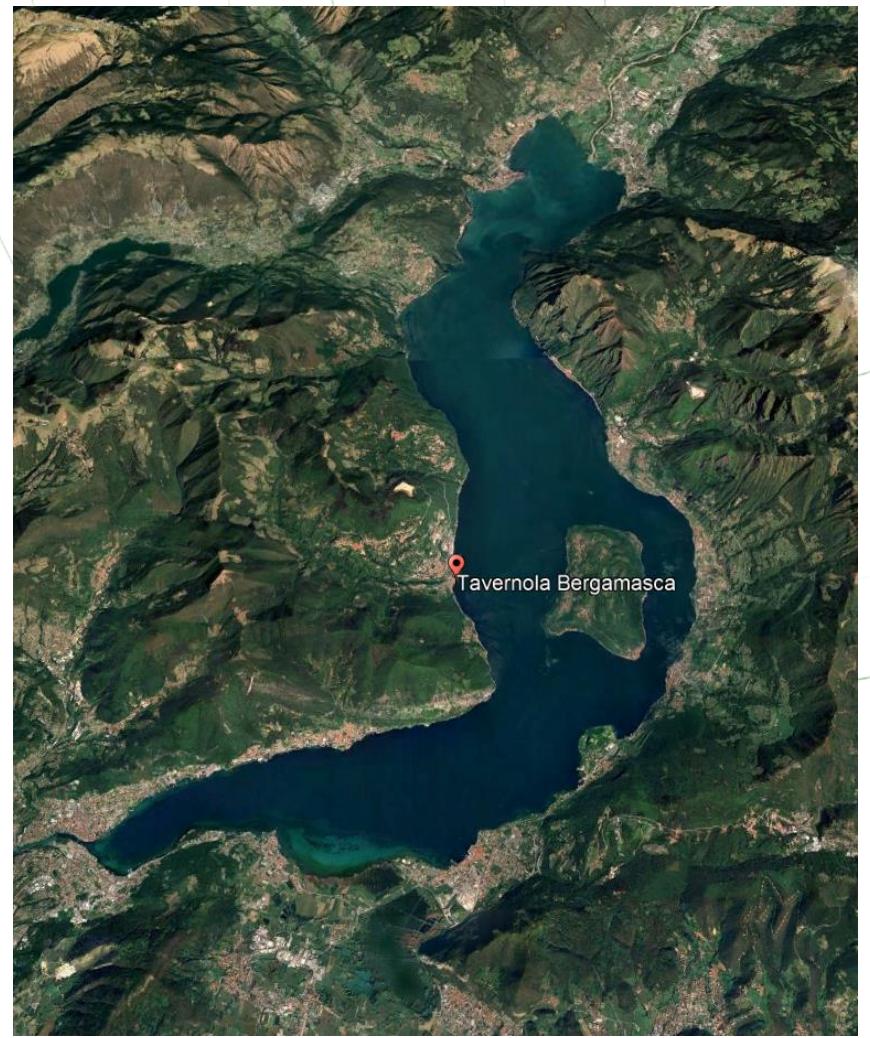


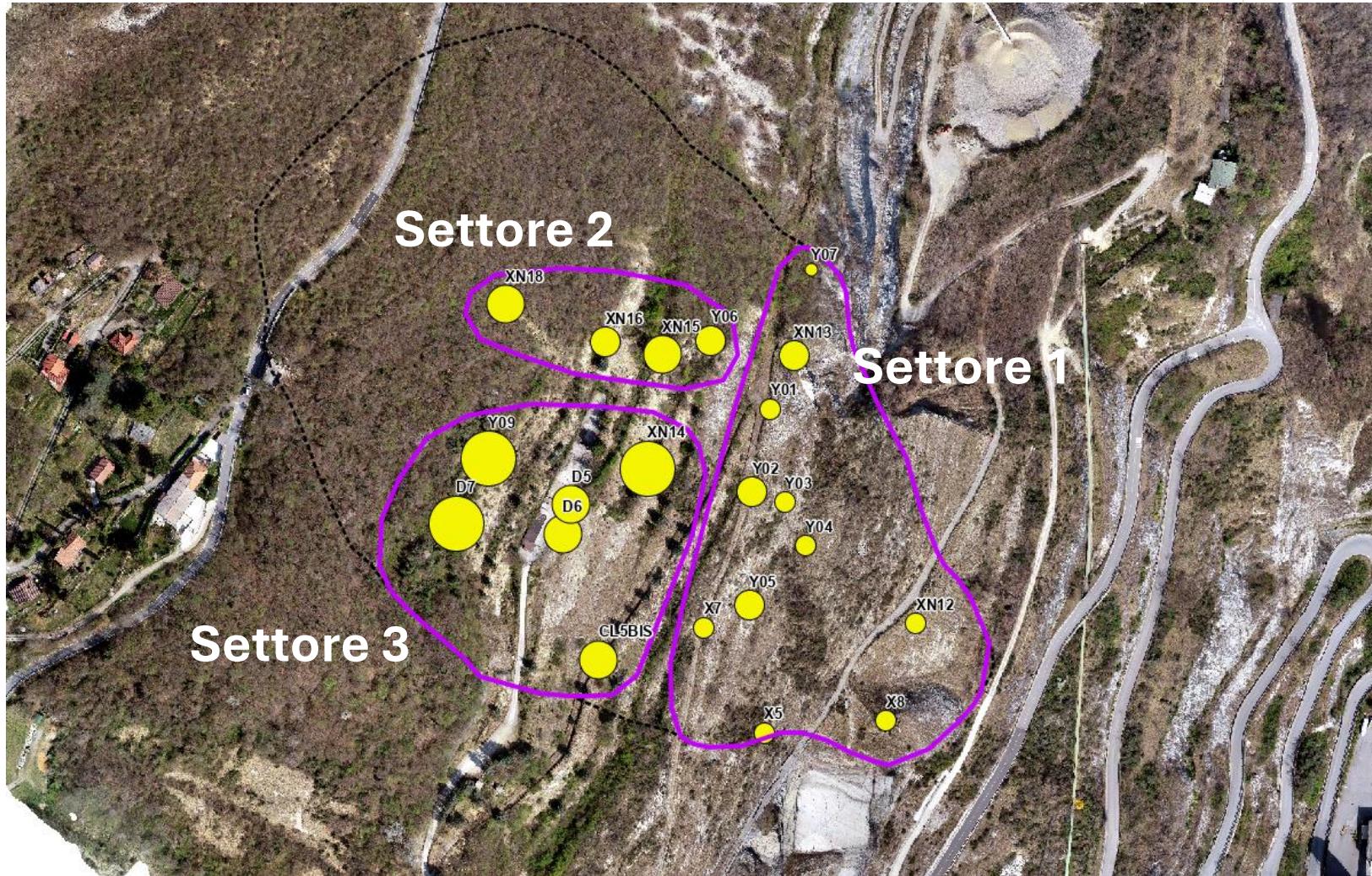
(Irvine et al., 2006)

Thresholds definition



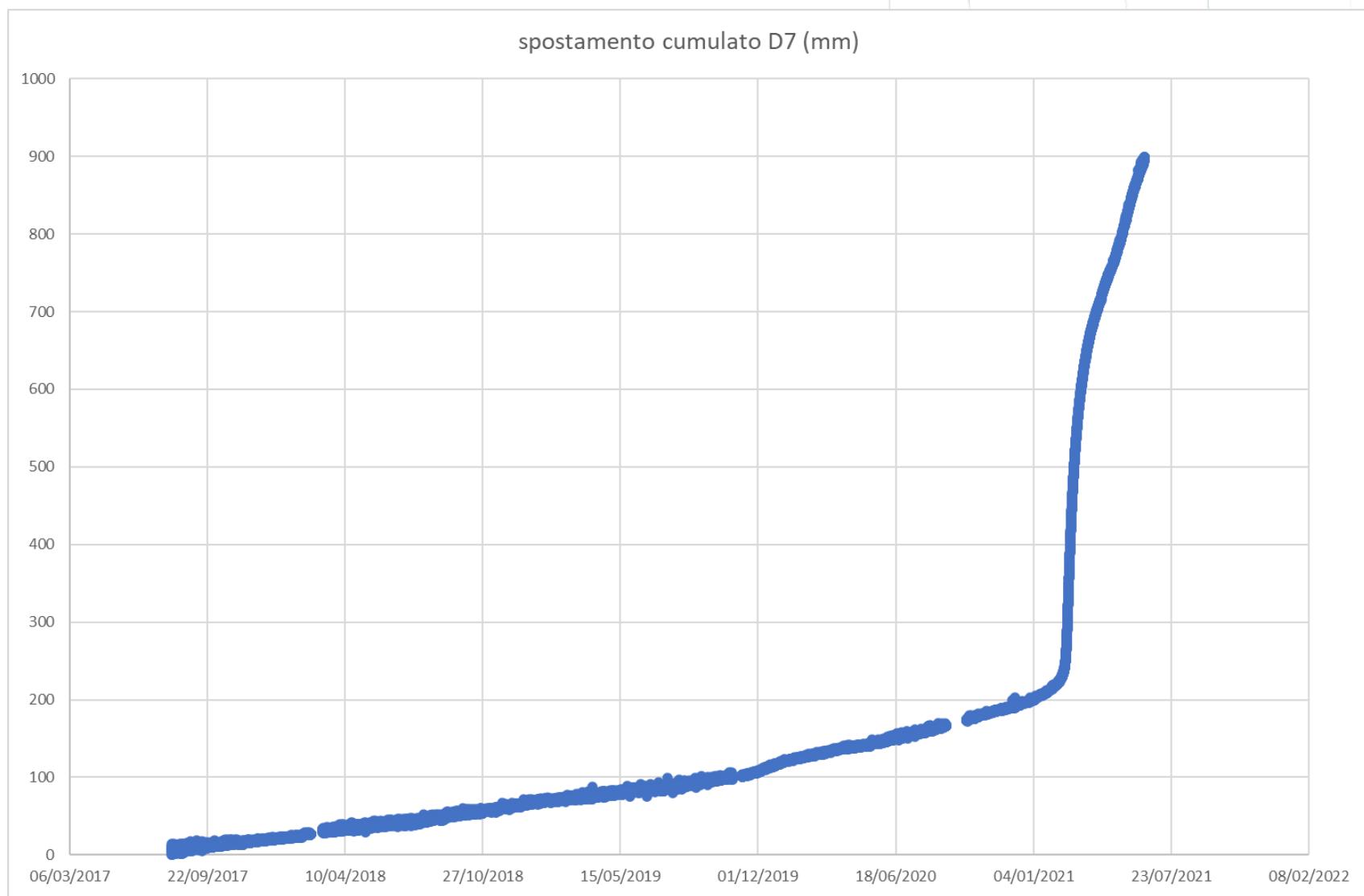
Tavernola Landslide



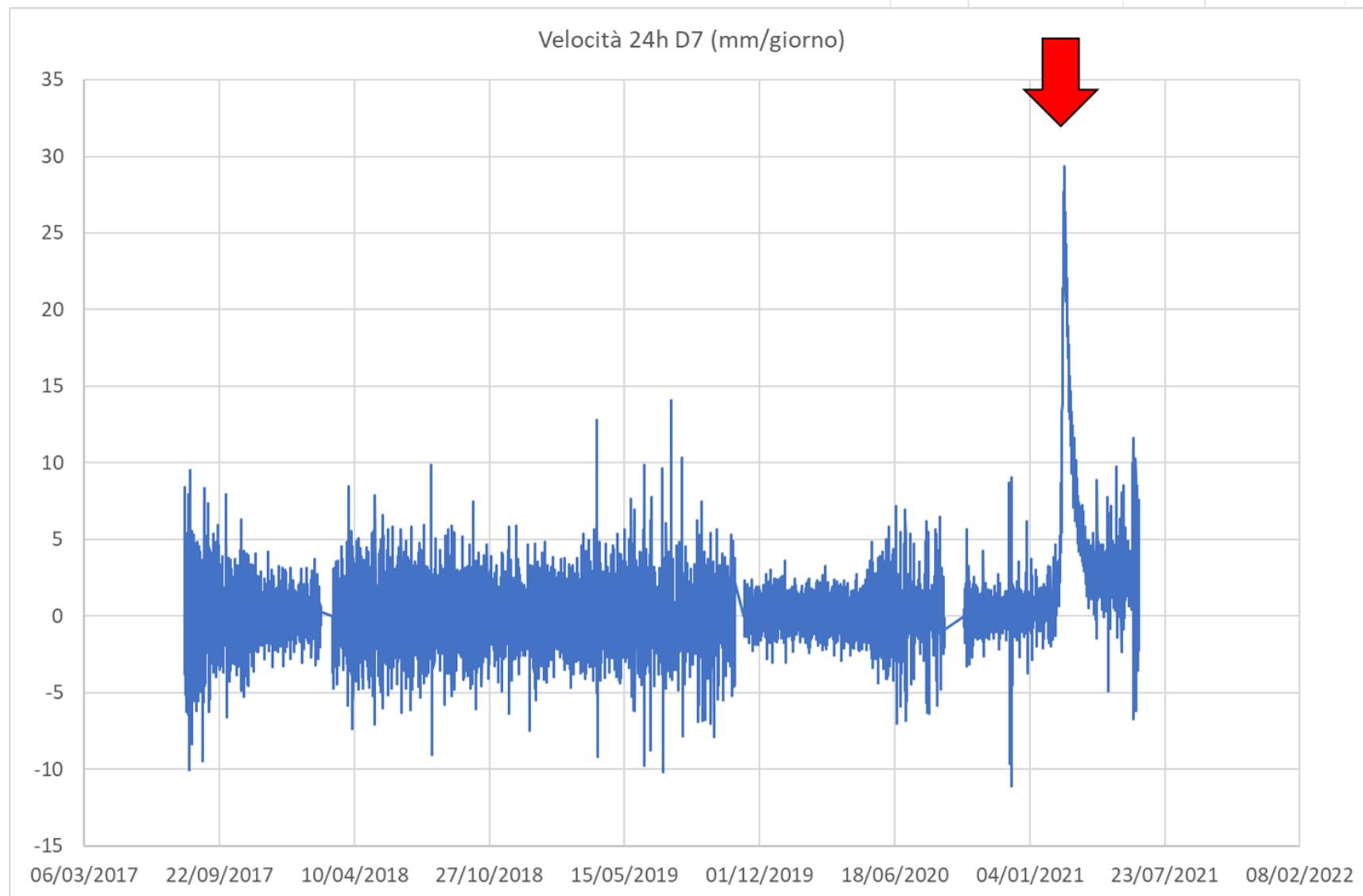


Nota: la distribuzione dei prismi si riferisce alla situazione del mese di febbraio 2021

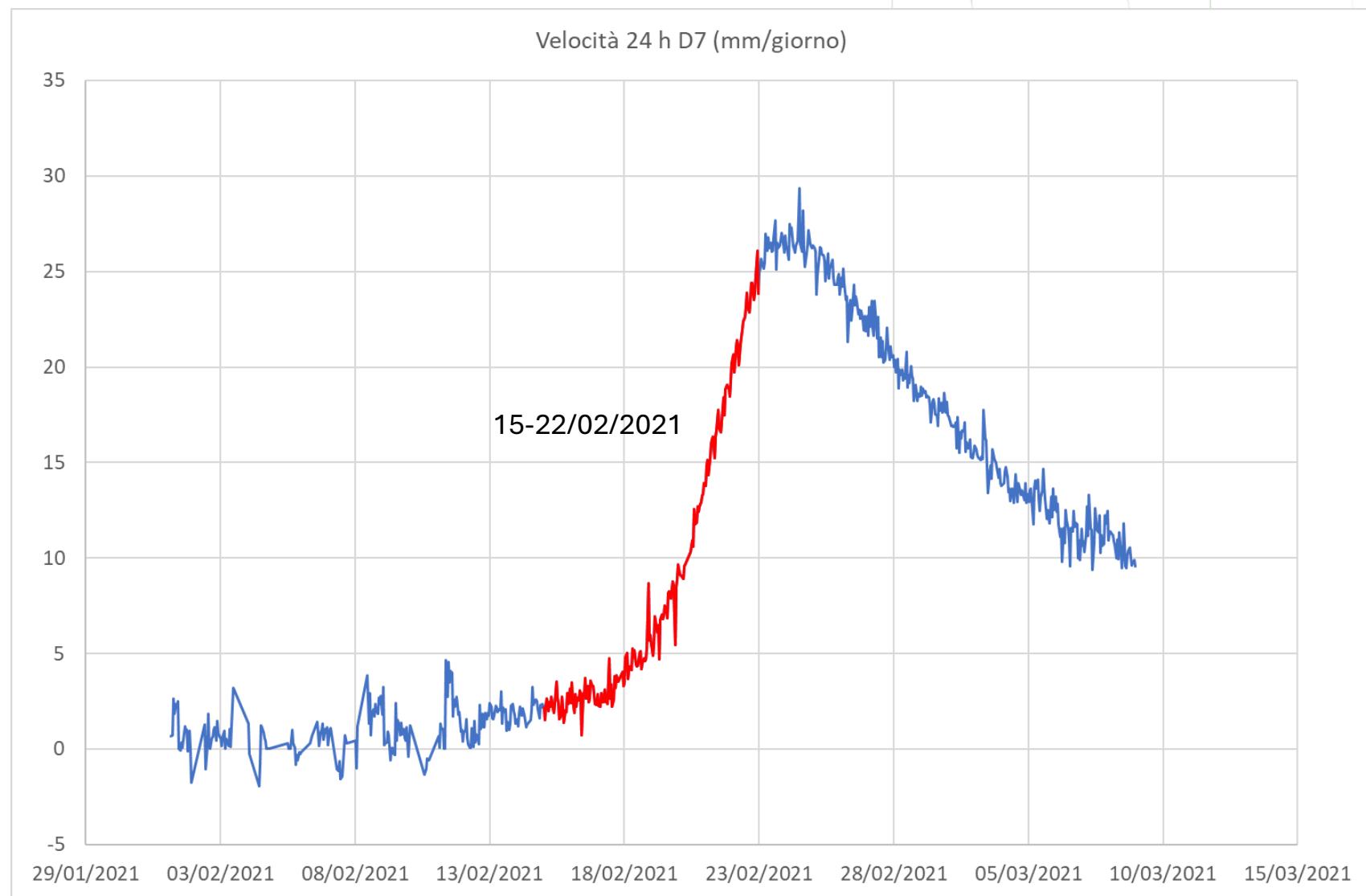
Cumulated displacement at D7



24h Velocity at D7



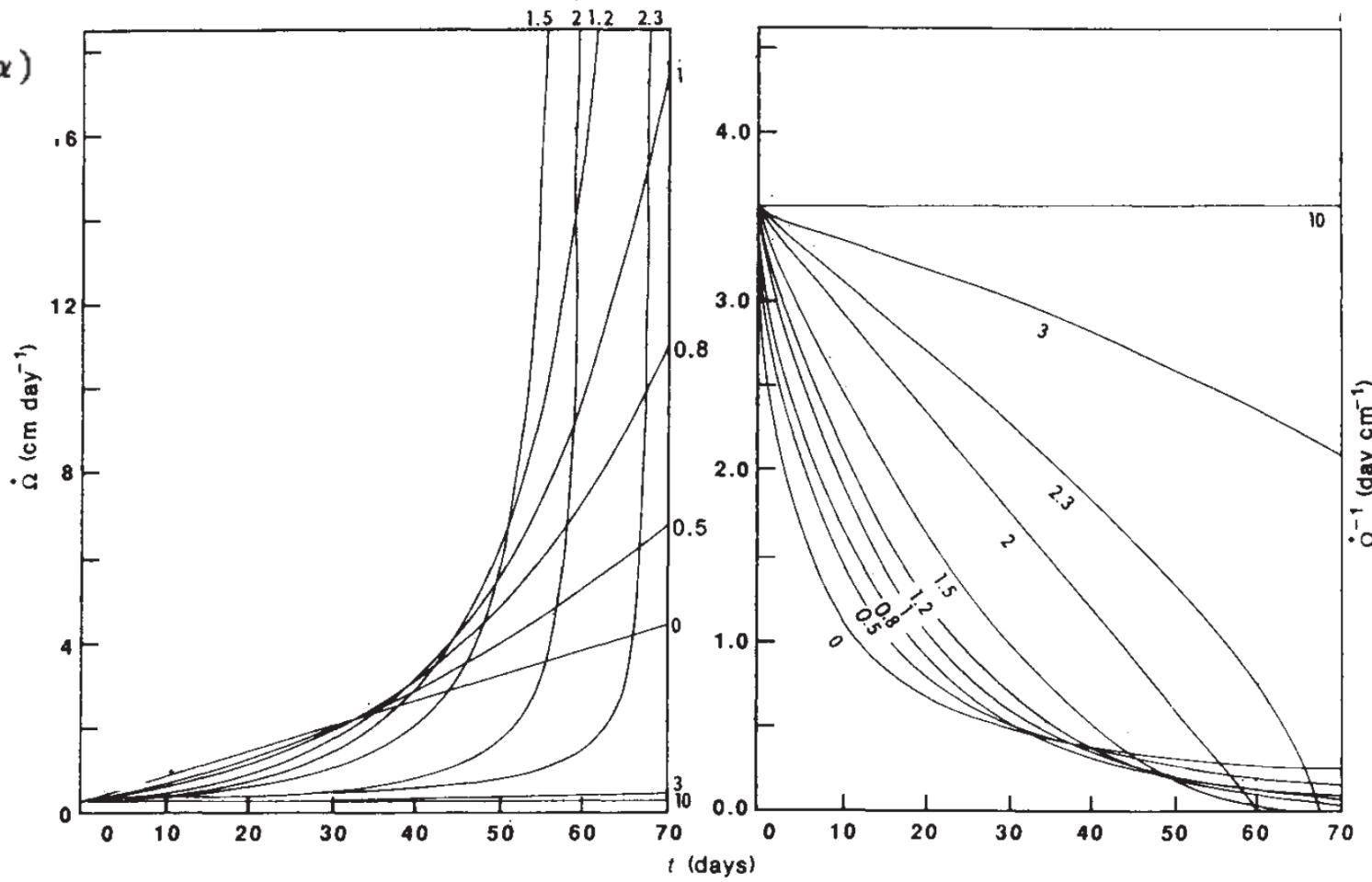
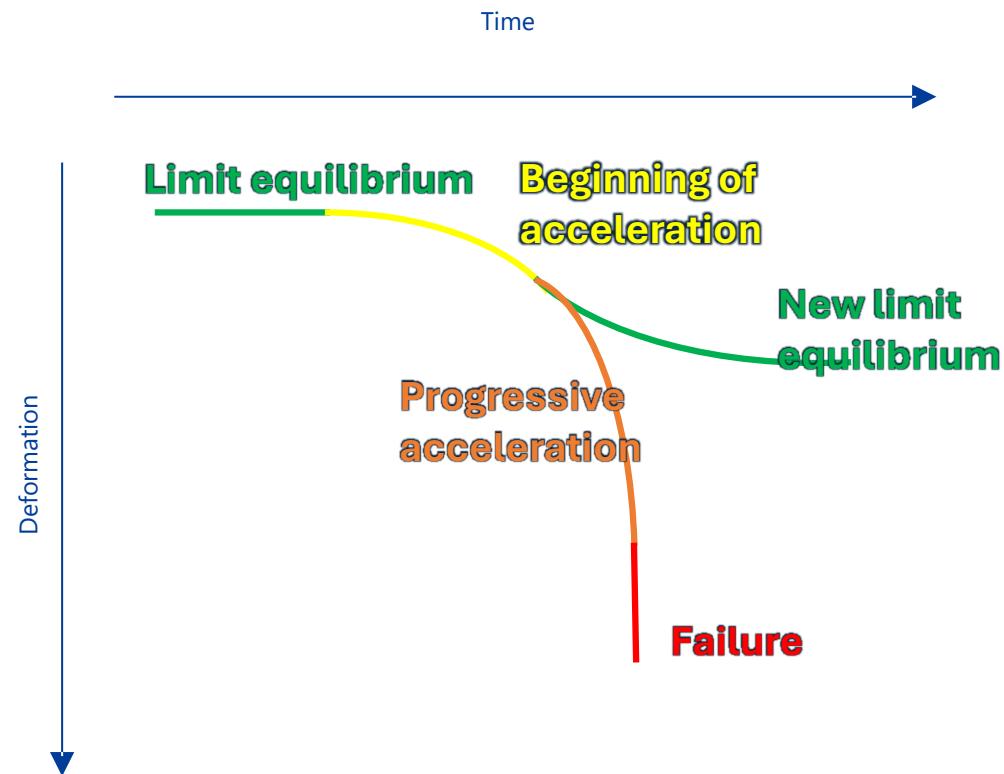
Selected time span



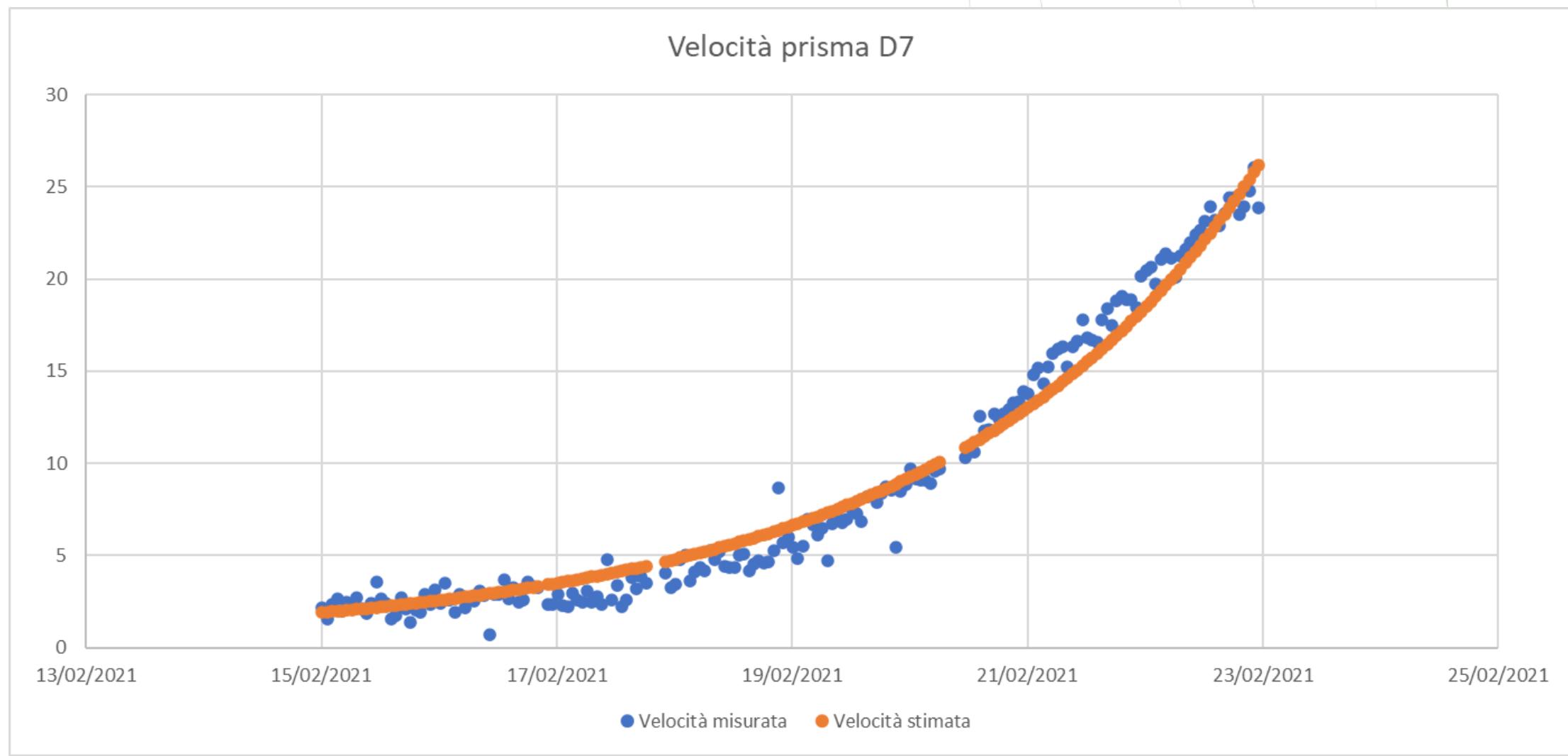
Non linear fitting

$$\dot{\Omega}^{-\alpha} \ddot{\Omega} - A = 0$$

$$\dot{\Omega} = [A(\alpha - 1)(t_f - t) + \dot{\Omega}_f^{1-\alpha}]^{1/(1-\alpha)}$$



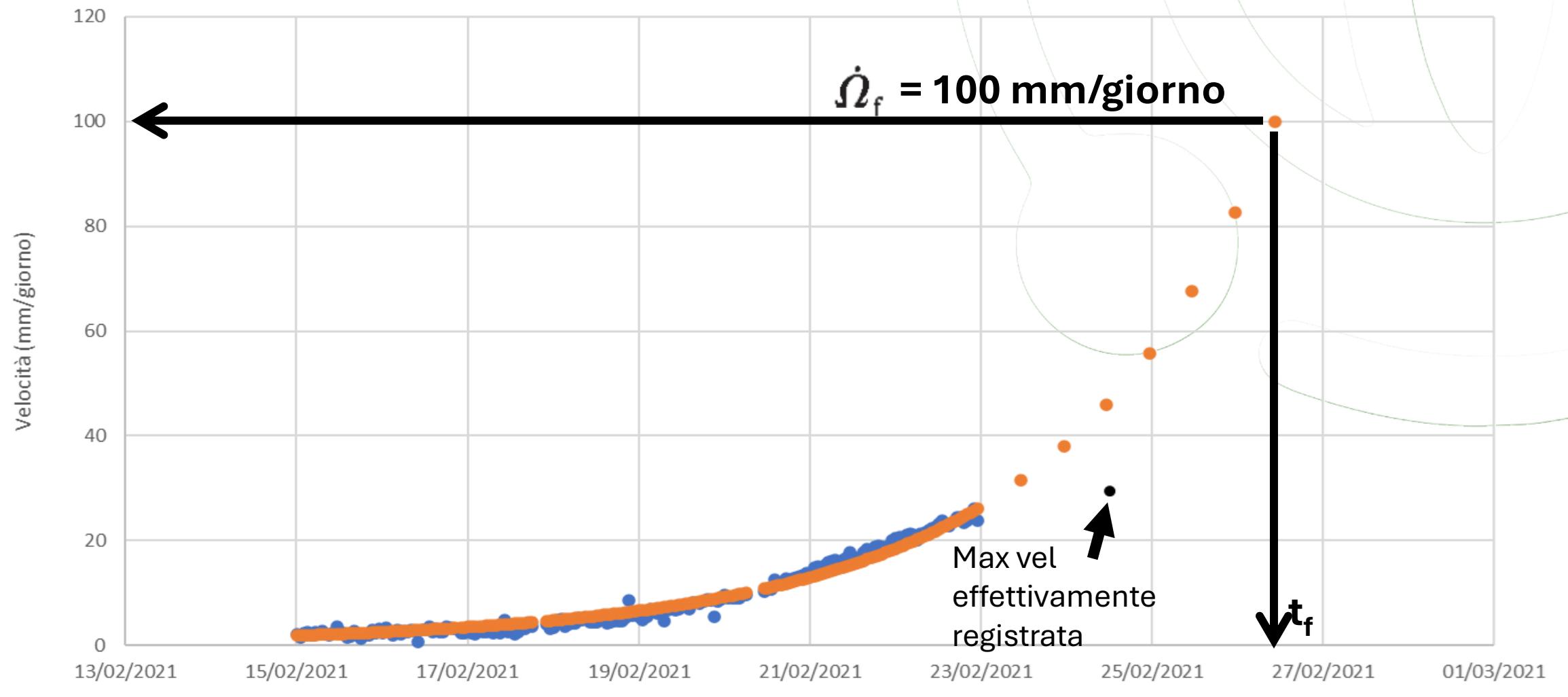
Non linear fitting



Velocity curve

Velocità 24h D7

● Velocità misurata ● Velocità stimata



Forecasting overview

Criterio per selezione soglia rossa



Criterio per selezione soglia arancione



	settore	Ore a failure da previsione in data 22/02	Vel +12h	Vel +24h	Vel +36h	Vel +48h	Vel +60h	Vel +72h	vel max effettivamente registrata	data vel max effettivamente registrata
'X5.csv'	1		106	18.1	22.1	27.1	33.4	41.4	51.5	17.4
'X7.csv'	1		104	20.9	25.3	30.7	37.4	45.8	56.2	18.3
'X8.csv'	1		106	19.6	23.8	25.9	35.4	43.4	53.6	15.9
'XN12.csv'	1		104	19.9	24.2	29.5	36.1	44.5	54.9	17.7
'XN13.csv'	1		105	20.8	25.1	30.4	37	45.2	55.5	18.9
'Y01.csv'	1		104	20.1	24.4	29.7	36.4	44.7	55.1	16.6
'Y02.csv'	1		102	21.4	26	31.6	38.6	47.2	58.1	18.9
'Y03.csv'	1		99	22.2	27	32.9	40.3	49.5	61.1	17.7
'Y04.csv'	1		100	20.7	25.3	31	38.3	47.4	57.9	17.8
'Y05.csv'	1		103	20.9	25.4	30.9	37.8	46.3	57	19.1
MEDIA SETTORE1			103.30	20.46	24.86	29.97	37.07	45.54	56.09	17.84
'XN15.csv'	2		96	23.2	28.2	34.4	42.2	51.9	64	21.65
'XN16.csv'	2		94	24	29.3	35.8	43.8	53.9	66.5	20.95
'XN18.csv'	2		97	25.5	30.6	36.9	44.6	54.1	65.8	22.94
'Y06.csv'	2		103	23	27.6	33.2	40.2	48.6	59.1	20.48
MEDIA SETTORE2			97.50	23.93	28.93	35.08	42.70	52.13	63.85	21.51
'CL5BIS.csv'	3		106	22.6	27.1	33.1	39.2	47.3	57.2	22.55
'D5.csv'	3		97	24.1	29.1	35.7	43	52.4	64.3	22.92
'D6.csv'	3		107	23.5	28.1	34.2	40.2	48.2	57.9	24.65
'D7.csv'	3		83	31.5	37.9	46.2	55.6	67.7	82.6	29.35
'XN14.csv'	3		93	26.3	31.7	39.8	46.4	56.4	68.8	25.80
'Y09.csv'	3		83	32.2	38.8	46.9	56.6	68.5	83.1	27.90
MEDIA SETTORE3			94.83	26.70	32.12	39.32	46.83	56.75	68.98	25.53

Proposed thresholds

		Stazione totale		
		settore 1	settore 2	settore 3
Giallo	10	12.5	15	
	18	22	26	
	30	35	40	

Note:

- ai prismi all'esterno del perimetro di frana si associano le soglie più basse (settore 1)
- le soglie relative al livello giallo sono state calibrate sulla base del rumore della serie di dati

Timeline D7

Stazione totale			
	settore 1	settore 2	settore 3
Giallo	10	12.5	15
Arancione	18	22	26
Rosso	30	35	40

Entrata	Uscita
21/2/21 4.10	22/2/21 22.13
22/2/21 22.13	22/2/21 23.11
22/2/21 23.11	23/2/21 6.10
23/2/21 6.10	23/2/21 15.11
23/2/21 15.11	23/2/21 16.10
23/2/21 16.10	23/2/21 22.10
23/2/21 22.10	23/2/21 23.11
23/2/21 23.11	24/2/21 2.11
24/2/21 2.11	24/2/21 3.10
24/2/21 3.10	24/2/21 17.11
24/2/21 17.11	24/2/21 19.10
24/2/21 19.10	25/2/21 3.10
25/2/21 3.10	25/2/21 6.10
25/2/21 6.10	25/2/21 8.11
25/2/21 8.11	3/3/21 11.12



19/02/2021

21/02/2021

23/02/2021

25/02/2021

27/02/2021

01/03/2021

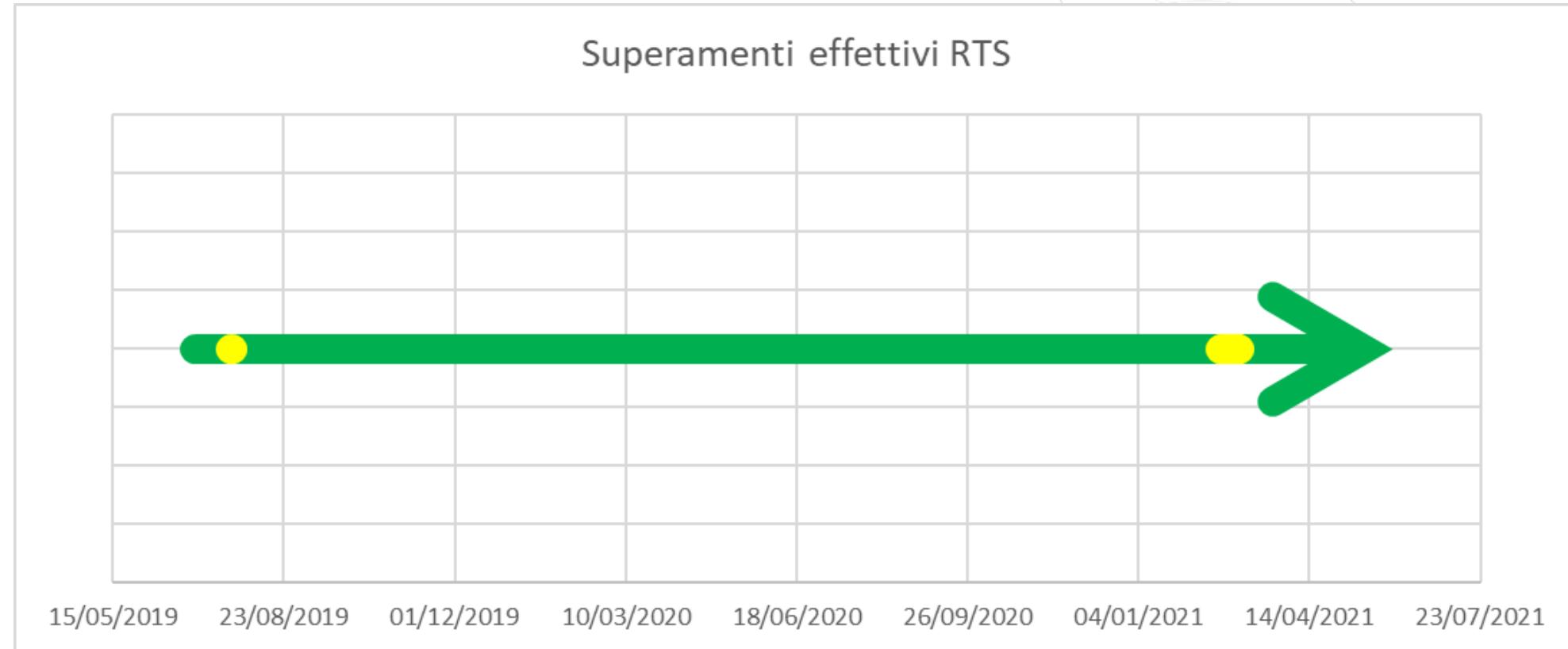
03/03/2021

05/03/2021

Criticality activation criteria

- 1) almeno il 50% dei prismi di ciascun settore > soglia**
- 2) almeno 2 settori su 3**

Entrata	Uscita
22/7/19 18.24	22/7/19 19.16
21/2/21 9.23	21/2/21 15.14
21/2/21 18.17	2/3/21 1.19
2/3/21 6.17	2/3/21 10.20
2/3/21 14.21	2/3/21 16.23
3/3/21 8.21	3/3/21 15.18



Monitoring and early warning platforms



Trimble Connect



part of Hexagon

LISALAB



Scientific Instrumentation



Data Sharing and EW Platform

LOGO

+ Layers Styles

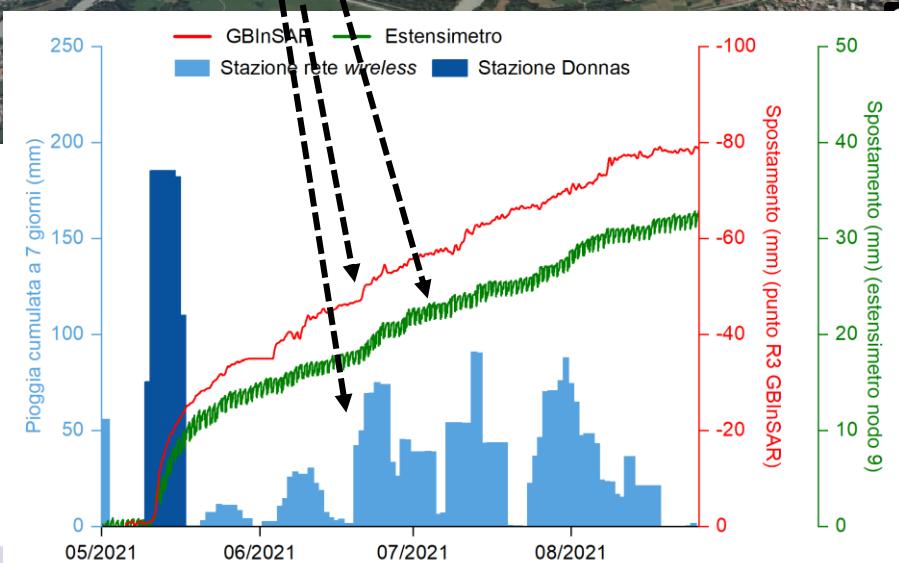
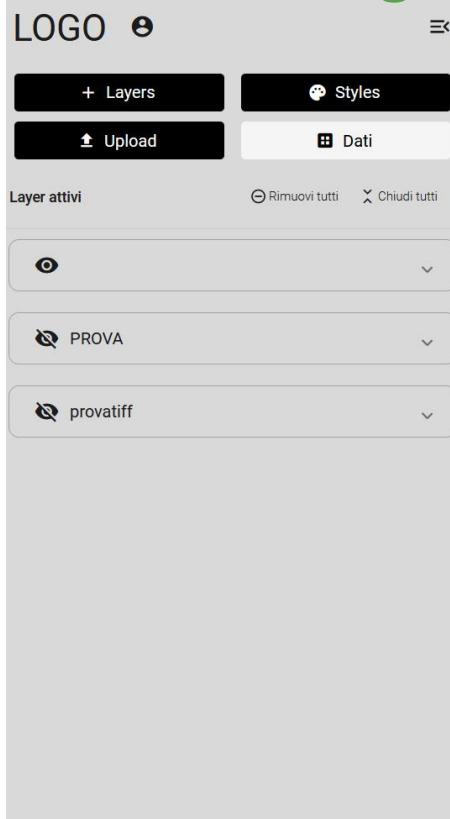
Upload Dati

Layer attivi

Rimuovi tutti Chiudi tutti

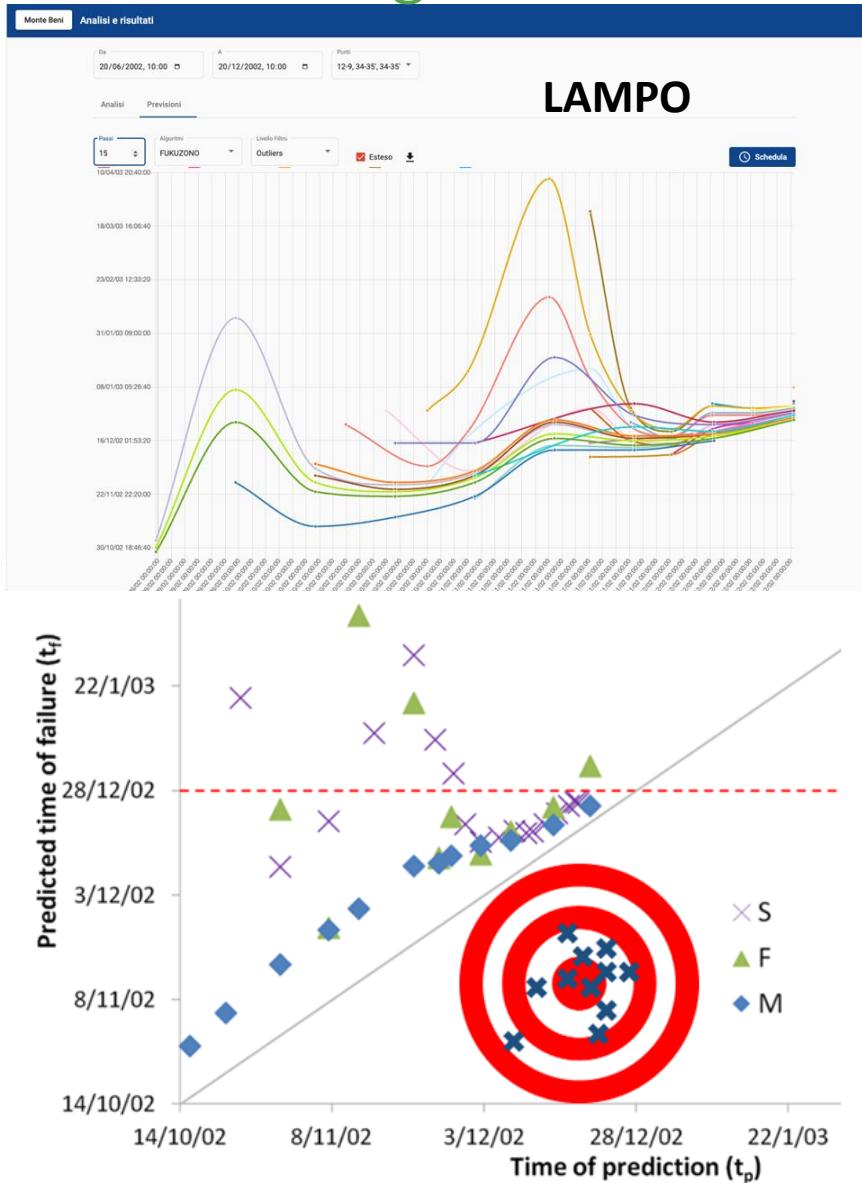
PROVA

provatiff



- Display and share planimetric and 3D data
- Real-time monitoring data
- Customised diagrams
- Dashboard for emergency management
- Tools for quickly defining risk scenarios
- Real-time forecasting algorithms
- Definition of alarm thresholds
- Threshold exceeding notifications

Forecasting Models

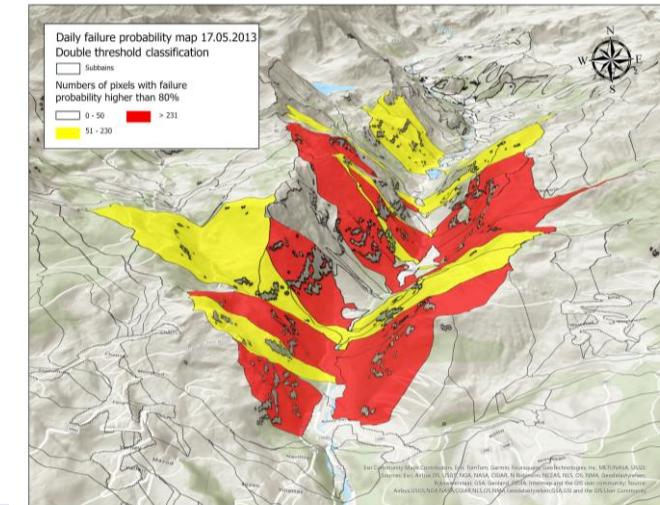
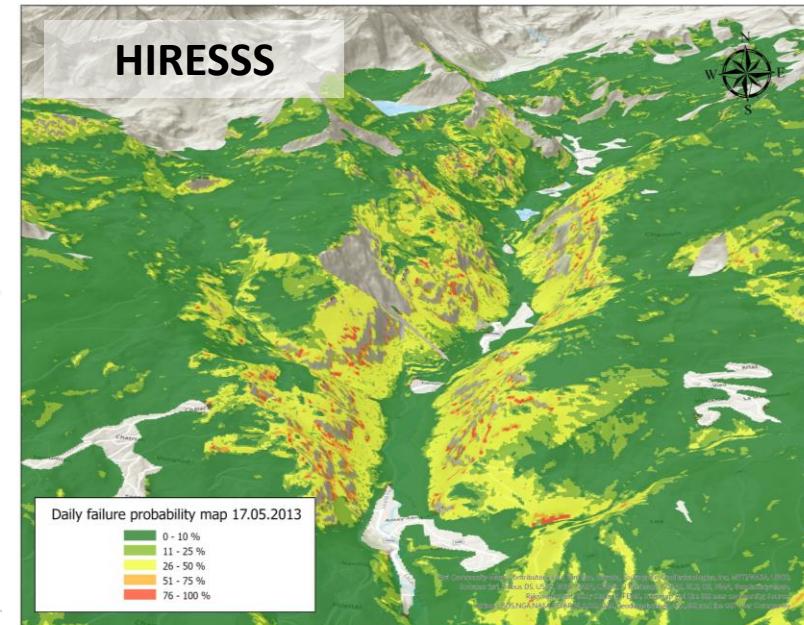
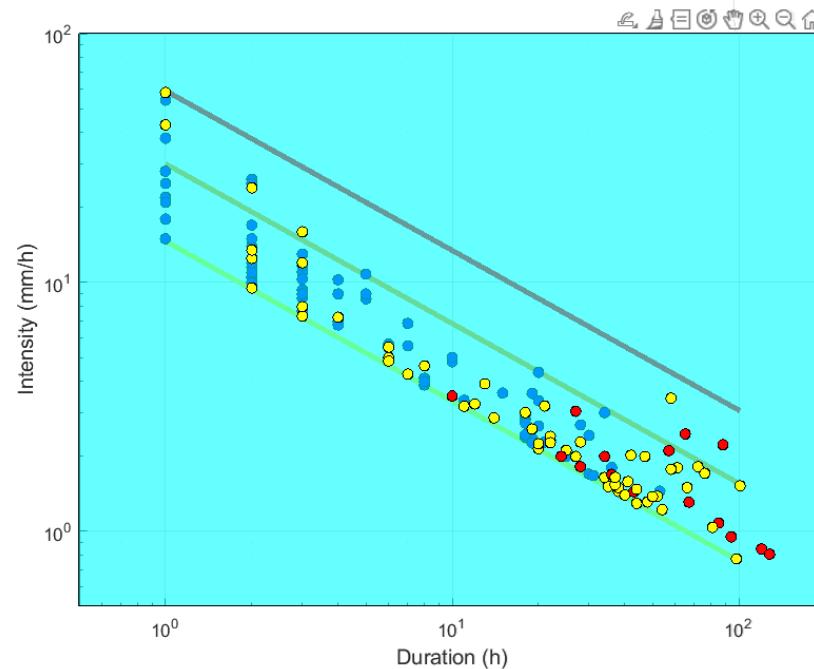


PROTEZIONE CIVILE
Pre Dip



MACUMBA

- False Alarms
- Correct Alarms
- I-D Low Criticality Threshold
- I-D Moderate Criticality Threshold
- I-D High Criticality Threshold
- OMAR Threshold
- Filtered False Alarms



References



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